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by

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ABSTRACT

An approximated formula for the vertical attenuation coefficient as a function of the absorption coefficient, the scattering coefficient, the sun height, the cloudiness and the depth is deduced. A relation between only the vertical attenuation coefficient, sun height, cloudiness and depth is also proposed.

THE VERTICAL ATTENUATION COEFFICIENT OF SUBMARINE IRRADIANCE.

1. INTRODUCTION.

While analyzing irradiance observations at 465 nm from the Norwegian Sea and the Barents Sea (AAS and BERGE, 1976), a relation between the vertical attenuation coefficient and the sun height was needed. A usual assumption is that close to the surface the vertical attenuation coefficient K of downward irradiance will be related to the zenith angle j of the refracted sun rays by the relation

$$K = K / \cos j = K \sec j$$
 (1)

K is then the coefficient for a zenith sun.

This relation has been tested by KOSLYANINOV and PELEVIN (1966), JERLOV and NYGARD (1969), and HØJERSLEV (1973, 1974 a). KOSLYANINOV and PELEVIN found the relation valid down to an optical depth cz = 2.5 (c is the beam attenuation coefficient, z is the depth), JERLOV and NYGARD found it valid down to 10 m for green light in the Baltic Sea and to 75 m for blue light in the Sargasso Sea. Both these depths correspond roughly to an optical depth 4. According to HØJERSLEV (1974a) it should be expected from theory that K was essentially independent of the sun height for sun heights less than 25° . He found for green light in the Baltic little variation for heights less than 40° . In the Mediterranean he found for blue light little dependence upon the sun height for heights less than 50° (1974 b).

It is, however, clear that it should be a gradual transition from the state when the "secans relation" (eq.1) is valid to the state when it is not.

- 1 -

In connection with the before-mentioned irradiance measurements in the Norwegian Sea and the Barents Sea there were no measurements of the optical depth cz, so the formula which is developed here is based finally only on observed values of vertical attenuation coefficient, cloudiness, sun height and depth.

2. THE FUNCTION K_d(a,R,D_D,j,r).

For an ocean which is optically homogeneous in horrisontal directions, the GERSHUN equation (1939) yields

$$\frac{\mathrm{d}}{\mathrm{d}z}(\mathrm{E}_{\mathrm{d}} - \mathrm{E}_{\mathrm{u}}) = -\mathrm{a}\mathrm{E}_{\mathrm{o}} \tag{2.1}$$

 E_d is downward irradiance, E_u upward irradiance, a is the absorption coefficient and E_o is the scalar irradiance. By introducing the vertical attenuation coefficients K_d and K_u , defined by

$$K_{d} = -\frac{1}{E_{d}} \frac{dE_{d}}{dz}, \quad K_{u} = -\frac{1}{E_{u}} \frac{dE_{u}}{dz}$$
 (2.2)

and the downward and upward part of the scalar irradiance,

$$E_{o} = E_{od} + E_{ou}$$
(2.3)

the equation becomes

$$K_{d}E_{d} - K_{u}E_{u} = a(E_{od} + E_{ou})$$
 (2.4)

By means of the irradiance ratio

$$R = \frac{E_u}{E_d}$$
(2.5)

and the scalar irradiance ratio

$$R_{o} = \frac{E_{ou}}{E_{od}}$$
(2.6)

eq. 2.4 may be written

$$K_{d} = a \frac{E_{od}(1+R_{o})}{E_{d}(1-R_{W}K_{d})} = a \frac{D_{d}(1+R_{o})}{1-R_{W}K_{d}}$$
(2.7)

The function

$$D_{d} = {}^{E} od / {}_{E_{d}}$$
(2.8)

is termed the downward distribution function by TYLER and PREISENDORFER (1962). In Table 1, which is calculated and interpolated from TYLER's radiance observations at 480 nm in Lake Pend Oreille (TYLER and PREISENDORFER, 1962), it is seen that the relative standard deviation, S_{rel} , of the ratio K_u/K_d is 4%, and that the mean value of the ratio is 1.02. It is also seen that the standard deviation of the ratio R_o/R is 2%, and that the mean value is 2.13. In lack of other knowledge I then make the assumptions

$$\frac{R_{u}}{R_{d}} \approx 1$$

$$\frac{R_{o}}{R} \approx 2$$
(2.9)
(2.10)

and eq. 2.7 becomes, since from Table 1 R << 1,

$$K_{d} \approx \frac{a D_{d}(1+2R)}{1-R} \approx a(1+3R)D_{d} \qquad (2.11)$$

The equation (2.11) may also be obtained in the following way: Table 1 gives that the upward distribution function

$$D_{u} = \frac{E_{ou}}{E_{u}}$$
(2.12)

has the mean value 2.8 with a standard deviation of 2%. If we assume that this value has a general validity, we may return to eq. 2.4 and write it

- 3 -

$$K_{d}E_{d} - K_{u}E_{u} \approx a(E_{od} + 2.8 E_{u})$$
 (2.13)

This may be rewritten as

$$K_{d}E_{d}(1 - \frac{K_{u}}{K_{d}}R - \frac{2.8 a}{K_{d}}R = a E_{od}$$
 (2.14)

From Table 1 it is seen that the mean value of a/K_d in this case is 0.7, so that

$$K_{d}E_{d}(1 - R - 2R) = K_{d}E_{d}(1 - 3R) = a E_{od},$$
 (2.15)

or again

$$K_{d} \approx a(1 + 3R)D_{d}$$
. (2.16)

The distribution function D_d is a function of the down-ward radiance L, given by

$$D_{d} = \frac{E_{od}}{E_{d}} = \frac{\int L d \omega}{\int L \cos \Theta d\omega} = \frac{1}{\cos \Theta_{M}} = \sec \Theta_{M} \quad (2.17)$$

dw is an infinitesimal solid angle in the direction of L, and the integral is performed in the upper hemisphere. 0 is the angle between L and the vertical. $\Theta_{\rm M}$ is the mean value of 0 in the integral. When the two integrals in eq. 2.17 are dominated by the radiance from the sun, $\Theta_{\rm M}$ will be close to j, and eq. 2.16 will be of the same form as eq. 1. In the case of a clear sky in Table 1, the sun height was 56.6°. This makes sec_j = 1.10, which is not equal to the values of D_d.

The distribution function may be separated into two main factors, namely the contribution from the direct sun light and from the diffuse light. If the radiance from the diffuse light is termed L_D and the radiance from the sun L_S , we get from eq. 2.17

_ 4 _

$$\frac{E_{od}}{E_{d}} = \frac{L_{S}^{d\omega}S + \int L_{D}^{d\omega}}{L_{S}^{cos} \int d\omega_{S} + \int L_{D}^{d\omega}}$$
(2.18)

The direct contribution to the irradiance from the sun is

$$E_{dS} = L_S \cos j \, d\omega_S \tag{2.19}$$

which makes

$$L_{S}d\omega_{S} = E_{dS}sec j.$$
 (2.20)

The contribution to the irradiance from the diffuse light is

$$E_{dD} = \int L_{D} \cos \Theta d\omega = \cos \Theta_{D} \int L_{D} d\omega \qquad (2.21)$$

$$2\pi - d\omega_{S}$$

where Θ_{D} is the mean value of Θ in the integration. We may write eq. 2.21 as

$$\int_{2\pi - d\omega_{\rm S}} L_{\rm D} d\omega_{\rm S} = E_{\rm dD} \sec \Theta_{\rm D}$$
(2.22)

and eq. 2.18 then becomes

$$\frac{E_{od}}{E_{d}} = \frac{E_{dS}^{sec} j + E_{dD}^{sec} \Theta_{D}}{E_{dS} + E_{dD}}$$
(2.23)

Since

$$E_{dD} = E_{d} - E_{dS}, \qquad (2.24)$$

eq. 2.23 may be written

$$D_{d} = \frac{E_{od}}{E_{d}} = \frac{E_{dS} \sec j + (E_{d} - E_{dS}) \sec \Theta_{D}}{E_{d}}$$

= $\sec \Theta_{D} + (\sec j - \sec \Theta_{D}) \frac{E_{dS}}{E_{d}}$ (2.25)

- 5 -

The unknown distribution function D_d has then been separated into a known function of the solar altitude, sec j, a still unknown distribution function of the diffuse light,

$$\sec \Theta_{\rm D} = D_{\rm D} \approx \frac{2\pi L_{\rm D}^{\rm d\omega}}{\int L_{\rm D} \cos \Theta d\omega}$$
(2.26)

and an unknown ratio between the solar contribution to the irradiance and the total irradiance. The relation between the sun height h and the sun ray's angle of refraction j is given by SNELL's law in the form

$$\sec j = 1/\sqrt{1-(\frac{3}{4})^2 \cos^2 h}$$
 (2.27)

Eq. 2.16 and 2.25 give

$$K_{d} = a(1+3R)(\sec \theta_{D} + (\sec j - \sec \theta_{D}) \frac{Ed_{S}}{E_{d}}) \qquad (2.28)$$

For convenience, we may now omit the index d and introduce

$$a_p = a(1 + 3R)$$
 (2.29)

and

$$\mathbf{r} = {}^{\mathrm{E}}\mathrm{S}/\mathrm{E} \tag{2.30}$$

We then have for the vertical attenuation coefficient

$$K = a_{R}(\sec \theta_{D} + (\sec j - \sec \theta_{D})r)$$
(2.31)

I assume that the distribution function $D_D = \sec \theta_D$ of the diffuse light may be regarded as independent of the sun height, at least compared with the function sec j of the direct sun rays. The ratio r, however, should be a function of the sun height, the cloudiness, the depth and the turbidity of the water.

When the sun is dominating the irradiande, r will be close to 1 and K will be given by

When the diffuse light is dominating, r will be close to 0, and K will be given by

$$K = a_R \sec \theta_D$$
 (2.33)

3. THE FUNCTION r_o(h,C).

In eq. 2.30 the downward irradiance E may be expressed as

$$E(z) = E(o) e^{-Kz}$$
 (3.1)

where z is the depth.

Similarly we may express E_S as

$$E_{S}(z) = E_{S}(0) e^{-K_{S}z}$$
 (3.2)

where K_S is the still unknown vertical attenuation coefficient of the sun rays. Eq. 2.30 may then be written

$$r = \frac{E_{S}(z)}{E(z)} = \frac{E_{S}(o)}{E(o)} e^{-(K_{S}-K)z} = r_{o}e^{-(K_{S}-K)z}$$
(3.3)

where

$$r_{o} = \frac{E_{S}(o)}{E(o)}$$
(3.4)

The function r_0 is the value of r just beneath the sea surface, and will depend on E_S and E in air, and on their transmission through the sea surface. We

shall first consider their ratio in air

$$r_{a} = \frac{E_{sa}}{E_{a}}$$
(3.5)

In clear weather this ratio is mainly a function of wavelength and sun height, Fig. 1, but it depends also on the transmittance of the air, that is on the dust and vapour contents of the air (KIMBALL, 1924, HINZPETER, 1955,1956,1957, GATES, 1966), and on the albedo of the ground (DEIRMENDJIAN and SEKERA, 1954). Due to the low albedo of the sea, the last effect will only reduce r_a with maximum 2% at small sun heights at sea, and this effect shall be disregarded here. r_o is obtained from r_a by

$$r_{o} = \frac{\tau_{S} r_{a}}{\tau_{S} r_{a}^{+} \tau_{D} (1 - r_{a})}$$
(3.6)

Here $\tau_{\rm S}$ is the Fresnel transmittance of the sun rays through the sea surface and $\tau_{\rm D}$ is the corresponding transmittance of the diffuse irradiance. I have chosen $\tau_{\rm D}$ = 0.93 (isotropic radiance distribution).

The three cases in Fig. 1 may then be expressed as

a) $r_0 = 1/(1 + 0.13 \operatorname{cosec} h e^{0.20 \operatorname{cosec} h}$ (3.7)

b)
$$r_0 = 1/(1 + 0.20 \operatorname{cosec} h e^{-0.22 \operatorname{cosec} h})$$
 (3.8)

c)
$$r_0 = 1/(1 + 0.27 \operatorname{cosec} h e^{0.50 \operatorname{cosec} h})$$
 (3.9)

In lack again of other knowledge I have chosen

$$r_0 = 1/(1 + 0.2 \operatorname{cosec} h e^{0.3 \operatorname{cosec} h})$$
 (3.10)

When there are clouds, the solar irradiance may be reduced to a mean value of

$$E_{S}' = E_{S}(1 - C)$$
 (3.11)

- 8 -

C is the cloudiness in parts of one. Correspondingly the contribution of diffuse light from the blue part of the sky will be $E_D(1 - C)$. The contribution of diffuse light from the cloudy part of the sky may be written E_CC . E_C is the irradiance when the cloudiness is 1. By comparison with data by KALITIN (KONDRATYEV, 1969, p. 459) and ROBINSON (1966, p. 214-216), I have chosen as a mean value $E_C \approx 0.5$ E, where E is the irradiance of a clear sky. r_O then becomes

- 9 -

$$r_{o}' = \frac{E_{S}'}{E_{S}' + E_{D}} = \frac{E_{S}(1-C)}{ES(1-C) + E_{D}(1-C) + 0.5EC}$$

$$= \frac{ES(1-C)}{E(1-C+0.5C)} = r_0 \frac{1-C}{1-0.5C}$$
(3.12)

Thus the effect of clouds is the correction term (1 - C)/(1 - 0.5C). Eq. 3.10 and 3.12 give

 $r_{o}' = \frac{1 - C}{1 - 0.5C} / (1 + 0.2 \operatorname{cosec} h e^{0.3 \operatorname{cosec} h}) (3.13)$

4. THE FUNCTION r(r_o,a,b,K,j,z).

In eq. 3.2 the sun rays are attenuated by the coefficient

$$K_{\rm S} = (a + b) \sec j$$
 (4.1)

However, as about 50% of the scattered light will be contained within a 10[°] cone around the rays (JERLOV, 1968, p. 39) it is questionable if all of this light should be considered as lost from the solar irradiance. If not, it may be more correct to write

 $K_{S} = (a + \alpha b) \sec j$

(4.2)

where α is the fraction of b which contributes to the attenuation.

In Chapter 5 it is found that this factor α is 0.86.

With this value eq. 3.3 becomes

$$r = r_0 e^{-((a+0.86b)sec j - K)z}$$
 (4.3)

5. THE FUNCTION D_D(a,b,K,j,z).

Measurements of the downward distribution function of diffuse light, $D_D = \sec \Theta_D$, are rather few. JERLOV and LILJEQVIST (1938) found that the ratio E_O/E_d at 530 nm in cloudy weather had values between 1.33 and 1.37. TYLER's observations at 480 nm, quoted in Table 1, give values of D_d in cloudy weather between 1.29 and 1.34. In the last case the values may seem to increase asymptotically from the surface and down towards a fixed value.

From HØJERSLEV's observations at 477 nm (1973, 1974a), the least squares method gives (Table 2) that the sum

$$\Sigma(K-(a_{R}(\sec \Theta_{D} + (\sec j - \sec \Theta_{D})r_{O}e^{-(K_{S}-K)z} 2)))$$
(5.1)
where $K_{S} = (a + \alpha b)sec j$, obtains its lowest value
for $\alpha = 0.72$ and sec $\Theta_{D} = 1.38$. However, if we solve
for $sec \Theta_{D}$ from eq. 2.31, we get

$$\sec \Theta_{\rm D} = \frac{{\rm K/a_R} - {\rm r} \sec j}{1 - {\rm r}}$$
(5.2)

and the ratio on the right side of this equation does not seem to be constant. I will, as already mentioned, assume that sec Θ_D has less variation with the sun height than sec j, but that it may have the same kind of variation with depth as TYLER's measurements indicate. From eq. 5.2 it seem natural that sec Θ_D should have the same dependence on depth as r, and I have then chosen the simple form

sec
$$\Theta_{\rm D} = \beta - \gamma e^{-(K_{\rm S}-K)z}$$
 (5.3)

The sum 5.1 will now get a still lower value for $\alpha = 0.86$, $\beta = 1.41$, and $\gamma = 0.21$ (Table 2). The last form of sec Θ_D ,

sec
$$\theta_{\rm D}$$
 = 1.41 - 0.21 e^{-((a+0.86 b)sec j-K)z (5.4)}

has the interesting result that sec $\Theta_D = 1.20$ just beneath the surface. If we assume that the diffuse radiance is constant inside the critical solid angle of total reflection and zero outside, then sec Θ_D becomes

$$\sec \Theta_{\rm D} = \frac{2\pi \int_{0}^{\Theta} L_{\rm D} \sin \Theta \, \mathrm{d}\Theta}{2\pi \int_{0}^{\Theta} L_{\rm D} \sin \Theta \, \cos \Theta \, \mathrm{d}\Theta} = \frac{1 - \cos \Theta_{\rm C}}{\sin^2 \Theta_{\rm C}/2} = \frac{2}{1 + \cos \Theta_{\rm C}} \quad (5.5)$$
$$= 1.20$$
since $\Theta_{\rm C} = 48.3^{\circ}.$

Thus from this result the diffuse radiance seems to be contained within the critical solid angle at zero depth. With increasing depth the value of sec 0_D increases asymptotically from 1.20 towards 1.41.

While this result was obtained for light at 477 nm, I shall assume that it is also valid at 465 nm.

$$K = a_{R}(\sec \theta_{D} + (\sec j - \sec \theta_{D})r)$$
 (6.1)

where

$$a_{R} = a(1 + 3R),$$
 (6.2)

sec
$$\theta_{\rm D} = 1.41 - 0.21 \, {\rm e}^{-(K_{\rm S}-K)Z}$$
 (6.3)

$$r = r_0 e^{-(K_S - K)z}$$
 (6.4)

$$r_0 = \frac{1 - C}{1 - 0.5C} / (1 + 0.2 \operatorname{cosec} h e^{0.3 \operatorname{cosec} h}) (6.5)$$

sec j =
$$(1 - (\frac{3}{4})^2 \cos^2 h)^{-\frac{1}{2}}$$
 (6.6)

$$K_{\rm S} = (a + 0.86 b) \sec j$$
 (6.7)

This gives a functional relation between K, R, a, b, h, C and z. However, if we should want to calculate K, eq. 6.1 does not give an explicit solution for K. It would be more practical if R and K on the right side of the equation were substituted with approximated functions of a, b, h and z. In Chapter 7 it is deduced that

$$R \approx 0.009 \text{ b/a}$$
 (6.8)

It is also decuced that

$$K \approx (a + 0.022 b)D_d$$
 (6.9)

so that

 $K_{\rm S}$ - K \approx a(sec j - D_d) + b(0.86 sec j - 0.022 D_d) (6.10) In Table 2 it is shown that an approximated form of this is $K_{\rm S}$ - K \approx -0.01 a + 0.73 b sec j \approx 0.73 b sec j (6.11) Thus the equations 6.1-6.6, 6.8 and 6.11 give K(a,b,h,c,z). Fig. 2 shows calculated and observed values of K, based on the same data by HØJERSLEV as used in Table 2. If we have observations of a and b then K_S is determined from eq. 6.7. However, in my case, I have measurements only for K, so that K_S should rather be expressed as a function of K. The contents of yellow substance in the Norwegian Sea and the Barents Sea is very low, except in the coastal areas. The attenuation should then be dominated by particles, and if we assume that there is a fairly constant ratio between the scattering and absorption coefficients, there may also be an almost constant ratio between (a + 0.86b)sec j and K. Table 2 gives for Mediteranean waters with low yellow substance contents that this ratio is 2.12. Eq. 6.7 then becomes

$$K_{\rm S} \approx 2.12 \text{ K}$$
 (6.12)

The difference K_S - K may then just as well be approximated to the simple expression

$$K_{S} - K \approx K \tag{6.13}$$

The equations 6.1-6.6 and 6.13 then defines a relation between K, a_R , h and z. In Table 3 are given calculated values of K for 3 different values of a_R in 0, 10 and 20 m depth. It is seen that according to this model the maximum value of K will not occure for $h = 0^{\circ}$, but for $h \approx 20^{\circ}$. It is also seen that the mean value of K in the range 0 - 20 m coincides very well with the value of K calculated for 10 m. In the before-mentioned work by AAS and BERGE the mean value of K between the surface and 20 m depth was derived from irradiance observations.

To obtain the value of K for
$$h = 35^{\circ}$$
 and $C = 0$, the relation

$$\frac{K(35,0,)}{K(h,C)} = \frac{(\sec \theta_D + (\sec j - \sec \theta_D)r)_{35,0,10}}{(\sec \theta_D + (\sec j - \sec \theta_D)r)_{h,C,10}}$$
(6 14)

where

$$(\text{sec } j)_{35} = 1.27$$
 (6.15)

$$r_{035,0} = 0.63$$
 (6.16)

was used. This relation may then be written

$$\overline{K(35,0)} = \overline{K(h,C)} \frac{1.41 - 0.298 e^{-10K} + 0.132 e^{-20K}}{1.41 - (0.21 + (1.41 - \sec j)r_0)e^{-10K} + 0.21r_0 \bar{e}^{20K}}$$
(6.17)

whre r_0 is given by eq. 6.5.

7. APPENDIX 1.

THE MODEL OF KOZLYANINOV AND PELEVIN.

The following is a very simplified presentation of the model of KOZLYANINOV and PELEVIN (1966).

$$\frac{dE_{d}}{dz} = -(a' + b')E_{d} + b'E_{u}$$
(7.1)

$$-\frac{dE_{u}}{dz} = -(a'+b')E_{u} + b'E_{d}$$
(7.2)

By differensiating the first of these two simplified equations of transfer with regard to z, and then eliminating dE_u/dz by means of the second, one obtains

$$\frac{d^{2}E_{d}}{dz^{2}} = (a'^{2} + 2a'b')E_{d}$$
(7.3)

KOZLYANINOV and PELEVIN term a' the "efficient" coefficient of absorption and b' the "efficient" coefficient of scattering, and to obtain a practical formula, they have made the approximation that these coefficients are the same for downward and upward irradiance. By definition a' is

$$a' = a \frac{2\pi}{\int L \cos \Theta \, d\omega} = a D \qquad (7.4)$$
$$\frac{2\pi}{2\pi}$$

With the assumption

$$\frac{b'}{b_b} = \frac{a'}{a} = D \tag{7.5}$$

where b_b is the backward scattering coefficient, and by assuming that the distribution function D varies only little with depth in the upper layer of the sea, eq. 7.3 may be integrated to

$$E_{d}(z) = E_{d}(o) e^{-\sqrt{a^{2}+2ab_{b}}Dz}$$
 (7.6)

By inserting this expression in eq. 7.1 and solving for E_{μ} one gets

$$E_{u} = \frac{a + b_{b} - \sqrt{a^{2} + 2ab_{b}}}{b_{b}} E_{d}(o) e^{-\sqrt{a^{2} + 2ab_{b}} Dz}$$
(7.7)

Thus

$$K_{d} = K_{u} = \sqrt{a^{2} + 2ab_{b}} D$$
 (7.8)

and

$$R = \frac{E_{u}}{E_{d}} = \frac{a + b_{b} - \sqrt{a^{2} + 2ab_{b}}}{b_{b}}$$
(7.9)

By solving for b_b from eq. 7.9, one gets

$$b_{b} = \frac{2a R}{(1-R)^{2}}$$
 (7.10)

and substitution of this value in eq. 7.8 gives

$$K = a \frac{1 + R}{1 - R} D$$
 (7.11)

In order to see better the resemblance between this expression and eq. 2.16, we should make some simplifications. By dividing numerator and denumerator in eq. 7.9 with $a+b_b$, and noting that $a^2+2ab_b=(a+b_b)^2-b_b^2$, one gets

$$R = \frac{1 - \sqrt{1 - b_b^2 / (a + b_b)^2}}{b_b / (a + b_b)}$$
(7.12)

Now the ratio $b_b/(a+b_b) = (b_b/a)/(1+b/a)$ is very small. For particles $b_b/b \approx 0.02$ (JERLOV 1968, p. 39). So when particles are dominating the attenuance with a and b of the same order, the ratio b_b/a too will be of order 0.02. When yellow substance is dominating the attenuance, the ratio will be even smaller. For <u>pure</u> sea water at 465 nm b_b/a will have its highest value, about 0.1. The square root in eq. 7.12 may then be expanded to

$$R = \frac{1 - (1 - \frac{1}{2} - \frac{b_b^2}{(a + b_b)^2})}{\frac{b_b}{(a + b_b)}} = \frac{1}{2} \frac{\frac{b_b}{a}}{1 + \frac{b_b}{a}} \approx \frac{1}{2} \frac{\frac{b_b}{a}}{a} (1 - \frac{b_b}{a}) (7.13)$$
$$\approx \frac{1}{2} \frac{b_b}{a}$$

Since R is of the same order as b_b/a_s eq. 7.11 may be approximated to

$$K = a(1 + 2R)D$$
 (7.14)

Thus by eq. 7.8, the model of KOZLYANINOV and PELEVIN justifies the earlier assumption in eq. 2.9: $K_d \approx K_u$, and eq. 7.14 confirms the result in eq. 2.16. The only difference is the factor 1 + 2R instead of 1 + 3R, but since R is a small number, this difference is small. The difference originates from the observa ion in eq. 2.10 which yields

$$\frac{R_o}{R} = \frac{E_{ou}E_d}{E_{od}E_u} = \frac{D_u}{D_d} \approx 2$$
(7.15)

or

$$D_{u} \approx 2D_{d} \tag{7.16}$$

However, according to eq. 7.1, 7.2, and 7.4 in the present model

$$a'_{u} = aD_{u} = a'_{d} = aD_{d}$$
(7.17)

or

$$D_{u} = D_{d} = D$$
 (7.18)

which is certainly less correct.

Expansion of the square root in eq. 7.8 gives the interesting result

$$K = a\sqrt{1 + 2b_{b/a}} D \approx a(1 + b_{b/a})D$$
(7.19)
$$= (a + b_{b})D = (a + \varepsilon b)D$$

where

$$\epsilon = b_{\rm b}/b \tag{7.20}$$

As already mentioned, ε may be about

$$\epsilon = b_{b/b} \approx 0.02 \tag{7.21}$$

except when the water is very pure.

From similtaneous observations of K,a,b, and D, we

should then expect that

$$K = (a + 0.02 b)D$$
 (7.22)

HØJERSLEV (1973, 1974a) has presented such observations, and by applying the least square method as shown in Table 2, his data give

$$K = (a + 0.022 b)D_d$$
 (7.23)

With the assumption in eq. 7.21, one should expect that

$$R \approx \frac{1}{2} \frac{0.02 \text{ b}}{a + 0.02 \text{ b}}$$
(7.24)

or

or

$$R \approx \frac{1}{2} \frac{0.02 \text{ b}}{a}$$
 (7.25)

In fact, the same set of data gives, as shown in Table 2, that

$$R \approx \frac{1}{2} \frac{0.015 \text{ b}}{a \div 0.015 \text{ b}}$$
(7.26)

$$R \approx \frac{1}{2} \frac{0.017 \text{ b}}{a} \tag{7.27}$$

8. APPENDIX 2.

THE MODEL OF LUNDGREN AND HØJERSLEV.

LUNDGREN and HØJERSLEV (1971) deduced the approximated equation

$$K_{d} \simeq a(4R + sec j) \tag{8.1}$$

By following the assumptions in their model, but not their procedure, we may obtain a result which is more similar to eq. 6.1.

Their simplified model of radiance distribu-

tion consists of three radiance types:

- 1) The direct radiance L_{S} from the sun.
- 2) The diffuse constant radiance L_D inside the solid angle of total reflection.
- 3) The diffuse constant radiance L u outside the solid angle of total reflection.

The downward solar irradiance Es then

becomes

$$E_{g} = L_{g} \cos j \, d\omega_{g} \tag{8.2}$$

The downward diffuse irradiance E_D becomes

 $E_{\rm D} = \int_{0}^{\theta} 2\pi L_{\rm D} \sin \theta \cos \theta \, d\theta + \int_{0}^{\pi/2} 2\pi L_{\rm U} \sin \theta \cos \theta \, d\theta$

$$= \pi L_{\rm D} \sin^2 \Theta_{\rm cr} + \pi L_{\rm u} (1 - \sin^2 \Theta_{\rm cr})$$
 (8.3)

The upward irradiance E_{u} becomes

$$E_{u} = \int_{0}^{\pi/2} 2\pi L_{u} \sin \Theta \cos \Theta d\Theta = \pi L_{u}$$
(8.4)

and the scalar irradiance E_0 becomes

$$E_{o} = L_{S}d\omega_{S} + \int_{0}^{\theta} 2\pi L_{D}\sin\theta \, d\theta + \int_{0}^{\pi} 2\pi L_{u}\sin\theta \, d\theta$$

$$= L_{S}d\omega_{S} + 2\pi L_{D}(1 - \cos\theta_{cr}) + 2\pi L_{u}(\cos\theta_{cr} + 1) \qquad (8.5)$$
By inserting for L_{v} L and L_{v} from eq. 8.2.8.3 and

By inserting for L_S , L_D and L_u from eq. 8.2, 8.3 and 8.4, eq. 8.5 may be written

$$E_{o} = \frac{E_{S}}{\cos j} + \frac{2}{\sin^{2}\theta_{cr}} (E_{D} - E_{u}(1 - \sin^{2}\theta_{cr}))(1 - \cos\theta_{cr})$$
$$+ 2 E_{u}(\cos\theta_{cr} + 1)$$
(8.6)

With $\theta_{cr} = 48.6^{\circ}$, E_{o} becomes

$$E_{o} = E_{S} \operatorname{sec} j + 1.20 E_{D} + 2.80 E_{u}$$
 (8.7)

We may now return to eq. 2.4 and insert for E_{o}

$$K_{d}E_{d} - K_{u}E_{u} = a(E_{s} \sec j + 1.20(E_{d} - E_{s}) + 2.80 E_{u}$$
 (8.8)

This may be rewritten as

$$K_d E_d (1 - (\frac{K_u}{K_d} + 2.8 \frac{a}{K_d}) \frac{E_u}{E_d}) = a(1.2 E_d + (\text{sec j} - 1.2)E_S)$$
 (8.9)
If we insert the values $K_u/K_d \approx 1$, $a/K_d \approx 0.7$ from
Table 1, eq 8.9 becomes

$$K_{d}E_{d}(1 - (1 + 2.0)R) = a(1.2 E_{d} + (sec j - 1.2)E_{s})$$
 (8.10)
or

$$K_d \approx a(1 + 3R)(1.2 + (sec j - 1.2)r)$$
 (8.11)

Thus the radiance distribution model of LUNDGREN and HØJERSLEV may lead to the same result as in eq. 6.1-3, with one exception: - eq. 6.3 gives sec Θ_D = 1.2 only just beneath the surface.

- 20 -

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-	23	topa -
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TTATT	7
LABUE	1

Depth m	D _d	Du	R %	R %	R _o /R	^K u [/] K _d	a/ _{Kd}
			Clear	sunny	sky, h = 57	,0	
5 10 20 30 40 50 60	1.25 1.28 1.30 1.31 1.32 1.31 1.31	2.70 2.73 2.78 2.78 2.76 2.76 2.86	2.10 1.87 2.10 2.27 2.34 2.34 2.12	4.55 4.00 4.52 4.82 4.90 4.93 4.59	2.16 2.12 2.15 2.12 2.10 2.10 2.10 2.18	0.95 1.06 1.03 1.01 1.02	0.76 0.68 0.69 0.71 0.71
Mean value	1.30	2.77	2.16	4.62	2.13	1.01	0.71
			Over	east sky	$h = 40^{\circ}$		
5 10 20 30 40 50 60	1.29 1.30 1.33 1.33 1.34 1.34 1.34 1.34	2.77 2.79 2.81 2.77 2.79 2.87 2.97	2.19 2.30 2.52 2.65 2.76 2.67 2.50	4.70 4.93 5.34 5.52 5.74 5.72 5.60	2.15 2.14 2.11 2.08 2.08 2.14 2.23	1.05 1.04 1.03 1.00 0.96	0.74 0.69 0.63 0.67 0.72
Mean value	1.32	2.82	2.51	5.36	2.13	1.02	0.69
Total mean	1.31	2.80	2.34	4.99	2.13	1.02	0.70
S _{rel} %	2	2	11	10	2	4	5

The table is inter- and extrapolated from TYLER's observations at 480 nm of D_d , D_u , R, K_d and a in Lake Pend Oreille.

 $R_0, R_0/R$ and K_u/K_d were calculated from

 $\frac{K_{u}}{K_{d}} = 1 + \frac{\ln(R(z_{2})/R(z_{1}))}{(z_{2}-z_{1})K_{d}}$

TABLE	2
TUDUU	4

- 24 -

Y	ΣY ² = min for	B=Baltic Sea M=Mediterranean N= Number of observations
$K-(a_{R}(\sec \Theta_{D} + (\sec j - \sec \Theta_{D})r_{O}e^{-(K_{S}-K)z})$ where $K_{S} = (a + \alpha b) \sec j$	α = 0.72 sec Θ _D = 1.38	B + M N = 39
as above, but sec $\Theta_{D} = \beta - \gamma e^{-(K_{S}-K)z}$	α = 0.86 β 1.41 γ = 0.21	B + M N = 39
K - (a + ε b)D _d	ε = 0.0219	B + M N = 24
R(a + ε b) - 0.5 ε b	ε = 0.0145	B + M N = 24
R - 0.5 eb/a	ε = 0.0166	B + M N = 24
((а + 0.86 b)sec ј — К) — (λа + µb sec ј)	$\lambda = -0.010$ $\mu = 0.734$	B + M N = 24
(a + 0.86 b)sec j - ν K	v = 2.12	M N = 14

K, E_0 , E_d , E_u and a are observed at 477 nm, b is observed at 655 nm (HØJERSLEV 1973, 1974a). By the assumption that scattering by particles is independent of the wavelength, b_{477} can be calculated from

 $b_{477} = b_{655} + (b_{w477} - b_{w655}) = b_{655} + 0.0026 \text{ m}^{-1}$

 b_{W} is the scattering coefficient of pure sea water (MOREL, 1974). FROM eq. 2.4, 2.9 and 2.11 it may be deduced that

$$D_{d} = \frac{1}{1+3R} \frac{E_{o}}{E_{d}-E_{u}}$$

TABLE	3
TUTTT	5

	$a_{R} = 0.015$				a _R = 0.15			
h	ĸo	Klo	^K 20	K	ĸo	Klo	^K 20	K
05 10 15 225 320 450 5605 750 850 90	.0180 .0180 .0186 .0191 .0193 .0192 .0190 .0186 .0182 .0178 .0174 .0170 .0166 .0163 .0161 .0159 .0158 .0156 .0156	.0186 .0189 .0193 .0195 .0194 .0191 .0188 .0184 .0180 .0177 .0174 .0170 .0168 .0165 .0164 .0162 .0162 .0162	.0190 .0193 .0195 .0196 .0195 .0193 .0190 .0187 .0183 .0180 .0177 .0174 .0172 .0171 .0179 .0171 .0169 .0168 .0167	.0185 .0190 .0193 .0195 .0194 .0192 .0188 .0185 .0181 .0177 .0174 .0170 .0168 .0166 .0164 .0163 .0162 .0162	.180 .180 .186 .191 .193 .192 .190 .186 .182 .178 .174 .170 .166 .163 .161 .159 .158 .156 .156	207 208 208 208 207 207 207 206 205 204 204 204 204 204 203 202 201 201 201	.211 .211 .211 .211 .211 .211 .211 .211	.204 .205 .207 .207 .207 .207 .205 .205 .204 .203 .202 .201 .200 .200 .200 .200 .200 .199 .199 .199
				a _R = 1	•5			
		n 0510 1205 220 3405 550 550 50 750 859 90	K 0 1.80 1.80 1.91 1.93 1.92 1.90 1.86 1.82 1.74 1.70 1.66 1.63 1.61 1.57 1.56 1.56	K10 2.11 2.11 2.11 2.11 2.11 2.11 2.11 2.	K20 2.11 2.11 2.11 2.11 2.11 2.11 2.11 2.	K 2.10 2.10 2.11 2.11 2.11 2.11 2.10 2.10		

The vertical attenuation coefficients just beneath the surface and at 10 and 20 meters depth, K_0 , K_{10} and K_{20} , were determined from eq.6.1-6.6 and 6.13 by means of a computer. Although K changes with depth, the same K was used on both sides of eq.6.1. The error introduced in this way was assumed to be of the same order as the other approximations or less.

To obtain an expression for the mean value of K we consider the more simple form

$$K = a_R (1.38 + (sec j - 1.38) r_0 e^{-KZ})$$

which may be written

$$K = A + B e^{-KZ}$$
 ((I)

The mean value in the range 0 - 20 m becomes

$$\overline{K} = \frac{1}{20} \int_{0}^{20} K \, dz \approx A + B \frac{(1 - e^{-20K_{20}})}{20 K_{20}} .$$
(II)

Eq.I gives that

$$K_0 = A + B$$
 (III)

$$K_{20} = A + B e^{-20K_{20}}$$
 (IV)

Insertion from eq.III and IV in II gives

$$\overline{K} \approx \frac{K_{20} - K_0 e^{-20K_{20}}}{1 - e^{-20K_{20}}} + \frac{K_0 - K_{20}}{20 K_{20}}$$



Fig.1. The function r_a for three different water vapour contents, (Data from HIN2PETER 1957).

- 27 -



attenuation coefficients.

- 28 -