

**UNIVERSITY  
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**Exploring Fluid Properties in  
Confined Mineral Interfaces: A  
Molecular Investigation**

– Implications for EOR

**Thesis submitted for the degree of Philosophiae Doctor**

Department of Geosciences  
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*To my beloved ones*



# Preface

As I began my doctoral research journey, I couldn't have imagined the unprecedented challenges that awaited. The onset of the COVID-19 pandemic in early 2020 shattered normalcy, deeply affecting not just daily life but also the trajectory of academic pursuits. Despite this turbulence, my dedication to advancing knowledge stayed unwavering, propelling me to navigate through uncertainties and persist in the pursuit of academic excellence. In the face of adversity, scientists worldwide mobilized their expertise and resources, ultimately delivering life-saving vaccines to combat the devastating effects of the coronavirus. While the loss of some million lives is a tragic reminder of the pandemic's severity, it underscores humanity's remarkable ability to overcome seemingly insurmountable challenges. This sobering lesson drives home the urgency of addressing global warming. Just as the pandemic exposed our vulnerabilities, the looming specter of climate change poses a grave risk to life on Earth. However, inspired by the resilience and collaboration witnessed in the fight against COVID-19, we embark on a new mission to confront the existential threat of climate change. In this endeavor, I hope that the findings of this Ph.D. project will make a meaningful contribution, fostering a brighter and more sustainable future for generations to come.

This dissertation is submitted to the Department of Geosciences of the Faculty of Mathematics and Natural Sciences, University of Oslo (UiO) in accordance with the requirements for the degree of *Philosophiae Doctor* (PhD). The candidate has been employed as a Ph.D. research fellow at this institution, with funding provided by the University of Oslo. Professor Helge Hellevang served as the main supervisor, with Associate Professor Rohaldin Miri providing co-supervision. Additionally, Professor Francois Renard contributed to scientific discussions, reviewed results, and provided feedback on the research.

This Ph.D. dissertation collects and summarizes the candidate's research findings, presented in accordance with the University's Manuscript Document Format. This thesis has focused on understanding fluid thermodynamics at confined mineral interfaces by simulating the rock-fluid interface at the nanoscale using first principle molecular dynamics technique. The present manuscript is organized into five main chapters:

- **Chapter 1** (Introduction) provides a framework for the coherence and scientific motivation of the dissertation, as well as identifying scientific questions.

- **Chapter 2** (Theoretical background) presents an overview of the theoretical foundation of the research.
- **Chapter 3** (Summary of papers and outlook for future works) summarizes the key findings and provides future directions for further investigations.
- **Chapter 4** (Journal papers) introduces three peer-reviewed published papers in which the candidate is the first author.
- **Chapter 5** (Appendices) provides summaries of conference proceedings and extended abstracts in which the candidate is the first author.

**Sajjad Ahmadigoltapeh**

Oslo, May 2024

# Summary

Contact between rocks and fluids is ubiquitous in nature, observed in oceans, coastal boundaries, river banks, subsurface geological repositories, etc. Rocks are mostly made up of crystalline materials, known as minerals, which possess a periodic structure. The structural geometry of the constituent minerals determines the physical and chemical properties of the rocks. Among the organic and inorganic fluids that are in contact with rocks in nature, water is the dominant fluid playing the role of solvent in most cases. The rock-water interface is important because it does not only impacts processes like dissolution and precipitation but also serves as the location of interactions between the solid surface and the liquid phase. In addition to water molecules, the presence of other dissolved components, e.g., organic compounds, inorganic molecules, ions, and gases such as  $\text{CO}_2$  affect the interface properties. On the one hand, these components interact with each other. On the other hand, they interact with the rock surface. The fluid-rock interaction influences the characteristics of the fluid entrapped at the boundary layer, causing the physical properties and phase behavior of the fluid to differ considerably from the equivalent bulk phase. The boundary layer, in this context, refers to a layer that is directly in contact with the rock surface. Regardless of whether the bulk fluid is in turbulent motion or not, the attraction forces between the rock surface and the fluid molecules restrict the fluid velocity to zero, resulting in the so-called noslip condition.

Although it has long been acknowledged that the solid mineral affects the fluid thermodynamic properties at the fluid-solid interface, the underlying mechanism of fluid-solid interactions still is inaccessible because of (i) limitations of the experimental technique and (ii) integration of experimental observations across relevant time scales. From a microscopic perspective, when the confinement size decreases and approaches the molecular dimension, which is comparable to the mean free path, the free thermal motion of fluid molecules is interrupted, resulting in diverse and unique thermodynamic properties. Therefore, it is critical to enhance our understanding of molecular aspects of fluid-solid interactions by employing a reliable approach. The first-principal molecular dynamics (MD) simulation is a trustworthy technique that can be utilized to study molecular aspects of fluid-rock interactions. Due to the developments in hardware (CPU and GPU) technology, the execution of MD computational algorithms has been shortened in terms of time. However, choosing large dimensions for the simulation box extends run-time, which means that the computational cost impact remains a challenge.

In this Ph.D. dissertation, the first-principal molecular dynamics simulation technique was utilized to capture the interaction between fluid molecules and the solid mineral surface. Furthermore, statistical associating fluid theory (SAFT) is

employed to model the complex thermodynamics of interfaces and incorporate the mineral effect into the fluid physicochemical properties confined in the nanopore. To be specific, the effort of this dissertation was to find answers for these key questions: (1) How to capture the above-mentioned deviations in fluid properties on the nanoscale? (2) How do we survey these deviations on the bulk scale? (3) How does the change in fluid chemistry affect the behavior of the mineral surface?

The above inquiries have been addressed through three distinct studies:

1. An investigation into the interface of pure water and calcite utilizing molecular dynamics simulation, alongside modelling the governing thermodynamics of the water-calcite interface with Perturbed Chain-Statistical Association Fluid Theory (PC-SAFT) equation of state.
2. An exploration of the properties of confined water sandwiched within a calcite nanopore, as well as modeling the dominant thermodynamics with the equation of state inspired by Statistical Association Fluid Theory (SAFT) .
3. The molecular dynamics simulation was used to examine the interface of low-saline water and calcite mineral with the aim of probing oil replacement dynamics and the behavior of various ions.

The methodology described and the subsequent outcomes of these basic studies can be applied in various fields of study. These applications include catalysis, contaminant transport, the effect of mineral grain size on chemical weathering, the effect of solid surfaces on limiting mineralization in oceans, the mechanisms by which microbes facilitate exchange between solid particles and solution, estimating solubility limits in multicomponent fluid processing, the mechanism of CO<sub>2</sub> exchange with sea water, enhanced oil recovery (EOR), subsurface CO<sub>2</sub> storage and more.



# Sammendrag

Kontakt mellom bergarter og fluider i naturen foregår i sjøer, kystgrenser, elvebredder, underjordiske geologiske depoter, osv. Bergarter består for det meste av krystallinske materialer med periodiske strukturer, kjent som mineraler. Den strukturelle sammensetningen av mineraler i bergarter bestemmer deres fysiske og kjemiske egenskaper. Blandt de organiske og ikke-organiske fluider som er i kontakt med bergarter i naturen er vann et dominerende medium, og som oftest fungerer vannet som et løsemiddel. Grenseflaten mellom bergarter og fluider er viktig siden den ikke bare påvirker reaksjoner som oppløsning og utfelling, men også fungerer som stedet hvor alle interaksjoner mellom faste overflater og væsker foregår. I tillegg til vannmolekyler påvirker også tilstedeværelsen av andre oppløste komponenter, for eksempel organiske forbindelser, uorganiske molekyler, ioner, gasser som  $\text{CO}_2$ , grenseflateegenskapene. Dette skjer fordi disse komponentene på den ene siden påvirker hverandre samtidig som de på den andre siden interagerer med overflaten. Fluid-bergart interaksjoner påvirker egenskapene til fluider som er fanget i grensesjiktet. Dette gjør at de fysiske egenskapene og faseoppførselen til fluiden skiller seg fra den tilsvarende bulkfasen. Grensesjiktet i denne konteksten refererer til et lag som er i direkte kontakt med overflaten. Uavhengig av om fluiden er i turbulent bevegelse eller ei vil de tiltrekkende kreftene mellom overflaten og fluidmolekylene begrense fluidens hastighet til null, hvilket resulterer i den såkalte "noslip" tilstanden.

Selv om det lenge har vært kjent at mineraler påvirker en fluids termodynamiske egenskaper ved grenseflaten, er de underliggende mekanismene til fluid-fast-stoff-interaksjoner fortsatt ikke godt forstått på grunn av (i) begrensninger i eksperimentelle teknikker og (ii) integrasjon av eksperimentelle observasjoner over relevante tidsskalaer. Fra et mikroskopisk perspektiv, når størrelsen på et porerom reduseres og nærmer seg molekylære størrelser som er sammenlignbare med midlere fri veilengde (*mean free path*), blir de frie termodynamiske bevegelsene til fluidmolekylene begrenset, noe som resulterer i unike termodynamiske egenskaper. Det er derfor kritisk å fremme vår forståelse av molekylære aspekter ved fluid-fast-stoff-interaksjoner ved å ta i bruk en robust vitenskapelig tilnærming. Molekylærdynamiske (MD) simuleringer er en slik teknikk som kan brukes for å studere molekylære aspekter ved fluid-stein interaksjoner. Takket være utviklingen i data-teknologi (CPU og GPU) tar kjøringen av MD beregnings-algoritmer mindre tid. Likevel er det fortsatt utfordringer relatert til begrensninger i tilgjengelig beregningstid og for store simuleringer på grunn av de tunge beregningene.

I denne doktorgradsavhandlingen ble molekylærdynamikksimulering benyttet for å forstå interaksjonen mellom fluid-molekyler og en mineraloverflate. Videre ble statistical associating fluid theory (SAFT) brukt til å modellere den komplekse

termodynamikkene ved grensesnitt og inkorporere effekter av mineraloverflaten på de fysikokjemiske egenskapene til vann som var innesluttet i en nanopore. Det spesifikke formålet med avhandlingen var å finne svar på følgende nøkkelspørsmål: (1) Hvordan beregne de nevnte avvikene i fluidegenskaper på nanoskala? (2) Hvordan undersøker vi disse avvikene på bulk-skala? (3) Hvordan påvirker endringen i fluidkjemi tilstanden til mineraloverflaten?

De nevnte spørsmålene har i neste steg blitt besvart i tre studier:

1. Undersøke grensesjiktet til rent vann og kalsitt med MD simulasjoner og modellere termodynamikken til vann-kalsitt-grenseflaten med PC-SAFT tilstandsligninger.
2. Undersøke egenskapene til vann innestengt i en nanopore med kalsitt på begge sider ved å bruke MD-simuleringer, og simulere den termodynamikken med SAFT2 tilstandsligninger.
3. Bruke MD for å simulere grenseflaten til urent vann og kalsittmineraler, og undersøke dynamikken til de ulike komponentene.

Metoden og de påfølgende resultatene av disse grunnleggende studiene kan anvendes innen ulike fagfelt. Disse inkluderer katalyse, transport av forurensninger, effekten av mineralstørrelse på kjemisk forvitring, effekten av faste overflater på begrensning av mineralisering i havet, mekanismer der mikrober katalyserer utveksling mellom faste partikler og løsning, estimering av løselighetsgrenser i flerkomponent fluidbehandling, mekanismen for CO<sub>2</sub>-utveksling med sjøvann, økt oljeutvinning (EOR), lagring av CO<sub>2</sub> under bakken, osv.

# Acknowledgements

First, I extend my heartfelt gratitude to my supervisors, Professor Helge Hellevang and Associate Professor Rohaldin Miri, for their invaluable motivation, support, and expertise. Dear Helge, your enthusiasm and dedication to scientific research have been truly inspiring, helping me to develop confidence and independence as a researcher. Dear Rohaldin, I am immensely grateful for your availability whenever I needed help, your unwavering support, and your prompt responses even on weekends.

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Throughout my time at the University of Oslo, it has been a privilege to be a member of the esteemed Department of Geosciences, where I have had the opportunity to apply my computational skills to the study of geological systems. I would like to thank all members of the department for fostering a positive atmosphere, offering generous support, and maintaining ongoing camaraderie. Special thanks to Professor Bernd Etzelmuller, Professor Valerie Maupin, Professor Emeritus Per Aagaard, Professor Jens Jahren, and Professor Nazmul Haque Mondol for their guidance and advice.

Endless gratitude for the companionship of my skilled and cheerful colleagues and office mates: Payman, Irfan, Clara, and Beyene. During my Ph.D. journey, I had the pleasure of collaborating with two brilliant friends Saeed and Jamluir, whose contributions greatly enriched my research. In particular, Jamilur, your unwavering support and determination have turned the seemingly impossible into reality.

I extend special thanks to my entire family, especially my parents, for their unwavering encouragement over the years. My wife deserves particular recognition for her patience and companionship. Her steadfast belief in me and enduring support have been crucial in helping me navigate the challenges and complexities of my academic journey. Last but certainly not least, I am deeply thankful for my little daughter. Though it has been a short time since you came into our lives, your love has been a constant source of strength and motivation, propelling me forward.

**Sajjad Ahmadigoltapeh**  
Oslo, May 2024



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## Paper I

Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Rohaldin Miri and Helge Hellevang. “Extension of PC-SAFT equation of state to include mineral surface effect in fluid properties using molecular dynamics simulation”. In: *Sustainable Energy Technologies and Assessments*. Vol. 48, (2021), pp. 101624.  
DOI: <https://doi.org/10.1016/j.seta.2021.101624>.

## Paper II

Sajjad Ahmadi Goltapeh, Rohaldin Miri, Per Aagaard and Helge Hellevang. “Extension of SAFT Equation of State for Fluids Confined in Nano-pores of Sedimentary Rocks Using Molecular Dynamics Simulation”. In: *Journal of Molecular Liquids*. Vol. 348, (2022), pp. 118045.  
DOI: <https://doi.org/10.1016/j.molliq.2021.118045>.

## Paper III

Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Jens Sigurd Jahren, Rohaldin Miri and Helge Hellevang. “Drivers of Low Salinity Effect in Carbonate Reservoirs Using Molecular Dynamics Simulation”. In: *Journal of Molecular Liquids*. Vol. 360, (2022), pp. 119490.  
DOI: <https://doi.org/10.1016/j.molliq.2022.119490>.



# Conference proceedings

**A:** Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Rohaldin Miri and Helge Hellevang. “Extension of SAFT equation of state to include calcite wall effect in water properties within water-calcite interface using molecular dynamic simulations.” In: *InterPore 13<sup>th</sup> Annual Meeting, 31May - 4June 2021*.

**B:** Sajjad Ahmadigoltapeh, Rohaldin Miri, Per Aagaard, Helge Hellevang. “Extension of the SAFT equation of state to capture the effect of the solid wall into the confined fluid properties: using molecular dynamic simulation.” In: *InterPore 14<sup>th</sup> Annual Meeting, 30May - 2June 2022*.

**C:** Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Rohaldin Miri and Helge Hellevang. “Mineral-Fluid Interface Properties: A Molecular Dynamic Study.” In: *83<sup>th</sup> EAGE Annual Conference & Exhibition, 6-9 June 2022, Madrid, Spain*. DOI: <https://doi.org/10.3997/2214-4609.202210013>.

**D:** Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Rohaldin Miri and Helge Hellevang. “Low Salinity Water Impact on the Calcite-Water Interface: A Molecular Dynamic Study.” In: *Geoconvention Conference, 20-22 June 2022, Calgary, Canada*. <https://geoconvention.com>





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# Chapter 1

## Introduction

To efficiently utilize our planet's resources located in the subsurface and effectively tackle environmental challenges, a deep understanding of the interactions between minerals and fluids is required. Imagine a future where one could efficiently remove contamination from water resources and soils [1, 2], precisely estimate water capacities in groundwater aquifers [3, 4], cost-effectively develop geological hydrogen storage [5–7], rapidly advance geological CO<sub>2</sub> storage [8, 9], accurately predict the behavior of petroleum fluids [10, 11] and thoroughly understand the geological factors influencing the enhancement of oil recovery [12, 13]. These challenges may appear complex and all involve processes at the mineral-fluid interface. Understanding these processes is critical to paving the way for a more eco-friendly and greener future.

### 1.1 Carbonate minerals

Carbonates are the most abundant minerals found in Earth's sedimentary layers [14]. They have a long history of construction, dating back to their use during the Roman Empire [15]. Often, children interact with calcium carbonate for the first time at school, where it is used to write on chalkboards, as chalk is composed of fine microcrystalline calcite particles [16]. Prehistoric paintings found in limestone caves reveal that humans from ancient times carved information onto limestone slabs [17]. The discovery of inscriptions (cuneiform texts) on limestone such as the Kish tablet [18] highlights the long-standing use of limestone as a writing tool for ancient civilizations [19, 20].

#### 1.1.1 Calcium carbonate in marine organisms

Calcium carbonate is not limited to the Earth's crust, it is a key component in marine animals, including mollusks, invertebrates (corals, seashells), and even vertebrates, such as fish, which utilize biogenic calcium carbonate [21–23]. Combining organic molecules with biogenic calcium carbonate gives unique advantages to marine organisms, including precise control over the morphology of biogenic crystals of calcite or aragonite [24–26]. Coccolithophores, for example, demonstrate the ability to control the growth of calcite shells in seawater through biomineralization [27]. Marine organisms utilize calcite to grow skeletons and exoskeletons, which exhibit stronger mechanical strength compared to non-biogenic ones [28, 29]. The improved strength is attributed to the incorporation of amino acids into their structure [30]. Furthermore, the hierarchical structure of these biominerals plays a significant role in their overall hardness, enhancing their ability to tolerate external pressure [31]. This mechanical strength makes

## 1. Introduction

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biogenic calcium carbonate an excellent choice for the development of composites with improved stiffness [32, 33].

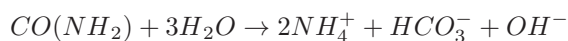
### 1.1.2 Calcium carbonate in medicine

Another example of the versatility of calcite can be seen in its numerous applications in the field of medicine. Calcite is used for applications such as the development of synthetic bones and the treatment of bone defects [34, 35]. Its suitability is attributed to a range of valuable properties, including its antibacterial activity [36], biocompatibility [37, 38], bioinductivity [39] and non-toxicity [40]. Furthermore, due to slow degradation and sensitivity to pH, calcite can function as a controlled release agent, ensuring that drugs remain at targeted sites in the body for longer periods after administration [41]. It is worth noting that its history in dentistry dates back more than a century, when calcium carbonate was used as filling materials to seal root perforation [42].

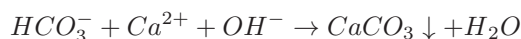
### 1.1.3 Calcium carbonate in industrial applications

Calcite has attracted interest in various industrial applications due to its natural abundance and low production cost. Some notable applications of calcite include, but are not limited to, environmental utilization, surfactants, paint manufacturing, paper production, fire extinguisher formulation, adhesives, household cleaning products, food coloring, and cosmetics [43–45]. Ordinary concrete, for example, is highly valued in the construction industry due to its compressive strength [46]. In cement limestone production, mainly composed of calcite, limestone is used as a permitted and essential additive [47]. When water is added to cement, it initiates a chemical reaction (cement hydration), resulting in the formation of a C-S-H paste. This paste hardens and reinforces the strength of hydrated cement [48]. Recent progress in nanotechnology has opened up new possibilities for the modification of cement-based materials on the nanoscale [49]. To be specific, the mechanical [50] and chemical adjustments [51] of cement on a nanoscale enable the generation of cement composites with improved properties and functionalities [52].

In addition, in alignment with global efforts to reduce greenhouse gas emissions, interest in environmentally friendly green cement has increased. One novel approach for green cement production involves the use of the microbiologically induced calcium carbonate precipitation (MICP) technique [53], employing the biomineralization reaction of  $\text{CaCO}_3$ . This process begins with the hydrolysis of urea catalyzed by urease, leading to an increase in pH through the following reaction [54]:



then, produced bicarbonate ions together with calcium ions  $\text{Ca}^{2+}$  will induce calcium carbonate precipitation:



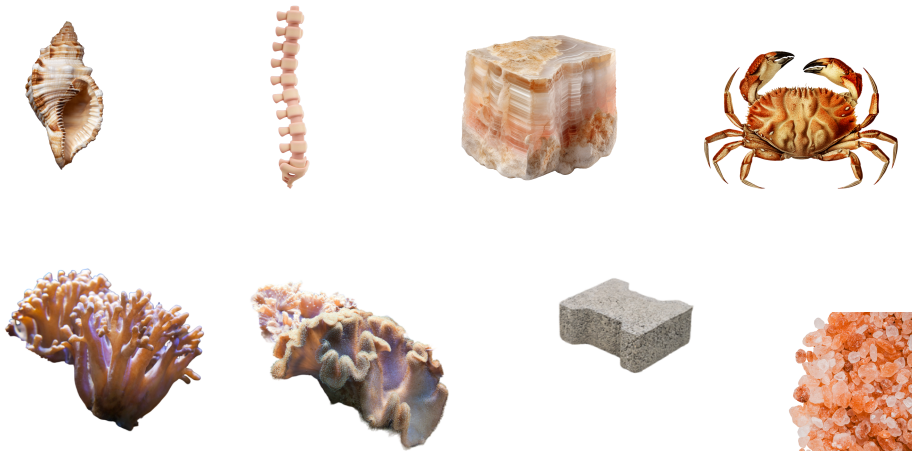


Figure 1.1: Some typical forms of calcite in nature, from left to right, top row: seashell, human spine bone, calcite crystal, crab shell. Bottom row: coral, molluscs, marble, and aragonite crystals. (images:freepik.com)

The urease enzyme, which is present in bacteria, plants and some invertebrates, plays an essential role in this process [55]. It is important to note that alternative materials, such as coal ash and slag from the blast furnace [56], as well as food wastes [57] can serve as the main components in the production of green cement. Green cement has a significant advantage due to its lower  $\text{CO}_2$  emission rate compared to the conventional method, because it eliminates the need for a high-temperature calcination step in cement production [58]. In addition to its environmental benefits, green cement technology provides an opportunity to utilize waste streams [59, 60].

## 1.2 Carbonate reservoirs

In sedimentary basins, two main types of reservoir rocks can be defined: sandstone sequences [61] and carbonate sequences [62]. The former are mainly composed of quartz and other detritic minerals, and the latter are mainly composed of carbonate minerals, such as calcite and dolomite [63]. Carbonate rocks are formed through the accumulation and cementation of organic remains on the seabed [64]. These rocks have a porous structure that allows them to store a significant amount of fluid. They may host important groundwater aquifers and promising sites for  $\text{CO}_2$  storage because of available storage capacity and geological integrity when covered by low-permeability caprocks [65, 66]. In addition, carbonate rocks are recognized as reservoirs for significant petroleum deposits. In fact, calcite is the major component of more than 50% of the world's oil reservoirs [67, 68]. In particular, the Middle East region is characterized

by its huge carbonate fields, housing around 70% oil and 90% gas reservoirs [69, 70]. In the North Sea, the Ekofisk field is another example of a reservoir characterized by high porosity and low permeability that has been in continuous production since 1987 [71].

### 1.3 Carbonate rock and aqueous phase interactions

In subsurface carbonate reservoirs, the interactions between calcite grains and aqueous phases are crucial. These interactions occur at the calcite-fluid interface, where water serves as the primary solvent [72]. To initiate a chemical reaction, it is essential for ions to attach to the calcite surface, necessitating the displacement of adsorbed water molecules. In other words, to make room for ions to interact with the calcite surface, water molecules that were previously attached to the calcite surface must be pushed away [73–75]. Therefore, water interactions with the surface of the calcite are an important part of any chemical reaction [76–78].

In general, interpreting the interactions between calcite rock and water is a complex task due to the diverse phenomena observed at mineral-fluid interfaces [79]. Each of the observed phenomena is potentially governed by distinct mechanisms, making it challenging. For instance, water weakening, a frequently reported phenomenon in carbonate reservoirs, occurs as a result of interactions between the calcite and aqueous phase. Basically, water injection into the oil reservoir is performed to compensate for the pore pressure (ensuring that the crude oil remains above the bubble point) and improves the sweeping efficiency [80, 81]. However, interactions between calcite and water for long periods can affect the mechanical strength of the reservoir and lead to compaction and subsidence [82, 83]. Studies have shown that various factors such as surface energy [84] and the physicochemical properties of water [85] contribute to water weakening, finally leading to the deformation of carbonate rocks [86–89].

Another well-documented phenomenon in subsurface carbonate reservoirs is wettability alteration of carbonate rocks. The surface of calcite is naturally hydrophilic, namely it has an inherent tendency to adsorb water [90]. This is due to the positive electrostatic charges present on the calcite surface that attract water molecules, resulting in a water-wet surface [91]. However, in subsurface reservoirs, calcite exhibits moderate to strongly oil-wet behavior [92]. Wettability alteration in calcite occurs because of its interaction with hydrocarbon fluid at the calcite-fluid aqueous interface. This interaction results in the adsorption of polar compounds such as carboxylic acids and asphaltenes contained in crude oil [93] leading to the oil-wet surface property of calcite.

The examples mentioned above represent only a few instances among many, providing insights into colloidal interactions at the calcite-water interface in subsurface reservoirs. This complexity makes it a challenging but interesting field of study. One significant challenge that will be the central focus of this Ph.D. dissertation arises at the interface where calcite and water come into contact. At this nanoscale proximity, the behavior of water differs from its behavior in bulk scale. Indeed, when two opposing surfaces of calcite and water become very

close on a nanoscale level, the characteristics of water are affected and deviate from what is typically observed in bulk water.

## 1.4 Water properties confined in mineral domains

Mineral-induced changes in the physicochemical properties of fluid occur at confined mineral interfaces where a nanometer thick water layer interacts with the mineral surface. Understanding the underlying mechanisms of mineral-fluid interactions plays a crucial role in various fundamental and practical areas, ranging from surface science to materials science [94, 95]. In recent years, scientists have utilized diverse methodologies to accurately predict and determine the phase behavior and thermodynamic properties of fluids confined within restrictive nanoscale cavities [96, 97]. These cavities typically have dimensions ranging from 1 to 10 nm, imposing significant limitations on the fluid's behavior. For example, in a comprehensive investigation, Knight et al.[98] sought to understand the effects of nanoscale confinement on water properties. By combining experimental analyses and observations, they successfully demonstrated that mineral confinement at the nanoscale induces significant alterations in the physical properties of water. They observed a decrease in the melting and freezing point temperature of confined water as the spatial confinement level increased. Furthermore, they observed notable changes in the hydrogen-bonding network within the confined water.

Studying the unique physical and chemical properties exhibited by confined water under mineral confinement requires advanced empirical techniques for molecular scale investigations. An interesting area of study is the behavior of pure water at confined mineral interfaces. In pioneering studies, Salmeron and co-workers [99, 100] applied polarized force between the tip of atomic force microscopy and the solid mineral to investigate the condensation and evaporation processes of water. They found a relation between environmental humidity and formation of water monolayers on the mica surface. Their observations showed that when humidity remains below 25% a thin water film over mica surface grew to a thickness of several angstroms. However, for humidity over 25%, they reported the formation of a second layer of water, leading to the creation of large islands with distinct geometrical shapes [101]. In another study Wu et al.[102] used a nuclear magnetic resonance instrument to investigate how water behaves in calcite and silica pores. Their findings showed that the water molecules trapped within the calcite pores exhibited higher activity compared to those in the silica pores. This discrepancy can be attributed to the different kinds of hydroxyl groups at calcite and silica surfaces, leading to variations in the distribution of water molecules within the pores, resulting in higher activity for water in contact with calcite pore.

### 1.4.1 Aqueous phases confined at mineral interface

Expanding our understanding of mineral-fluid interactions, some studies have explored the behavior of aqueous phases confined at mineral interfaces. For

## 1. Introduction

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example, Ruiz and Putnis [103, 104] revealed that the rate of calcite dissolution in a water environment is influenced by the type and concentration of the electrolyte solution. This influence is explained by changes in the dynamics of water structure, particularly the alteration of the activation energy barrier for breaking water-water interactions. In a related study, Li et al. [105] investigated the growth of calcite crystals under conditions involving confinement near an aqueous phase. They identified two common types of confined growth: smooth and rough, which are not unique to calcite, but a general consequence of confinement.

Guren et al. [106] investigated the remediation potential of the calcite mineral for contaminated water resources. They utilized atomic force microscopy to investigate dissolution-precipitation processes in nanoslab calcite exposed to an aqueous phase enriched with chromium ions. They observed that chromium ions were trapped within the nanopores of the calcite surface, formed as a result of dissolution-precipitation mechanisms. The precipitated chromium carbonate established a passive layer on the calcite surface, effectively preventing further dissolution of the calcite. To this end, Julia et al. [107] investigated the efficiency of the carbonate rock surface in sequestering cadmium from contaminated water. Their findings revealed that the presence of a calcite surface facilitated cadmium precipitation from aqueous phase by a coupled dissolution-precipitation process.

Dziadkowiec et al. [108] highlighted how the composition of the aqueous phase and the hydration characteristics govern the thickness of the surface-adsorbed water layers on calcite. They studied the adhesive forces between two cleaved (10 $\bar{1}$ 4) calcite surfaces submerged in aqueous solutions with atomic force microscopy. They found altering the Ca<sup>2+</sup> content in aqueous phase had a limited impact on the adhesive forces between calcite pore-walls. However, Ca<sup>2+</sup> ions have stronger effect on adhesion, compared with Na<sup>+</sup> ions. Furthermore, strongly hydrated ions like Ca<sup>2+</sup> supported thicker water film on the calcite surface compared to Na<sup>+</sup>.

### 1.4.2 Experimental methods and relevant limitations

Despite numerous efforts, directly visualizing the mineral-water interface and measuring its physicochemical properties remains a challenge. This challenge stems primarily from limitations in experimental techniques. For example, the dynamic nature of the water film adhered to the mineral surface often requires experiments to be conducted under ultra-high vacuum conditions and cryogenic temperatures [109, 110]. Additionally, experiments with atomic force microscopy may lead to the formation of an ice structure due to the application of local pressure [111]. There are challenges in completely isolating water films when using the electron spectroscopy technique [112], and the water film on the mineral surface may be perturbed by scanning tunneling microscopy tip, causing the water molecules to move and form a cluster [113]. Alternatively, semi-empirical models such as Langmuir [114], Freundlich [115], and Brunauer-Emmett-Teller (BET) [116] adsorption methods may be used to determine the local properties of the fluid confined within a nanopore. These approaches are nevertheless incapable of capturing phase transitions. The time costs, non-repeatability, and



operational constraints (i.e., temperature and pressure) make it difficult for the mentioned empirical and semi-empirical methods to accurately forecast the confined fluid properties.

### 1.4.3 Computational techniques and relevant challenges

In the exploration of atomic-scale complexities related to mineral-fluid interfaces, computational techniques such as Density Functional Theory (DFT) and Molecular Dynamics (MD) have gained popularity as viable alternatives to direct empirical measurements and observations [117, 118]. These methods offer a comprehensive understanding of the underlying phenomena at the molecular level, offering valuable insights into the behavior of fluids confined within mineral nano-structures. DFT is a computational technique rooted in the principles of quantum mechanics that explicitly incorporates electron interactions, allowing the modeling of reaction mechanisms between calcite, oil, and brine water. Nevertheless, the complexity of composition and structure in most minerals, along with the numerous interactions involved in the mineral-fluid interface, often makes the use of DFT methods impractical due to their limited time- and length-scales. However, molecular dynamics (MD) simulations offer a reliable alternative to investigate the fluid properties at the solid-fluid interface. In molecular dynamics simulations, atoms are treated as spheres bonded to one another through a set of springs. This simplified approach, compared to DFT, enables simulations with significantly larger time- and length-scales [119].

The primary limitation of classical molecular dynamics (MD) simulations lies in their inability to capture bond breaking and formation, thereby hindering the modeling of chemical reactions without specialized parameter sets. Despite this drawback, classical MD simulations are gaining prominence as a crucial technique for investigating mineral-fluid interfaces, thanks to their capability to elucidate physical processes at the molecular level [120–122].

### 1.4.4 Exploring mineral-water interfaces with molecular dynamics

Using molecular dynamic simulations, de Leeuw and co-workers [123] reported that the physisorption of water molecules on the  $10\bar{1}4$  cleavage plane of calcite is favorable in terms of energy. Then, in a separate study, Kerisit and Parker [124] calculated the adsorption free energy of water on the  $10\bar{1}4$  calcite surface and demonstrated a reduction in water diffusion near the calcite surface. Rahaman et al. [125] simulated the calcite-water interface using molecular dynamics. They studied different humidity conditions in simulation domains to study the formation of interfacial liquid water on the  $10\bar{1}4$  surface of calcite. The results demonstrated that the mobility of water molecules increases when humidity remains high. In simpler terms, under low humidity conditions, water molecules strongly stick to the calcite surface, indicating that the water molecules occupied well-defined sites at the calcite surface. Furthermore, they reported that the water molecules exhibited higher mobility along the calcite surface compared to

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the perpendicular motion, which required substantial initial forces to overcome the steep barrier.

To better understand the interaction of water molecules with different sites on the calcite surface, Wolthers et al.[126] used molecular dynamic simulations. They chose  $10\bar{1}4$  surface of calcite, including the etch pit and growth island as the mineral surface. Simulations revealed that calcium ions on the mineral surface may adsorb up to three water molecules, depending on their surface position (face, edge, or corner). Additionally, carbonate groups on the mineral surface can interact with water molecules through all oxygen atoms, depending on whether they were located on a face, an edge, or a corner of the calcite lattice. This study concluded that the topography of the calcite surface determines its reactivity. In their computational experiment, Brekke-Svaland and Bresme[127] simulated the  $10\bar{1}4$  surface of calcite and the 001 surface of aragonite at a nanometer distance submerged in water using Large Atomic/Molecular Massively Parallel Simulator (LAMMPS) [128]. They quantified how the mineral-mineral interactions depend on the topography of the mineral surface structure of the adsorbed water on the mineral surface.

Regarding the behavior of organic and inorganic fluids dissolved in aqueous phases, Zhang [129] et al. studied the characteristics of oil and water within a calcite nanopore by analyzing the volumetric flow flux, the velocity profiles of water and oil, and the molecular configurations in the layers of oil and water. They observed that water tends to accumulate on the calcite surface as a result of the hydrophilic nature of this mineral, leading to specific flow phenomena. They reported that at low oil percentages, a slug flow regime is observed, characterized by the formation of a water bridge in the middle of the pore. As the oil content increases, a layered structure of water-oil-water forms, leading to a laminar flow regime. Ultimately, the transition from slug flow to laminar flow results in a significant decrease in the total volumetric flux.

Sedghi [130] et al. conducted a series of MD simulations to investigate the effect of pore-fluid interactions on threshold capillary pressures during crude oil-water brine displacements in angular calcite nanopores. To create realistic models of typical black crude oils, mixtures of various polar and nonpolar oil molecules were considered. Simulations examined the interfacial tension and contact angle under different oil compositions, brine compositions, as well as temperature and pressure conditions. The trends observed in the simulations revealed that the addition of polar components in crude oil led to a decrease in interfacial tension while increasing the contact angle, while the calcite surface remained strongly water-wet. Conversely, the salinity of the water had a negligible effect on contact angle but increased the interfacial tension. They introduced a novel effective theory that incorporates a slip boundary into the Navier-Stokes equation, providing a robust framework for describing the flow behavior of mixtures in nanoscale channels. Through rigorous validation, the authors demonstrated the efficiency of their theory in accurately capturing and describing the complex mixture flow phenomena that occur in nanoscale channels.

## 1.5 Motivation of the thesis

Contact between rocks and fluids is ubiquitous in nature, observed in oceans, coastal boundaries, river banks, subsurface geological repositories, and many other geological settings. Among the organic and inorganic fluids that are in contact with rocks in nature, water is the dominant fluid playing the role of solvent.

While conventional prospective in geochemistry defines thermodynamic properties of fluids at bulk scale, real interactions often occur at the confined interfaces between minerals and aqueous phases. For example, functionalized mineral-fluid interfaces offer effective solutions for waste water treatment [131, 132] and soil contamination remediation [133]. Although bulk water at atmospheric pressure solidifies within a phase at 273K, it has been shown that water confined between graphene sheets experiences different ice phases [134]. Moreover, empirical investigations showed that the adjustment of nanoscale features at the mineral-liquid interface controls the storage capacity of shale type reservoirs [135].

The phase behavior and thermodynamic properties of fluids confined within nanopore minerals deviate significantly from that observed in bulk scale. From a microscopic perspective, at the rock-fluid interface, rock and fluid molecular structures are related but not identical to the bulk structure. This implies that neither the mineral nor the fluid is similar to the bulk counterparts. For minerals, surface characteristics such as dangling bonds [136, 137], defects [138, 139], surface topology [140], among others, play a significant role. In fluids, the free thermal motion of fluid molecules is interrupted as the size of mineral confinement decreases and approaches the molecular dimensions, resulting in diverse and unique thermodynamic properties. Therefore, it is imperative to develop a deeper understanding of how mineral confinement influences the properties of confined fluids, including water and crude oil. This Ph.D. thesis aims to develop a method to investigate how the properties of confined water within calcite nanopores deviate from bulk water, as understanding of these deviations is crucial for developing accurate reservoir models that impact hydrocarbon recovery from subsurface carbonate rocks.

## 1.6 Objectives

In this Ph.D. dissertation, I employed statistical associating fluid theory (SAFT) to model the complex thermodynamics of the calcite-water interface at nanoscale level. Within this framework, I developed an equation of state (EoS) that calculates the properties of water confined near a calcite surface. To account for the impact of the calcite surface on confined fluid properties, a new formulation was derived for Helmholtz free energy and incorporated into the Helmholtz summation of SAFT. This newly defined Helmholtz equation describes the properties of confined fluid as a function of the calcite nanopore characteristics. In order to determine the newly defined Helmholtz free energy species, one needs

to calculate the confinement parameters and local properties in advance. To achieve this, I utilized first-principal molecular dynamics simulations to capture the interactions between water molecules and the calcite surface. I used the open source code Large-scale Atomic/Molecular Massively Parallel Simulator [128] (LAMMPS). To build the calcite-water interface, I chose the neutral surface of calcite, specifically the plane  $10\bar{1}4$ , to mimic the solid mineral surface at the nanoscale. To start, I used pure water as the interacting fluid and then introduced mono- or divalent ions to establish a more realistic system.

Numerous studies have examined the interactions between calcite and water, yet, to my knowledge, none have introduced a robust theoretical method to assess macroscopic changes resulting from microscopic interactions. To that end, the development of an equation of state is essential to accurately quantify the macroscopic properties of water influenced by the presence of the calcite surface on the pore scale (nanoscale). This EoS will also serve as a tool to predict the thermodynamical behaviour of confined water under different temperature and pressure conditions. The following chapter will introduce key thermodynamic concepts and quantities to build such an EoS. To approach this problem, a few key questions need to be addressed:

(i)-How can we link the complex interactions at microscopic level to the observable properties of the system at macroscopic scale?

The first step is to identify a theoretical method that can effectively translate the microscopic interactions of fluid molecules at the nanoscale into macroscopic properties. This involves modeling two fundamental types of molecular interactions near the calcite surface, namely, water-water and calcite-water interactions. To do this, I adopted a molecular-based equation of state inspired by SAFT. SAFT was chosen because of its proven ability to model strong intermolecular interactions within fluid molecules, such as hydrogen bonding between water molecules. This is in contrast to cubic EoS, which are mainly designed to model weak intermolecular interactions such as van der Waals forces. SAFT also has the potential to accommodate non-homogeneous interactions between calcite and water, a challenge that conventional cubic EoS often struggle with.

(ii)-How does the Statistical Associating Fluid Theory (SAFT) contribute to model complex interactions?

SAFT encapsulates all types of molecular interactions by incorporating relevant Helmholtz free energies. It models the strong interactions between water molecules by including an association term for Helmholtz free energy. Additionally, using fundamental principles in statistical mechanics, a Helmholtz term can be derived that represents calcite-water interactions. By incorporation of the square well formed between the adsorbed water and calcite surface, the latter Helmholtz term is defined as a function of the square-well characteristics. Hence, the newly derived Helmholtz term will be a function of confinement characteristics. More detailed explanation can be found in the forthcoming theoretical background.

(iii)-Which technique can be used to explore nanoscale interactions and calculate the necessary parameters for Helmholtz terms?

The molecular dynamics technique was employed to gain insight into how calcite influences the water molecules at the calcite-water interfaces. The previously discussed Helmholtz term that captures calcite-water interactions relies on various confinement parameters, including the potential of calcite-water interactions, the degree of confinement, the fraction of adsorbed water molecules and temperature. Molecular dynamics simulations emerge as a reliable method to calculate these parameters. Moreover, in the process of deriving the molecular-based equation of state, the density of confined water is counted as a key parameter. Molecular dynamics simulations are well suited to meet these demands, offering a proven capability to address these essential aspects.

The described methodology and consequent outcomes of these basic studies may find applications in several study fields such as catalysis, contaminant transfer, the effect of mineral grain size on chemical weathering, the effect of the calcite surface in limiting mineralization in oceans, the estimate of solubility limits in multicomponent fluid processing, and enhanced oil recovery (EOR), among other topics.

## 1.7 Thesis structure

The main focus of this study is behavior of water molecules at the calcite-water interface, and how the thermodynamic properties of water evolve from discrete near the interface, to bulk properties far from the interface.

In the absence of confinement in the bulk phase, water-water interactions govern and determine bulk water properties. However, introducing the calcite mineral into the bulk water system adds a group of extra molecular interactions, called calcite-water interactions. Thus, accurate estimations of bulk properties require a deep understanding of the underlying mechanisms, including the formation of the first adsorbed layer, the identification of multilayer structures bonding to the adsorbed layer, and the influence of environmental parameters like temperature, pressure, and confinement size. In the confined interface, water molecules are held close to the calcite surface through a combination of electrostatic attraction, repulsion, and induction energies. These energies collectively account for the physisorption of water onto the calcite surface. Therefore, an exploration of the energy and density profiles of confined water can provide valuable insights into the underlying interaction mechanisms between water and calcite. This leads to our first research question:

**Research Question-1 (RQ-1): How does the combination of water-water and calcite-water interactions affect the macroscopic properties of water, under one-dimensional confinement?**

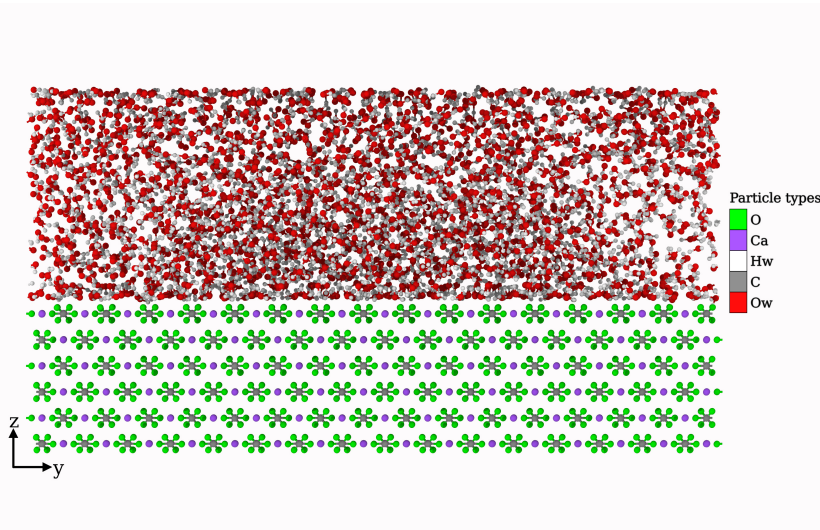


Figure 1.2: Sketch of the confinement geometry within water-calcite interface studied in Paper I.  $L_z$  is the distance from the uppermost layer of water bulk to the calcite surface.  $\delta$  is the thickness of the surface-adsorbed layers.

**Paper(I)** replies to this question by presenting simulation results of a model system with one-dimensional confinement for water molecules. In fact, adding this confinement will divide the simulated domain into several discrete regions with distinct behaviors: i) a region with adsorbed water molecules over the hydrophilic surface of calcite and ii) a region wherein water molecules tend to behave like bulk water far from any confinement.

In order to predict the water properties at near a calcite surface, a new contribution for the Helmholtz energy extended from Perturbed-Chain SAFT (PC-SAFT) EoS was defined. The new Helmholtz energy contribution depends on the confinement parameters, i.e. the potential of water-calcite interaction ( $\epsilon$ ), confinement degree ( $\theta$ ), bulk-like density ( $\rho$ ), and fraction of confined molecules ( $F_{pr}$ ), which were estimated by molecular dynamics simulations. The simulation results also show the adsorption of the fully structured layers of water on the calcite surface. In addition, the simulations confirm the energy deviation within the layering zone. Finally, it has been demonstrated that with increasing temperature and the level of confinement, the properties of confined water tend to align with those of the bulk liquid. Figure 1.2 shows the schematic geometry of the simulated system.

When a one-dimensional confinement is introduced to the system, multiple layers of water are adsorbed over the calcite surface. Beyond these adsorbed layers, water molecules form a network through hydrogen bonding, and water-water interactions are developed. As mentioned above, within one-dimensional confinement, molecular interactions shift from predominantly calcite-water

interactions to water-water interactions. As one moves away from the calcite surface, the attractive forces diminish, and water-water interactions approach bulk-like interactions where no confinement is present. What if one imposes two-dimensional confinement and prevents the establishment of pure water-water interactions from either end? This scenario sets the stage for the second research question:

**Research Question-2 (RQ-2): when water is constrained within a two-dimensional confinement, how does the interplay between water-water interactions and calcite-water interactions on both sides influence the bulk properties?**

**Paper(II)** replies to this question by simulating a system that comprises two calcite nanoslabs with water in between. In the context of a two-dimensional confinement, the hydrophilic nature of calcite slabs on both sides provides dual fronts of calcite-water interactions, encapsulating a cluster of water molecules that fall within the categories of calcite-water and water-water interactions in terms of energy. The two-dimensional confinement will separate the confined space into several regions. Reducing the confinement size may lead to the overlap of different regions, resulting in a new behavior. Analysis of the energy and density profile of confined water within different regions contributes to a better understanding of the phenomenon.

In order to incorporate the impact two-dimensional confinement on the properties of confined water, I developed an EoS based on SAFT principles. In this work, the newly introduced Helmholtz energy depends not only on the potential of water-calcite interactions ( $\varepsilon$ ) and bulk-like density ( $\rho$ ), but also on a novel parameter called CF, representing the density fraction within the adsorbed layer and bulk-like zone. Unlike cubic EoSs, which often use empirical parameters without physical meaning, CF is defined by the physics of the simulated system. Investigating various pore sizes at different temperatures reveals that temperature causes the density in the layering zone to rise, which differs from earlier findings. Furthermore, coupling CF with proposed EoS decreased the absolute relative error by nearly 50% at low temperatures, demonstrating that other parameters, such as geometry and layering pattern, influenced the properties of the confined fluid. Figure 1.2 shows the schematic geometry of the simulated system.

Up to this point, we have examined the interactions of pure water with calcite. The neutral surface (10 $\bar{1}$ 4) of the calcite is chosen to avoid the intervention of additional partial charges from the mineral side. By altering temperature and confinement size, we have investigated how water-water and water-calcite interactions combine under one- and two-dimensional confinements, resulting in distinct properties for confined water. The inherent hydrophilic properties of calcite result in the adsorption of water molecules onto its surface. This occurs as the surface Ca<sup>2+</sup> cations coordinate with oxygen atoms in water and surface CO<sub>3</sub><sup>2-</sup> anions make hydrogen bonds with hydrogen atoms in water. In fact, the surface chemistry of calcite imparts hydrophilic characteristics to its surface. Previous studies have investigated how physical parameters like temperature

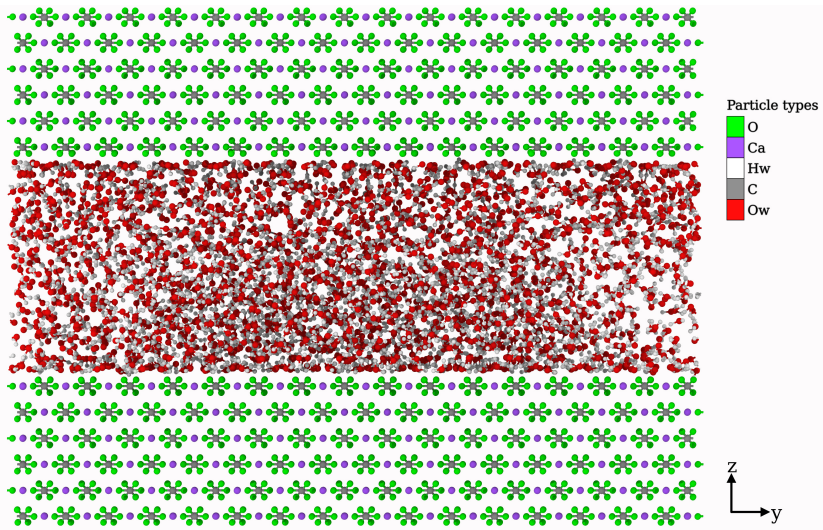


Figure 1.3: Illustration of the confinement geometry within a calcite nanopore used for the simulations in Paper II.  $L_z$  denotes the width of the calcite pore.  $\delta$  shows the thickness of the surface-adsorbed layers.

and confinement size affect the surface chemistry of calcite. It is now time to investigate the influence of chemical modifications on the surface chemistry of calcite. These modifications involve the introduction of anions and cations into the water, and the goal is to analyze how these changes affect the adsorption behavior of calcite. This question forms the basis for the third scientific question:

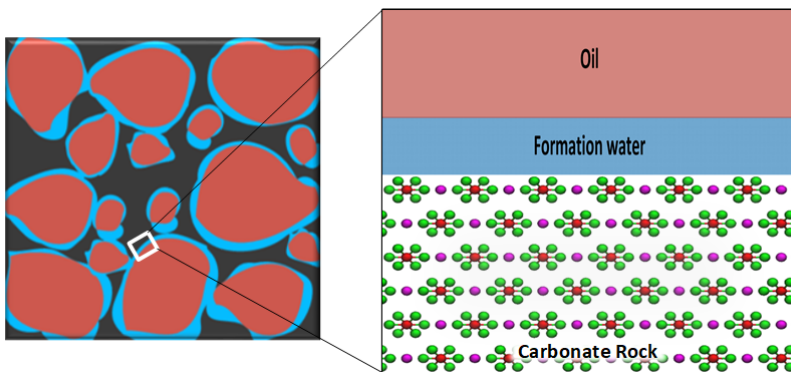


Figure 1.4: Sketch of the calcite-oil-brine system used in Paper III. Formation water ( $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Ca}^{2+}$ ) and oil (toluene, decane, benzoic acid) and interact with the calcite ( $10\bar{1}4$ ) surface.



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**Research Question-3 (RQ-3): How do mono/divalent ions at the brine water-oil-calcite interface affect the adsorption behavior of the calcite surface?**

**Paper(III)** replies to this question by simulating a calcite-oil-brine system so that high salinity brine, oil, and low salinity brine lay across a calcite nanoslab, respectively. The oil phase contains toluene, decane, and benzoic acid to simulate aromatic, hydrocarbon, and polar constituents dissolved in oil. The high- and low-salinity solutions contained water molecules in combination with mono/divalent ions, i.e.,  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ . The results of molecular dynamics simulation show that mono- and divalent ions initially undergo hydration, with monovalent ions forming an electrical double layer above the calcite surface. Characterizing the dynamics of different ions denotes that the monovalent ions ( $\text{Na}^+$  and  $\text{Cl}^-$ ) settle within the compact hydration layers on the calcite surface. However, divalent ions show different behaviors. Initially,  $\text{Ca}^{2+}$  ions, which are observed in close proximity to the calcite surface, migrate away over time. On the other hand,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ , which were initially distant from the calcite surface, move closer to the calcite surface following oil displacement. In essence, prior to oil displacement, the positions of ( $\text{Na}^+$ ,  $\text{Cl}^-$ ) and  $\text{Ca}^{2+}$  becomes fixed and the trend of double electric layer expands. This signifies that the detachment of oil from the calcite-brine interface occurs simultaneously with extension in charge density. Figure 1.4 shows the schematic geometry of the simulated system.

This Ph.D. dissertation collects and summarizes the findings from above mentioned questions, each of which will be answered in its own research paper.

## 1.8 Outline

This Ph.D. dissertation follows the Manuscript Document Format of Oslo University and is organized into three main chapters. Chapter 1 is referred to as the Introduction serves as a framework for better understanding the dissertation's coherence and motivation. Chapter 2 puts the research theory into a broader context by providing the theoretical background for statistical association fluid theory (SAFT) and molecular dynamics (MD) toolboxes, which were used as the main computational tools in the papers. Chapter 3 contains the key findings of the research and provides future directions for further investigation. Chapter 4 includes three published papers in which I am the first author. A summary of the appendices is given in Chapter 5, including several conference proceedings and extended abstracts.



## Chapter 2

# Theoretical background

Modern tools for calculating the properties of pure substances and mixtures are highly based on the cubic-type equation of states [141–143]. However, these equations struggle to accurately model complex molecular interactions found in polar systems, chain-like molecules, associating fluids, and electrolyte systems [144–147]. Moreover, this challenge extends to the precise calculation of liquid densities due to the inadequacy of the repulsive reference term in van der Waals equations [148, 149]. The challenges originate from the fact that cubic-type equations were initially formulated to characterize fluids composing of relatively simple molecules governed by van der Waals interactions and weak-dipole-induced electrostatic forces. However, in real-world scenarios, many fluids exhibit strong attractive forces between their molecules, presenting a challenge to the cubic-type equation of states. Here, statistical associating fluid theory (SAFT) becomes invaluable, providing an effective approach for modeling none-ideal and intense intermolecular interactions [150–153]. This chapter briefly reviews the main modeling tools used in this Ph.D. dissertation:

- Statistical Association Fluid Theory (SAFT)
- Molecular Dynamics Simulations

## 2.1 Equation of state

In thermodynamics, equations of states (EoS) establish relationships among state variables, including pressure ( $P$ ), volume ( $V$ ), and temperature ( $T$ ), under specific physical conditions. These equations serve as fundamental tools, providing a mathematical framework that connects P-V-T. In addition to the physical properties of pure substances, EoSs are able to predict the properties of mixtures, phase equilibrium conditions, boundary between states, and elucidate phase behavior [154, 155]. In the oil and gas industries, EoSs are widely used to calculate the properties of petroleum fluids. Figure 2.1 shows a typical 3-dimensional phase diagram [156].

### 2.1.1 Cubic equation of state

The simplest equation of state is the ideal gas law, which is presented in equation (2.1).

$$PV = nRT \quad (2.1)$$

This equation relates pressure, volume and absolute temperature with an universal gas constant ( $R$ ) and  $n$  which is the number of moles of the gas. In the

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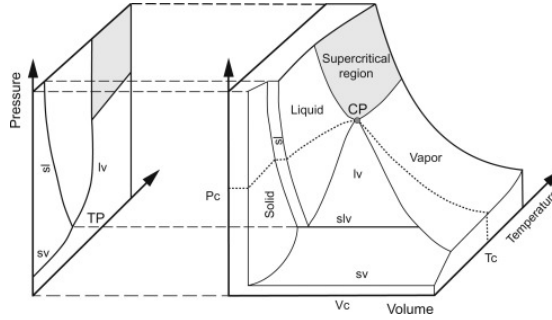


Figure 2.1: A typical three-dimensional phase diagram and its projection onto pressure-temperature (P-T) and pressure-volume (P-V) planes [156].

ideal gas context, gas molecules are assumed as point masses possessing perfectly elastic collisions. While this hypothesis is correct for dilute gases, Johannes D. van der Waals [157] improved the ideal gas law in 1873 by introducing two extra parameters: molecular size and molecular interaction forces. Equation (2.2) represents the van der Waals EoS for  $n$  moles of gas:

$$\left(P + a \left(\frac{n}{V}\right)^2\right) \left(\frac{V}{n} - b\right) = RT, \quad (2.2)$$

where  $a$  accounts for the intermolecular interactions and  $b$  represents the volume occupied by the molecules. Rearranging the equation (2.2) to solve for  $V$  gives a third order polynomial as:

$$V^3 - \left(\frac{RT}{P} + b\right)V^2 + \left(\frac{a}{P}\right)V - \frac{ab}{P} = 0. \quad (2.3)$$

The equation (2.3) represents a cubic function with respect to volume. In thermodynamics, the critical point denotes a state at which the liquid-vapor phase boundary vanishes, marking the endpoint of the equilibrium diagram. Thus, at the critical point, the volume equals the volume under critical <sup>1</sup> conditions, expressed as  $V - V_c = 0$ . Substituting  $V$  from equation (2.3), one can express the van der Waals equation in terms of  $Z$ , known as compressibility factor <sup>2</sup>:

$$Z^3 - (1 + B)Z^2 + AZ - AB = 0, \quad (2.4)$$

which introduces another cubic equation in terms of  $Z$ , where the dimensionless parameters  $A$  and  $B$  are defined as:

$$A = \frac{aP}{RT^2} \quad (2.5)$$

<sup>1</sup>The subscript  $c$  denotes the critical point

<sup>2</sup>Compressibility factor indicates how far a real gas deviates from an ideal gas

$$B = \frac{bP}{RT} \quad (2.6)$$

and  $a$  and  $b$  are defined as:

$$a = \frac{27R^2T_c^2}{64P_c} \quad (2.7)$$

$$b = \frac{RT_c}{8P_c} \quad (2.8)$$

where  $T_c$  and  $P_c$  represent the temperature and pressure at critical point.

Notably, the van der Waals equation of state marked a significant milestone, as it effectively represented the coexistence of vapor and liquid for the first time. This equation models fluid particles as hard spheres interacting through repulsive and attractive forces. Originally developed for simple fluids with weak intermolecular interactions, it offers a qualitative description of vapor-liquid phase transitions [158]. However, its accuracy is limited for critical properties and phase equilibrium calculations. Consequently, many research efforts since 1873 have concentrated on adopting the van der Waals equation of states to the fluids possessing more complex intermolecular interactions. Some studies have focused on modifying the attractive term [159–161], while others have addressed the repulsive term [162–164]. Additionally, certain studies have considered modifications to attractive and repulsive terms simultaneously [165–169].

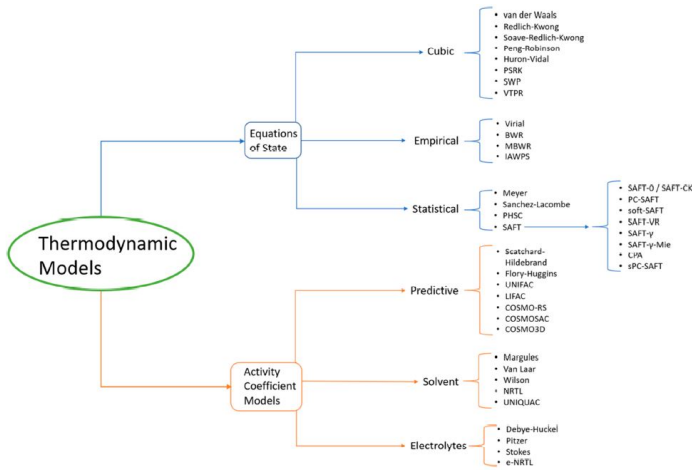


Figure 2.2: A brief overview of available thermodynamic EoS in literature [170].

## 2.1.2 Limitations of cubic-type equations of state

Van der Waals-based equations of state rely on a concept of hard-sphere interactions, wherein weak long-range dispersion forces are approximated at the mean-field level [171]. This approach works well for fluids with spherical or

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nearly spherical molecules interacting with weak intermolecular forces. Examples include low molecular mass hydrocarbons (e.g. methane) and simple organic (e.g., Toluene) and inorganic molecules (e.g.  $N_2$  and  $O_2$ ) [172].

However, more complex fluids, such as electrolytes, polar solvents and polymers present a different challenge. Unlike the simple fluids mentioned earlier, these fluids possess molecules exhibiting non-spherical (aspherical) shape interacting with highly directional forces [173]. In these complex fluids, the natural tendency is formation of associated species like dimers, trimers and longer chain-like structures. This category consists of fluids characterized by hydrogen bonding, charge transfer, non-homogeneous (non-ideal) interactions (e.g. mineral-fluid interaction) and various type of complexities [174].

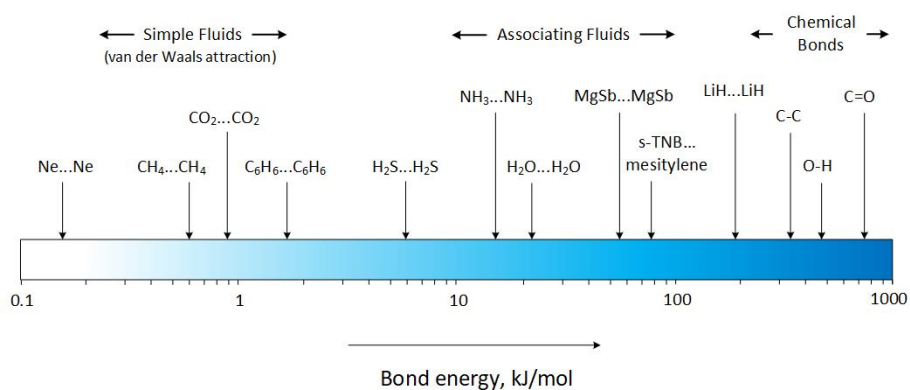


Figure 2.3: Visualizing the continuous spectrum of bond strengths . The energy spectrum highlighted in blue depicts the range from elementary van der Waals attractions to the formation of chemical bonds [172].

For instance, the association species in water are formed by the hydrogen bonding, which is a strong electrostatic interaction between hydrogen and oxygen atoms. The associated species continuously form and break apart due to thermal motion. The concentration and lifetime of these aggregates depend strongly on temperature and density [175].

In practice, well-established cubic equations of states are a common choice for modeling complex fluids [176, 177]. However, their limitations become apparent with the introduction of complex and unrealistic mixing rules [178] alongside temperature-dependent binary parameters [179], leading to a decrease in precision [180]. Therefore, the framework of cubic-type EoSs are poor to generate reliable predictions for fluids with complex intermolecular interactions [145, 181].

### 2.2 Statistical association fluid theory

The progress in statistical mechanics coupled with improved computational capabilities has paved the way for the utilization of equations of state based

on molecular principles. The statistical associating fluid theory (SAFT) is a molecular-based equation of states developed by Chapman and coworkers [182–185] based on the thermodynamic perturbation theory (TPT) of Wertheim [186–189]. Perturbation theories offer straightforward approximate solutions for a given molecular model by partitioning the total intermolecular forces into reference and perturbation terms. In this framework, the reference term corresponds to repulsive forces, while the perturbation term represents attractive forces [190]. The general framework of SAFT-type equations of state are written in the terms of Helmholtz free energy  $A(N, V, T)$  with the functional parameters representing the number of particles, volume and temperature of the system. In SAFT, molecules are seen as flexible chains, each consisting of  $m$  tangential segments (hard-spheres) with a diameter of  $\sigma$ . These chains may also have sites attracting other chains to associate with. Figure 2.4 presents a typical molecular chain with three association sites.

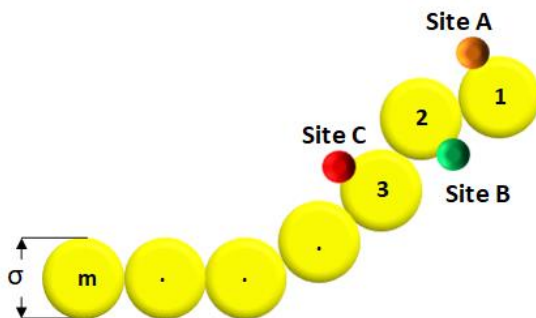


Figure 2.4: Illustration of a typical SAFT molecular model, consisting of  $m$  spherical segments with diameter  $\sigma$  and three association sites.

The definition of different intermolecular contributions in SAFT begins by introducing the dimensionless form of the total Helmholtz free energy:

$$\tilde{a} = \frac{A}{Nk_B T}. \quad (2.9)$$

In equation (2.9), the symbols  $N$ ,  $k_B$ ,  $T$  denote number of particles, Boltzmann constant and absolute temperature, respectively. Then, by considering the residual Helmholtz energy as  $\tilde{a}^{res} = \tilde{a} - \tilde{a}^{id}$ , the fundamental formulation of the SAFT-type equations of state can be expressed in terms of the residual Helmholtz energy [191]:

$$\tilde{a}^{res} = \underbrace{\tilde{a}^{hs}}_{\text{reference term}} + \underbrace{\tilde{a}^{chain} + \tilde{a}^{disp} + \tilde{a}^{assoc}}_{\text{perturbation term}}. \quad (2.10)$$

Different contributions in equation (2.10) are interpreted as:

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- $\tilde{a}^{hs}$  serves as the reference term, corresponding to the contribution of the hard-sphere and accounting for the repulsion interactions between the hard-spheres.
- $\tilde{a}^{chain}$  illustrates the chain contribution, corresponding to the formation of chains between hard-spheres through bonding (e.g. covalent bonding).
- $\tilde{a}^{disp}$  represents the dispersion contribution, corresponding to the attractive interactions between the chains.
- $\tilde{a}^{assoc}$  denotes the association contribution, corresponding to the formation of association complexes between the chains (e.g. hydrogen bonding)

Figure 2.5, provides graphical insights into the various elements incorporated in equation (2.9).

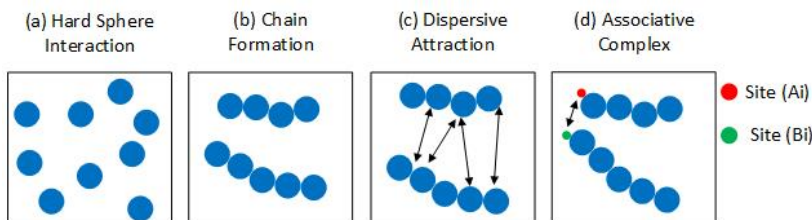


Figure 2.5: Different Helmholtz free energy contributions in SAFT. (a) Hard-spheres with repulsion-attraction interactions. (b) Formation of chains through covalent bonds between hard-spheres. (c) Dispersion interactions between the chains. (d) Association complex formation via association sites, such as hydrogen bonding, linking molecular structures.

### 2.2.1 Hard-sphere (reference term)

The hard-sphere term is defined as [174]:

$$\tilde{a}^{hs} = m \frac{4\eta - 3\eta^2}{(1 - \eta)^2}, \quad (2.11)$$

where  $m$  is the number of spherical segments per molecule and  $\eta$  is the reduced density defined as:

$$\eta = 0.74048\rho m v^0, \quad (2.12)$$

where  $v^0$  is the close-packed hard-core volume of the fluid. Based on the Chapman et al., [185] definition,  $v^0$  is calculated from :

$$v^0 = v^{00} \left( \frac{1 + \frac{0.2977}{C}}{1 + \frac{0.33163}{C} + \frac{0.0010477 + 0.025337\left(\frac{m-1}{m}\right)}{C^2}} \right), \quad (2.13)$$



where,  $C = u^0/kT$  is the dispersion energy per segment. Generally,  $m$ ,  $v^{00}$  and  $u^0/k$  are available for different fluids.

### 2.2.2 Chain term

The chain term is calculated as follows:

$$\tilde{a}^{chain} = (1 - m) \ln \frac{1 - 0.5\eta}{(1 - \eta)^3}. \quad (2.14)$$

### 2.2.3 Dispersion term

Chapman et al., [185] definition for dispersion term is:

$$\tilde{a}^{disp} = m \frac{u^0}{kT} \left( a_1^{disp} + \left( \frac{u^0}{kT} \right) a_2^{disp} \right), \quad (2.15)$$

where,

$$a_1^{disp} = -11.604\eta - 6.132\eta^2 - 2.871\eta^3 + 13.885\eta^4, \quad (2.16)$$

and

$$a_2^{disp} = -2.575\eta + 13.463\eta^2 - 29.992\eta^3 + 21.470\eta^4. \quad (2.17)$$

### 2.2.4 Association term

The association term for the residual Helmholtz free energy is calculated as [185]:

$$\tilde{a}^{ass} = \sum_{i=1}^{N_c} x_i \left( \sum_{A_i=1}^{n_i} \left( \ln X^{A_i} - \frac{X^{A_i}}{2} \right) + \frac{M_i}{2} \right), \quad (2.18)$$

where,

$N_c$ : number of components in the mixture,

$n_i$ : number of association sites of each molecule of component  $i$ ,

$A_i$ : association site  $A$  in molecule  $i$ ,

$M_i$ : number of association sites ( $A, B, C, \dots$ ) in molecule  $i$ .

$\sum_i$  and  $\sum_{A_i}$  in equation (2.18) are described as the summation over all components and summation over association sites, respectively. Furthermore,  $X^{A_i}$  is the fraction of molecules  $i$  which is not bonded at the site  $A$  and is defined as:

$$X^{A_i} = \left( 1 + \rho \sum_{j=1}^{N_c} \sum_{B_j=1}^{n_i} x_j X^{A_i} \Delta^{A_i B_j} \right)^{-1}, \quad (2.19)$$

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where,

$\Delta^{A_i B_j}$  is a parameter that describes the association strength between site  $A$  on molecule  $i$  and site  $B$  on molecule  $j$ , which is expressed as:

$$\Delta^{A_i B_j} = g_{ij}^{hs} \left( \exp \left( \frac{\varepsilon^{A_i B_j}}{k_B T} \right) - 1 \right) \sigma_{ij}^3 \kappa^{A_i B_j}. \quad (2.20)$$

To describe an associating fluid with SAFT, it is necessary to specify two pure-component parameters: association energy  $\varepsilon^{AB}$  and effective association volume of  $\kappa^{AB}$ . These parameters are in addition to the three pure-component parameters for simple fluids ( $m$ ,  $v^{00}$  and  $u^0/k$ ), all of which can be adjusted to match the data of pure component.

### 2.2.5 Mixing rules

Using straight-forward mixing rules are important to calculate the mixture parameters. In this regard, the mixing rule of Berthelot-Lorentz is used for pair of unlike segments:

$$\sigma_{ij} = \frac{1}{2}(\sigma_i + \sigma_j), \quad (2.21)$$

$$\varepsilon_{ij} = (1 - k_{ij}) (\varepsilon_i \varepsilon_j)^{0.5}. \quad (2.22)$$

The cross-associating interactions between associating components are evaluated by mixing rules of Wolbach and Sandler [192]:

$$\varepsilon^{A_i B_j} = \frac{1}{2} (\varepsilon^{A_i B_i} + \varepsilon^{A_j B_j}), \quad (2.23)$$

$$\kappa^{A_i B_j} = (\kappa^{A_i B_i} \kappa^{A_j B_j})^{0.5} \left( \frac{(\sigma_i \sigma_j)^{0.5}}{0.5(\sigma_i + \sigma_j)} \right)^3. \quad (2.24)$$

### 2.2.6 Helmholtz term for water-calcite interaction

The essence of SAFT is that the residual Helmholtz energy ( $\tilde{a}^{res}$ ) is given by a sum of Helmholtz species ( $\tilde{a}^i$ ) to account for the effects of hard sphere, chain, dispersion, association. As seen in equation (2.10), it is possible to describe a particular intermolecular interaction using relevant Helmholtz species. Hence, to include the interaction between water and calcite, the key step is to define a residual Helmholtz term associated with the water-calcite interaction. This defined species is then incorporated into the broader Helmholtz summation, highlighting its significance in modeling the complexities of water-mineral interactions. Figure 2.6 illustrates our assumptions and provides a better understanding of water-water and water-calcite interactions, wherein water is confined between two calcite nanoslabs. As seen, the confinement space is partitioned into three distinct regions based on their proximity to the calcite wall.

Region I (bulk-like) is the outermost section nearest to the pore center. The dominant interactions here are fluid-fluid interactions, which are characterized by a square-well potential. Region II (layering zone) with a thickness of  $\delta_{fw}$  involves water-calcite interactions, which are characterized by a square-well potential. Finally, Region III displays an empty margin adjacent to the pore walls with no water molecules inside, characterized by a thickness of  $\sigma_i/2$ .

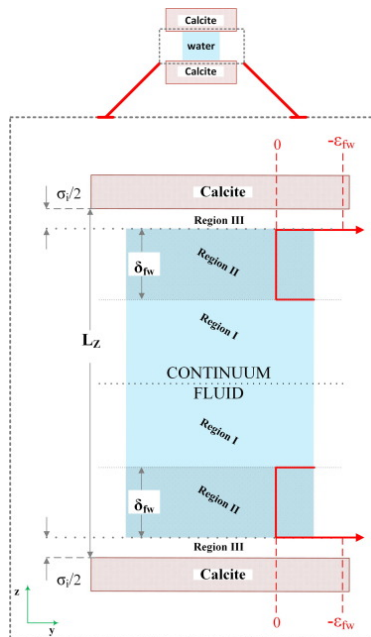


Figure 2.6: Configuration of a calcite pore that contains water. The mineral walls interact with water molecules through a square-well potential [193]. As depicted,  $L_z$  is the distance between the outermost layers of the calcite surfaces.  $\delta_{fw}$  and  $\varepsilon_{fw}$  are the width and depth of the square-well energy.  $\sigma_i/2$  is the thickness of space above the calcite surface which contains no water molecule.

In order to derive a definition for Helmholtz free energy in the context of water-calcite interaction, one can start the process by formulating the partition function equation. This equation serves as a bridge to relate the microscopic states of a system with its macroscopic properties observed at thermal equilibrium. Defining a partition function  $Q$  for a system of  $N$  particles gives [194, 195]:

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} V_f^N \exp \left( \int_{-\infty}^T \frac{E_{conf}}{kT^2} dT \right) \right), \quad (2.25)$$

where,  $q_{int}$  is the internal partition function,  $\lambda$  represents the de Broglie wavelength,  $T$  is the absolute temperature,  $E_{conf}$  is the configurational energy, and  $V_f$  denotes the free volume defined as:

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$$V_f = V - \frac{N}{\rho_{max}}, \quad (2.26)$$

where,  $\rho_{max}$  is the molecular density of the closed-pack fluid. The configurational energy  $E_{conf}$  in equation (2.25) includes the attractive part of the average total energy for  $N$  molecules in a system with volume  $V$ . In other words,  $E_{conf}$  defines the attractive part of the molecule–molecule interactions that occur throughout the system volume. Therefore, for a confined fluid, the definition of  $E_{conf}$  should take into account the fluid-fluid and fluid-wall interactions, namely:

$$E_{conf} = E_{conf-ff} + E_{conf-fw}, \quad (2.27)$$

where, the subscripts *ff* and *fw* describe fluid-fluid and fluid-wall interactions, respectively. Assuming that these interactions occur pairwise through the square-well potential, for fluid-fluid interactions, we have:

$$u(r_{ij}) = \begin{cases} \infty, & r_{ij} < \sigma_{ij} \\ -\varepsilon_{ij} & \sigma_{ij} < r_{ij} < \sigma_{ij} + \delta_{ij} \\ 0 & r_{ij} > \sigma_{ij} + \delta_{ij}, \end{cases} \quad (2.28)$$

where  $r_{ij}$  represents the distance between two water molecules,  $\varepsilon_{ij}$  is the depth of the square-well,  $\delta_{ij}$  is the relevant width of the square-well, and  $\sigma_{ij}$  is defined as the molecular diameter of the water. Here, the attractive part of interaction energy is defined based on the pairwise additive hypothesis, namely:

$$u(r_1, r_2, \dots, r_N) = \sum_i \sum_j u(r_{ij}). \quad (2.29)$$

By extending this hypothesis to the attractive part of fluid-wall interactions, we have the following:

$$u(l_{fw}) = \begin{cases} \infty & l_{fw} > L_Z - 2\sigma_i \\ -\varepsilon_{fw} & L_Z - 2\sigma_i - 2\delta_{fw} < l_{fw} < L_Z - 2\sigma_i \\ 0 & l_{fw} < L_Z - 2\sigma_i - 2\delta_{fw}, \end{cases} \quad (2.30)$$

where,  $l_{fw}$  is the distance between water molecules and calcite slab,  $L_Z$  denotes the width of the calcite nanoslabs (pore size) and  $\varepsilon_{fw}$  indicates the depth of square-well. Now, based on the square-well potentials defined in equations (2.28) and (2.30), one can redefine the attractive part of the interaction energy using  $E_{conf}$  as follows:

$$E_{conf} = -(N/2)N_c\varepsilon_{ij} - NC_F\varepsilon_{fw}. \quad (2.31)$$

The right side of equation (2.31) comprises two terms: the first term represents the water-water interaction, while the second term describes the water-calcite interaction.  $N_c$  represents the coordination number and  $C_F$  is the fraction counting the confined fluid density compared to the bulk-like fluid density. In fact,  $C_F$  incorporates the effect of the number of confined molecules and their

associated confined volume into the total  $E_{conf}$ .  $C_F$  will be calculated with molecular dynamic simulations. Substituting equation (2.31) into equation (2.25) yields:

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} V_f^N \exp \left( \int_{\infty}^T \frac{E_{conf-ff}}{kT^2} dT \right) \exp \left( \int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT \right) \right). \quad (2.32)$$

Based on the definition of the Helmholtz free energy, expressed as  $A = -kT \ln(Q)$ , incorporating the  $V_f$  from equation (2.26), substituting the relevant square-well potential from equations (2.28) and (2.30) and applying the natural logarithm to equation (2.32) gives:

$$\tilde{a}^{fw} = \left( \ln(\lambda^3) - \ln \left( \frac{1}{\rho} - \frac{1}{\rho_{max}} \right) - \left( \frac{\varepsilon_{conf-ff}}{kT} - 1 \right) - \left( \frac{\varepsilon_{conf-fw}}{kT} \right) \right), \quad (2.33)$$

where,  $\varepsilon_{conf-ff}$  describes the water-water interaction energy that is available in the literature for pure water, while  $\varepsilon_{conf-fw}$  and the fluid density under confinement will be calculated with molecular dynamics simulations. Adding the new developed term of  $\tilde{a}^{fw}$  to the summation of Helmholtz terms gives:

$$\tilde{a}^{res} = \tilde{a}^{hs} + \tilde{a}^{chain} + \tilde{a}^{disp} + \tilde{a}^{assoc} + \tilde{a}^{fw}. \quad (2.34)$$

Once the total Helmholtz energy is calculated, the rest of the thermodynamic properties can be evaluated on the basis of the total Helmholtz energy. For example, based on the residual Helmholtz derivatives, the residual chemical potential  $\mu_k^{res}$  as:

$$\frac{\mu_k^{res}(T, \nu)}{kT} = \tilde{a}^{res} + \left( \frac{\partial \tilde{a}^{res}}{\partial x_k} \right)_{T, \nu, x_i \neq k} - \sum_{j=1}^N \left[ x_j \left( \frac{\partial \tilde{a}^{res}}{\partial x_j} \right)_{T, \nu, x_i \neq j} \right] + (Z - 1), \quad (2.35)$$

where,  $x$  is the mole fraction of component  $i$  and  $Z$  is the compressibility factor written as:

$$Z = 1 + \eta \left( \frac{\partial \tilde{a}^{res}}{\partial \eta} \right)_{T, x_i}. \quad (2.36)$$

Here,  $\eta$  is the packing fraction. Then, the fugacity coefficient can be simply written with respect to  $\mu_k^{res}$  and  $Z$ :

$$\ln \phi_k = \frac{\mu_k^{res}(T, \nu)}{kT} - \ln Z. \quad (2.37)$$

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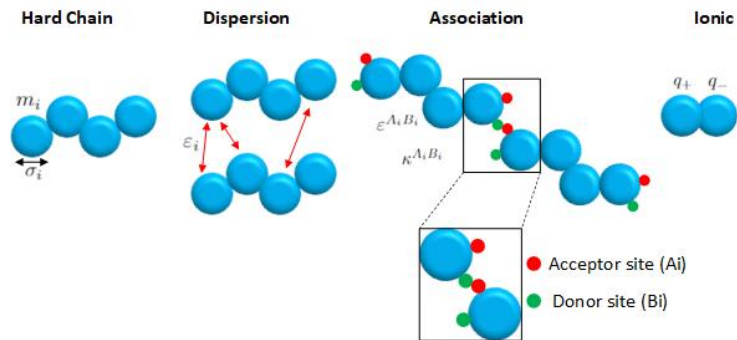


Figure 2.7: Illustration of different molecular contributions in PC-SAFT EoS including hard-chain (hc), dispersion (disp), association (ass) and ionic (ion).

### 2.3 Perturbed-Chain SAFT

Gross and Sadowski [196, 197] introduced a variant of SAFT known as Perturbed-Chain SAFT (PC-SAFT). They applied Barker and Henderson's [198, 199] perturbation theory to address the dispersion contribution ( $a^{disp}$ ), which will be added to the reference term of hard-chain instead of hard-spheres. In essence, the formalism of PC-SAFT can be expressed as:

$$\tilde{a}^{res} = \underbrace{\tilde{a}^{hc}}_{\text{reference term}} + \underbrace{\tilde{a}^{disp} + \tilde{a}^{assoc} + \tilde{a}^{ion}}_{\text{perturbation term}}. \quad (2.38)$$

Here,  $\tilde{a}^{hc}$ ,  $\tilde{a}^{disp}$ ,  $\tilde{a}^{assoc}$  and  $\tilde{a}^{ion}$  indicate the contributions to the Helmholtz energy attributed to hard-sphere chain, dispersion, association and ionic interactions, respectively. Figure 2.7, provides graphical insights into the various species incorporated in equation (2.38). As seen in equation (2.38), the distinction between PC-SAFT and SAFT is addressed to the different reference system that is considered. In other words, the reference system in PC-SAFT is composed of both hard-sphere and chain. Then, dispersion, association and ionic terms are introduced as the perturbation to the reference system.

Non-associating fluids are modeled with PC-SAFT using three parameters  $m$ ,  $\sigma$  and  $\varepsilon$ , representing the number of hard spheres in a chain, segment diameter and dispersion energy, respectively. However, to model a fluid with association and ionic contributions, three additional pure-component parameters are required. These are the association volume ( $\kappa^{A_i B_j}$ ), the association energy ( $\varepsilon^{A_i B_j}$ ) and the ionic valance ( $\nu_j$ ). In this context,  $A_i$  and  $B_i$  indicate different associating sites. The mentioned parameters are available in the literature for different fluids. The description of different contributions represented in equation (2.38) can be pursued in the following.

### 2.3.1 Hard-chain (reference term)

The hard-chain term in PC-SAFT, showing with  $\tilde{a}^{hc}$  accounts for the repulsion of the chain molecules and is written as:

$$\begin{aligned}\tilde{a}^{hc} &= \bar{m}\tilde{a}^{hs} + \tilde{a}^{ch} \\ &= \bar{m}\tilde{a}^{hs} - \sum_{i=1}^{N_c} x_i(m_i - 1) \ln g_{ii}^{hs},\end{aligned}\quad (2.39)$$

where,

$x_i$ : mole fraction of the component  $i$  in chain,

$m_i$ : segment number in a chain of component  $i$ ,

$N_c$ : number of particles,

in equation (2.39),  $\bar{m}$  indicates mean segment number, which is calculated by:

$$\bar{m} = \sum_{i=1}^{N_c} x_i m_i. \quad (2.40)$$

Furthermore, hard-sphere contribution  $\tilde{a}^{hs}$  and radial pair distribution of component  $i$  and  $g_{ii}^{hs}$  are respectively given by:

$$\tilde{a}^{hs} = \frac{1}{\xi_0} \left[ \frac{3\xi_1\xi_2}{(1-\xi_3)} + \frac{\xi_2^3}{\xi_3(1-\xi_3)^2} + \left( \frac{\xi_2^3}{\xi_3^2} - \xi_0 \right) \ln(1-\xi_3) \right], \quad (2.41)$$

$$g_{ij}^{hs} = \frac{1}{1-\xi_3} + \left( \frac{d_i d_j}{d_i + d_j} \right) \frac{3\xi_2}{(1-\xi_3)} + \left( \frac{d_i d_j}{d_i + d_j} \right)^2 \frac{2\xi_2^2}{(1-\xi_3)^3}, \quad (2.42)$$

where,

$d_i$  is segment diameter of component  $i$ , which is calculated by:

$$d_i(T) = \sigma_i \left[ 1 - 0.12 \exp \left( \frac{-3\varepsilon_i}{k_B T} \right) \right], \quad (2.43)$$

and  $\xi_i$  is defined as:

$$\xi_n = \frac{\pi}{6} \rho \sum_{i=1}^{N_c} x_i m_i d_i^n \quad n \in \{0, 1, 2, 3\}. \quad (2.44)$$

In equation (2.44),  $\rho$  represents the total number density, indicating the quantity of particles within a given volume.

### 2.3.2 Dispersion term

The description of the Helmholtz contribution for dispersion interactions is provided in equation (2.45). This description reveals two distinct statements, the first relates to the 1<sup>st</sup> order perturbation term and the second one addresses the 2<sup>nd</sup> order perturbation term.

$$\tilde{a}^{disp} = \underbrace{-2\pi\rho I_1(\eta, \bar{m})\overline{m^2\varepsilon\sigma^3}}_{\text{first order}} - \underbrace{\pi\rho\bar{m}C_1 I_2(\eta, \bar{m})\overline{m^2\varepsilon^2\sigma^3}}_{\text{second order}}, \quad (2.45)$$

where,

$C_1$ ,  $I_1(\eta, \bar{m})$ ,  $I_2(\eta, \bar{m})$ ,  $\overline{m^2\varepsilon\sigma^3}$  and  $\overline{m^2\varepsilon^2\sigma^3}$  are defined as:

$$\begin{aligned} C_1 &= \left(1 + Z^{hc} + \rho \frac{\partial Z^{hc}}{\partial \rho}\right)^{-1} \\ &= \left(1 + \bar{m} \frac{8\eta - 2\eta^2}{(1-\eta)^4} + (1-\bar{m}) \frac{20\eta - 27\eta^2 + 12\eta^3 - 2\eta^4}{(1-\eta)^2(2-\eta)^2}\right)^{-1}, \end{aligned} \quad (2.46)$$

$$I_1(\eta, \bar{m}) = \sum_{i=0}^6 a_i(\bar{m})\eta^i, \quad (2.47)$$

$$I_2(\eta, \bar{m}) = \sum_{i=0}^6 b_i(\bar{m})\eta^i, \quad (2.48)$$

$$\overline{m^2\varepsilon\sigma^3} = \sum_{i=1}^{N_c} \sum_{j=1}^{N_c} x_i x_j m_i m_j \left(\frac{\varepsilon_{ij}}{k_B T}\right) \sigma_{ij}^3, \quad (2.49)$$

$$\overline{m^2\varepsilon^2\sigma^3} = \sum_{i=1}^{N_c} \sum_{j=1}^{N_c} x_i x_j m_i m_j \left(\frac{\varepsilon_{ij}}{k_B T}\right)^2 \sigma_{ij}^3. \quad (2.50)$$

Here,  $i$  and  $j$  represent a pair of non-identical segments. In equations (2.47) and (2.48) two coefficients  $a_i$  and  $b_i$  are defined as functions of chain length:

$$a_i(\bar{m}) = a_{0i} + \left(\frac{\bar{m}-1}{\bar{m}}\right) a_{1i} + \left(\frac{\bar{m}-1}{\bar{m}}\right) \left(\frac{\bar{m}-2}{\bar{m}}\right) a_{2i}, \quad (2.51)$$

$$b_i(\bar{m}) = b_{0i} + \left(\frac{\bar{m}-1}{\bar{m}}\right) b_{1i} + \left(\frac{\bar{m}-1}{\bar{m}}\right) \left(\frac{\bar{m}-2}{\bar{m}}\right) b_{2i}, \quad (2.52)$$

The coefficient  $\eta$  in equation (2.46) is packing factor and its value varies between 0 and 0.745. Other parameters i.e.,  $a_{0i}$ ,  $a_{1i}$ ,  $a_{2i}$ ,  $b_{0i}$ ,  $b_{1i}$  and  $b_{2i}$  are constant numbers varying by changing the pure component to another. These parameters can be found in the literature.



### 2.3.3 Association term

The association term is considered for components characterized by hydrogen bonding between identical and nonidentical molecules such as water. PC-SAFT utilizes the same association term as the earlier SAFT equations, as discussed in Section 2.2.4.

### 2.3.4 Ionic term

The PC-SAFT model developed by Gross and Sadowski [196, 197] does not contain the ionic term. However, Cameretti et al. [200] modified PC-SAFT to include the electrostatic effect in the fluid properties. They defined the ions as charged hard-spheres in a dielectric continuum. The contribution of Helmholtz energy is written as:

$$\tilde{a}^{ion} = \frac{\kappa}{12\pi\epsilon k_B T} \sum_i x_i q_i^2 \chi, \quad (2.53)$$

where,

$\sum_i$ : summations over all ions in the mixture,

$q_i$ : charge of the ion.

The parameters  $\kappa$  and  $\chi$  in equation (2.53) are defined as:

$$\kappa = \left( \frac{\dot{\rho} e^2}{k_B T \epsilon} \sum_i \nu_i^2 x_i \right)^{\frac{1}{2}}, \quad (2.54)$$

$$\chi_i = \frac{3}{(\kappa \alpha_i)^3} \left( \frac{3}{2} + \ln(1 + \kappa \alpha_i) - 2(1 + \kappa \alpha_i) + \frac{1}{2}(1 + \kappa \alpha_i)^2 \right), \quad (2.55)$$

where,

$\nu_i$ : valance of ion  $i$ ,

$e$ :  $1.6022 \times 10^{-19}$ ,

$\epsilon$ : dielectric constant.

### 2.3.5 Helmholtz contribution for water-calcite interaction

To establish a definition for  $\tilde{a}^{fw}$ , we start by revisiting the concept of canonical partition function. As introduced previously, the canonical partition function is defined as:

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$$Q_{N,V,T} = \left( \frac{q_{\text{int}}^N}{\lambda^{3N} N!} V_f^N \exp \left( \int_{-\infty}^T \frac{E_{\text{conf}}}{kT^2} dT \right) \right). \quad (2.56)$$

For a detailed explanation of the parameters in equation (2.56), the reader can refer to Section (2.2.6). Now, let's delve into the schematic setup depicted in Figure 2.8, illustrating the interface between a calcite nanoslab and water. This figure visually depicts the underlying assumptions of the model.

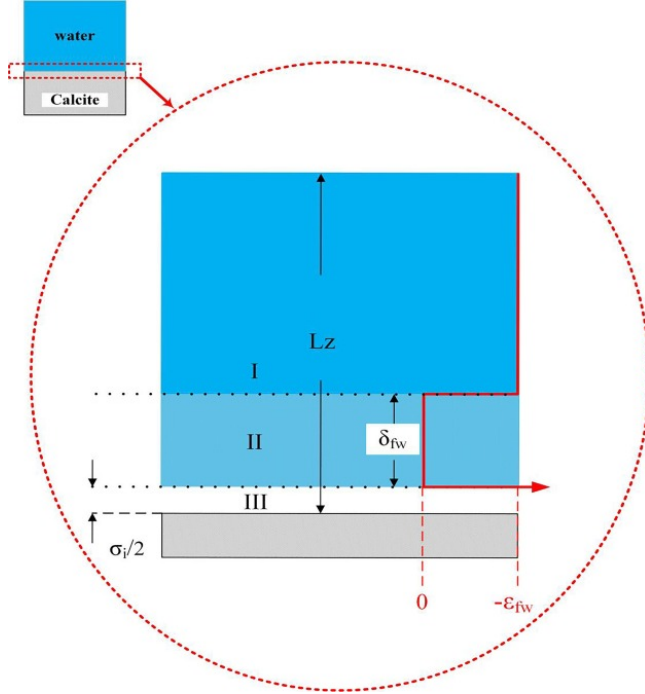


Figure 2.8: Illustration of a water-calcite interface. The calcite nanoslab interacts with water molecules through square-well potential [201].  $L_z$  is the distance between outermost layer of water and calcite surface.  $\delta_{fw}$  and  $\epsilon_{fw}$  are width and depth of the square-well energy.  $\sigma_i/2$  is the thickness of vacant space above the calcite surface.

In a scenario involving bulk water without a calcite slab, interactions purely occur between water molecules. However, introducing a calcite nanoslab results in three distinct zones near the calcite surface:

- Region I is located far from the calcite surface. It involves dominant water-water interactions with the thickness of  $L_z - (\delta_{fw} - \sigma_i/2)$ .

- Region II includes dominant water-calcite interactions with the thickness of  $\delta_{fw}$ .
- Region III exhibits the vacant space above the calcite surface with the thickness of  $\sigma_i/2$ .

Assuming pairwise interactions between the molecules, the interaction between water molecules will be modeled through square-well potential as follows:

$$u(r_{ij}) = \begin{cases} \infty & r_{ij} < \sigma_{ij} \\ -\varepsilon_{ij} & \sigma_{ij} < r_{ij} < \sigma_{ij} + \delta_{ij} \\ 0 & r_{ij} > \sigma_{ij} + \delta_{ij} \end{cases} \quad (2.57)$$

based on the same hypothesis, the square-well potential for water-calcite interaction is expressed as:

$$u(l_{fw}) = \begin{cases} \infty & l_{fw} < \frac{\sigma_i}{2} \\ -\varepsilon_{fw} & \frac{\sigma_i}{2} < l_{fw} < \frac{\sigma_i}{2} + \delta_{fw} \\ 0 & l_{fw} > \frac{\sigma_i}{2} + \delta_{fw} \end{cases} \quad (2.58)$$

To address the confined fluid condition at the water-calcite interface, it is necessary to modify the definition of configurational energy, by including the interactions between water molecules and calcite wall. Thus,  $E_{conf}$  will be split into fluid-fluid and fluid-wall interactions, allowing us to include the attractive part of the dominant molecular interactions within the system volume. In the subsequent analysis, we will utilize Travalloni's [202] approach and adopt his methodology to the geometry presented in Figure (2.8). By assuming the pairwise interaction energies, the modified configurational energy can be formulated as:

$$E_{conf} = \underbrace{-(N/2)N_c\varepsilon_{ij}}_{\text{water-water interaction}} - \underbrace{NF_p\varepsilon_{fw}}_{\text{water-calcite interaction}} \quad (2.59)$$

where,

$N_c$ : is the water-water coordination number

$\varepsilon_{ij}$ : is the depth of the square-well for water-water interaction

$\varepsilon_{fw}$ : is the depth of the square-well for water-calcite interaction

$F_p$ : is separately expressed with the following equation:

$$F_p = F_{pr} + (1 - F_{pr}) \left( 1 - \exp\left(\frac{-\varepsilon_{fw}}{kT}\right) \right) \left( 1 - \frac{\rho}{\rho_{max}} \right)^\theta \quad (2.60)$$

where,

$\theta$  is confinement degree and is given by:

$$\theta = \frac{l_z}{\delta_{fw} + \frac{\sigma}{2}} \quad (2.61)$$

and then,

$F_{pr}$  is expressed as:

$$\begin{aligned}
 F_{pr} &= \frac{\text{volume of region II}}{\text{volume of region I} + \text{volume of region II}} \\
 &= \frac{(l_z - \frac{\sigma}{2}) A_{xy} - (l_z - \frac{\sigma}{2} - \delta_{fw}) A_{xy}}{(l_z - \frac{\sigma}{2}) A_{xy}} \\
 &= \frac{(l_z - \frac{\sigma}{2}) - (l_z - \frac{\sigma}{2} - \delta_{fw})}{(l_z - \frac{\sigma}{2})} \tag{2.62}
 \end{aligned}$$

where,

$A_{xy}$  is the area of the calcite surface extended along  $xy$ -axis.

As per Travalloni's [202] definition in equation (2.60),  $F_p$  denotes the fraction of water molecules confined within the attractive field of the calcite nanoslab. This parameter essentially characterizes the distribution of water molecules within the confinement, which depends on parameters like temperature, interaction energy, fluid density, and confinement geometry [203]. by plugging in the equations (2.59), (2.60) and (2.62) into the definition of partition function in equation (2.56),  $\tilde{a}^{fw}$  is estimated as:

$$\tilde{a}^{fw} = -\frac{\varepsilon_{fw}}{k} \left[ \frac{F_{pr}}{T} + (1 - F_{pr}) \left( 1 - \frac{\rho}{\rho_{max}} \right)^\theta \left( \frac{k (\exp(-\frac{\varepsilon_{fw}}{kT}) - 1)}{\varepsilon_{fw}} + \frac{1}{T} \right) \right] \tag{2.63}$$

As seen, the expression for  $\tilde{a}^{fw}$  relies on confinement parameters  $\varepsilon_{fw}$ ,  $F_{pr}$ ,  $\theta$  and density of the confined fluid. These parameters can be determined through molecular dynamics simulation.

### 2.4 Molecular dynamics

Molecular dynamics simulations are computational tools that allow simulating a microscopic system, using simple principles in classical mechanics. This computational technique utilizes the Born-Oppenheimer [204] approximation, which separates the motion of the atomic nuclei and electrons. Within this framework, atomic nuclei are treated as points of mass, allowing the classical Newtonian equations of motion to describe the behavior of a many-body system. Various molecular dynamics simulation packages such as DLPOLY [205, 206], GROMACS [207–209] and LAMMPS [128] have been developed for different scientific aims. The remarkable advantages provided by molecular dynamics simulations have encouraged numerous researchers to extensively use this tool for various scientific purposes. These applications range from exploring space regions and time resolutions inaccessible through experimental methods [210] to predicting functional properties in biological systems [211] and even refining molecular structures obtained by experimental data [212].

## 2.4.1 Potentials in molecular dynamics simulations

To conduct molecular dynamics simulations for a system, it is necessary to establish the potential function. This function defines how the particles interact with each other, contributing to the overall potential energy. Different potential energy contributions are schematically illustrated in Figure 2.9.

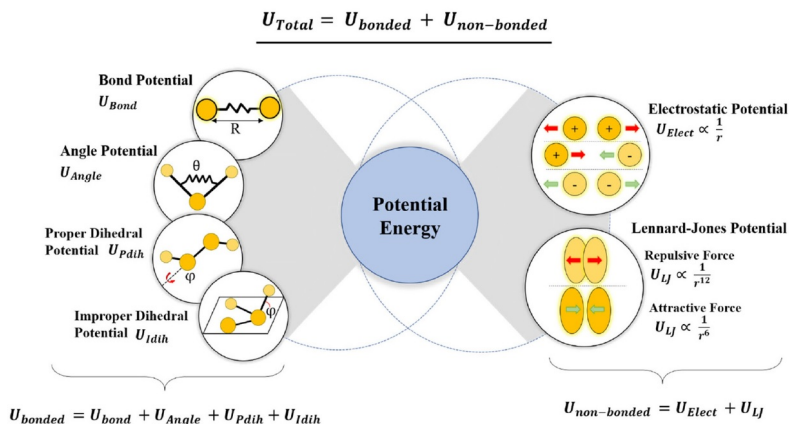


Figure 2.9: For molecular dynamics simulations, two main contributions of potential energy should be defined. The bonded term includes bond, angle, dihedral and improper species, while non-bonded one comprise van der Waals and electrostatic potentials [213]

Typically, the total potential energy contains contributions from bonded and non-bonded interactions [214]

$$U(r) = U_{bonded} + U_{non-bonded}. \quad (2.64)$$

Here, covalent and non-covalent type interactions are represented with bonded and non-bonded subscripts, respectively. Bonded potentials account for the stretching, bending and angle of chemical bonds, as well as the rotations around these bonds. These interactions are relatively strong and directly connected by chemical bonds [215].  $U_{bonded}$  can be expanded as:

$$U_{bonded} = \sum_i U_i^{bond} + \sum_i U_i^{angle} + \sum_i U_i^{dihedral} + \sum_i U_i^{improper}, \quad (2.65)$$

where:

$$U_i^{bond} = K_i^b (r_i - r_0)^2,$$

$$U_i^{angle} = K_i^\theta (\theta - \theta_0)^2,$$

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$$U_i^{dihedral} = K_i^\phi [1 - \cos(n\phi)],$$

$$U_i^{improper} = K_i^\omega (\omega - \omega_0)^2.$$

In equation (2.65), all bonded contributions were presented with harmonic potential formalism. The first term represents the energy as a result of variation in bond length. The second term represents the energy caused by the alteration in the bond angle. The third and fourth terms represent the contributions from dihedral and improper angles, respectively. These terms quantify the energy associated with deviations from a planar configuration and flipping over the mirror image. In other words, improper dihedrals are responsible for maintaining the planarity of planar groups and preventing molecules from flipping over to their mirror images. Furthermore,  $K_i^b, K_i^\theta, K_i^\phi, K_i^\omega$  are harmonic coefficients and  $r_0, \theta_0, n, \omega_0$  are initial geometric constants. On the other hand, non-bonded potentials refer to interactions between particles that are not directly connected by chemical bonds. They consist of van der Waals forces and electrostatic interactions as represented below:

$$U_{non-bonded} = \sum_i U_i^{vdW} + \sum_i U_i^{elec}. \quad (2.66)$$

Non-bonded potentials are typically weaker compared to bonded interactions and act over longer ranges. The van der Waals term includes forces originating from temporary dipoles that can either attract or repel particles based on the distance between them. The van der Waals potential is typically modeled by Lennard Jones as follows:

$$U^{vdw} = 4\varepsilon \left[ \left( \frac{\sigma}{r} \right)^{12} + \left( \frac{\sigma}{r} \right)^6 \right], \quad (2.67)$$

where  $\varepsilon$  is the depth of the potential well,  $\sigma$  is the distance at which the interaction potential reaches zero, and  $r$  is the distance between two particles. Figure 2.10 shows the profile of potential energy versus particle-particle distance according to the classical 12 – 6 Lennard-Jones.

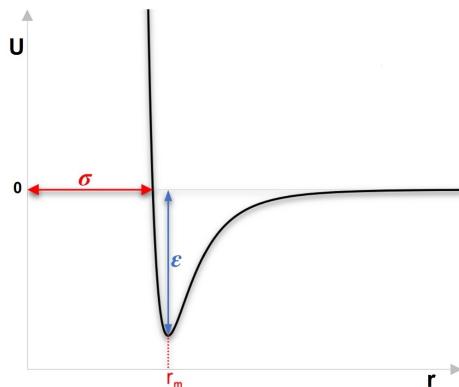


Figure 2.10: Illustration of the Lennard-Jones (12 – 6 potential) function, where parameter  $r_m$  represents the equilibrium distance corresponding to the minimum bonding potential. The figure is adopted from [216].

Electrostatic interactions involve the attraction or repulsion between charged particles and follow the Coulomb interaction formalism:

$$U^{elec} = \frac{1}{4\pi\epsilon} \frac{q_i q_j}{r} \quad (2.68)$$

where  $\epsilon$  is the dielectric constant,  $r$  is the distance between point charges  $q_i$  and  $q_j$ . The potential function formulation and parameters chosen for each species are given in equations (2.65) and (2.66). These parameters typically rely on fitting available experimental data. To be specific, coefficients for each term are adjusted to better match the experimental data.

## 2.4.2 Newton's equations of motion

In molecular dynamics, the motion of the particles is computed by Newton's equations of motion. According to classical mechanics, the total force acting on each particle is derived from the gradient of the potential energy  $U(r)$ , mathematically represented by:

$$\begin{aligned} F &= -\nabla U(r) \\ &= -\left( \frac{\partial U}{\partial x} + \frac{\partial U}{\partial y} + \frac{\partial U}{\partial z} \right), \end{aligned} \quad (2.69)$$

where,  $F$  represents the total force,  $U$  denotes the potential energy and position vector  $r$  consists of the components along the  $x$ ,  $y$  and  $z$  axes. Once the force is known, the acceleration can be obtained using Newton's second law. Re-writing the definition of acceleration ( $a = \frac{dv}{dt}$ ) and velocity ( $v = \frac{dx}{dt}$ ) with Hamiltonian

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formalism leads to a system of differential equations:

$$\frac{dp}{dt} = F \quad (2.70a)$$

$$\frac{dr}{dt} = \frac{p}{m}, \quad (2.70b)$$

where  $p$  is the momentum and  $t$  is time. The numerical solution of the differential equation system introduced in equations (2.70a,2.70b) provides information on the dynamic evolution of the system, by calculating the trajectories of interacting particles over time. In essence, equation (2.70a,2.70b) is the basis for time integration in molecular dynamics simulations and propagation of the system forward in time.

### 2.4.3 Velocity Verlet algorithm

Velocity Verlet [217] algorithm is widely used for integrating Newton's equations of motion due to its time reversibility and energy conservation [218]. This algorithm has been consistently applied in all molecular dynamics simulations conducted within this thesis. It computes the positions and velocities of particles as follows:

- Calculate velocity at half time-step:  $\mathbf{v}(t + \frac{1}{2}dt) = \mathbf{v}(t) + \frac{1}{2} \left( \frac{\mathbf{F}(t)}{m} \right) \cdot dt$ ,
- Correct position:  $\mathbf{r}(t + dt) = \mathbf{r}(t) + \mathbf{v}(t + \frac{1}{2}dt) \cdot dt$ .

Using the above algorithm, one can represent the time integration sequences in molecular dynamics simulation as [219]:



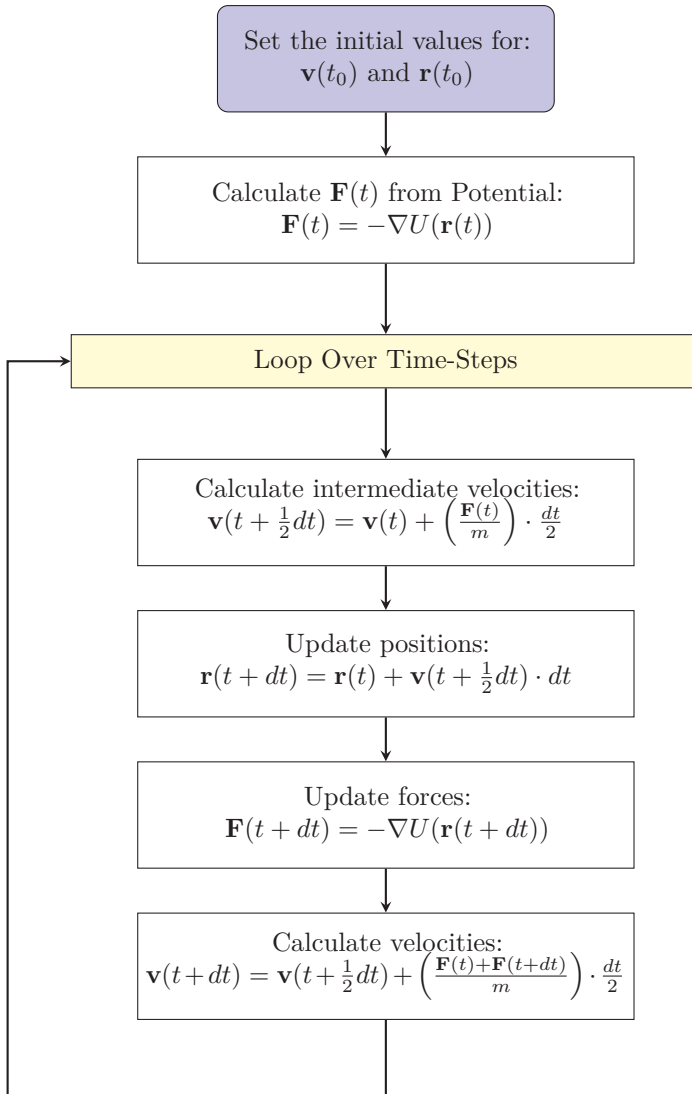


Figure 2.11: Overall approach of time integration in molecular dynamics simulations. The initial state (position and velocity) and interaction potential are input data to the simulations.

As seen, the intermediate velocity at half time-step  $\frac{dt}{2}$  is calculated based on the force at the previous time-step  $t$ . Then, this intermediate velocity is used to calculate the position at the time-step  $dt$ . Now, forces can be updated based on the position at a new time-step. Finally, the velocity at time-step  $dt$  is calculated based on the intermediate velocity and total force acting on a particle. In molecular dynamics simulations, choosing an appropriate time-step

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is crucial to prevent error accumulation. Large time-steps lead to significant error accumulation, while excessively small ones are computationally inefficient. As molecular vibrations occur approximately at frequencies of the order of  $10^{14}$  Hz, a period of about 10 fs ( $10^{-15}$ s) is required. In this Ph.D. thesis, time-step of 1 fs and 0.5 fs were chosen.

### 2.4.4 Periodic boundary conditions

With today's high-performance computing facilities, molecular dynamics simulation can model thousands of particles [220]. Yet, directly simulating systems on a macroscopic scale, close to Avogadro's number ( $6.02 \times 10^{23}$ ) remains unfeasible due to high computational costs. Instead, utilizing periodic boundary conditions along with the minimum image convention facilitates the exploration of macroscopic properties within nanoscale simulations. Under the minimum image convention, only the nearest image of each particle within the periodic boundary conditions is taken into account for pair interactions [221].

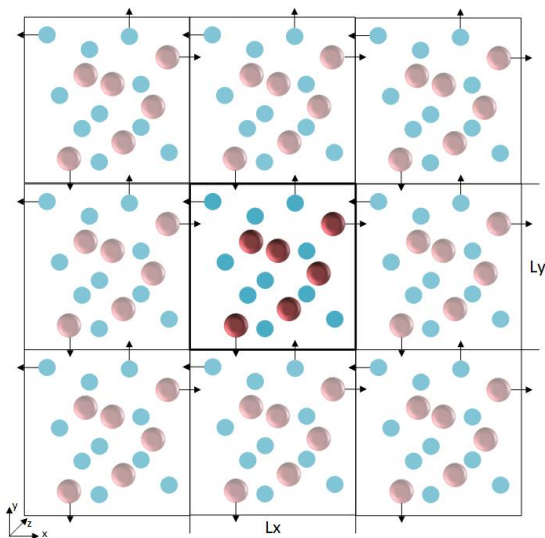


Figure 2.12: Sketch of a binary system, showing periodic boundary conditions. The black arrows show the velocity vector of the relevant particle. The central box represents the main simulation system. The particles that leave the central box are replaced by their image from the opposite box. Each particle interacts with the nearest image of other particles to adhere to minimum image convention.

With periodic boundary conditions, one can replicate an infinite system by ensuring that a particle exiting the simulation box through one side re-enters from the opposite side. The visual representation of a binary system with periodic boundary conditions is shown in Figure 2.12. In this illustration, the central box depicts the main simulated system, while the periodic images of this

system are mapped around it. For a system of dimensions  $L_x \times L_y \times L_z$ , the mathematical representation of the periodic boundary condition for particle  $i$  is given as:

$$x_i^{new} = x_i - L_x \left( \frac{x_i}{L_x} \right) \quad (2.71a)$$

$$y_i^{new} = y_i - L_y \left( \frac{y_i}{L_y} \right) \quad (2.71b)$$

$$z_i^{new} = z_i - L_z \left( \frac{z_i}{L_z} \right) \quad (2.71c)$$

The minimum image convention, on the other hand, calculates the shortest distance between particles in a periodic system. In other words, the convention algorithm considers the periodic nature of the system to determine the shortest possible distance.

### 2.4.5 Ergodicity hypothesis

In experimental methods, computing a property involves conducting measurements over time and averaging them. Similarly, in molecular dynamics simulations, the properties of interest are averaged by numerically evolving the system. In these simulations, a sufficient run-time is required to set the time-averaged property equal to the ensemble-averaged property over the phase space, which includes all possible states in the simulated system [222]. Consider a system containing  $N$  particles, each identified with position  $r_i$  and momentum  $p_i$ . In this system a specific microstate in phase space is represented as  $\Gamma(r^N, p^N)$  where  $r^N \in \{r_1, r_2, \dots, r_N\}$  and  $p^N \in \{p_1, p_2, \dots, p_N\}$ . If the property of interest is denoted as  $A(\Gamma)$ , it changes as the system evolves over time. Thus, ensemble-averaged property can be expressed as:

$$\langle A(r^N, p^N) \rangle = \lim_{t \rightarrow \infty} \frac{1}{t} \int_0^t A(\Gamma(r^N, p^N, t)) dt. \quad (2.72)$$

In molecular dynamics simulations, it is clear that we cannot extend the integral in equation (2.72) to infinite time, but it can potentially be approximated (fulfilled) by averaging over a sufficiently long finite time  $\tau$  such that  $\tau < t$ , namely:

$$\langle A(r^N, p^N) \rangle = \frac{1}{\tau} \sum_{\tau=0}^{\tau < t} A(\Gamma(r^N, p^N, \tau)). \quad (2.73)$$

According to the ergodicity hypothesis, in an adequately long molecular dynamics simulation, the system will explore all possible configurations consistent with the given energy, resulting in time-averaged properties that match the ensemble-averaged properties [223]. To meet the requirements of the ergodicity hypothesis in this Ph.D. thesis, the run-time of all simulation is partitioned

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into equilibration and production phases. During equilibration, the system's properties such as temperature and energy stabilize gradually, ensuring the system reaches a state representative of the desired conditions. Following the equilibration, production begins, during which the system remains stable and data are collected for analysis.

### 2.4.6 Nosé-Hoover thermostat

In molecular dynamics simulations, the behavior of a system is studied within a specific thermodynamic ensemble, allowing for a comprehensive exploration of the dynamics, interactions, and properties exhibited by the simulated system. The thermodynamic ensemble of a system comprising a fixed number of atoms ( $N$ ) confined within a fixed volume ( $V$ ) at a constant temperature ( $T$ ), commonly denoted as  $NVT$ , is known as the canonical ensemble in thermodynamics. Characterization of a system at constant temperature in molecular dynamics can be achieved through various methods. For instance, there exists an early proposal suggesting the control of the system's temperature by limiting kinetic energy. In this method, the velocity of the particle alters at every simulation time-step to comply with the Maxwell-Boltzmann distribution [224, 225]. However, the drawback of this method is that the effects on the dynamical properties of the system are ignored [226]. In this Ph.D. thesis, a thermostat proposed by Nosé-Hoover [227, 228] controls the establishment of  $NVT$  ensemble. In this method, the simulation box is exposed to an external heat bath to achieve equilibrium, presuming that the simulation box boundaries permit only the exchange of energy, not mass. Thus, as the simulation box reaches equilibrium with the external heat bath, the components of both systems reach a uniform temperature  $T$  [229]. The following outline the essential steps to derive Nosé-Hoover thermostat, adopted from Frenkel and Smith's [119] work:

The Lagrangian  $\mathcal{L}$  in a classical system is defined as:

$$\mathcal{L} = K - U, \quad (2.74)$$

where  $K$  is a kinetic energy and  $U$  is a potential energy. Nosé initially derived Lagrangian of a classical system by assuming an additional coordinate  $s$  as:

$$\mathcal{L}_{\text{Nosé}} = \sum_{i=1}^N \frac{1}{2} m_i \left( s \frac{dr_i}{dt} \right)^2 - U(r^N) + \frac{1}{2} Q \left( \frac{ds}{dt} \right)^2 - \frac{3N}{\beta} \ln s \quad (2.75)$$

where  $\beta = \frac{1}{kT}$ ,  $m$  is the mass of particle  $i$  and  $Q$  is an effective mass related to the additional variable  $s$ . Considering the momentum conjugate of  $r_i$  and  $s$  which is defined respectively as :

$$p_i = \frac{\partial \mathcal{L}}{\partial r_i} = m_i s^2 \frac{dr_i}{dt} \quad (2.76)$$

$$p_s = \frac{\partial \mathcal{L}}{\partial \frac{ds}{dt}} = Q \frac{ds}{dt}, \quad (2.77)$$

the Hamiltonian of the system plus one extended variable can be expressed as:

$$\mathcal{H}_{Nosé} = \sum_{i=1}^N \frac{p_i^2}{2m_i s^2} + U(r^N) + \frac{p_s^2}{2Q} + \frac{3N \ln s}{\beta}. \quad (2.78)$$

Hereafter, the real variables are marked with prime ( $r'$ ,  $p'$ ,  $s'$ ,  $t'$ ) to distinguish them from virtual heat bath variables ( $r$ ,  $p$ ,  $s$ ,  $t$ ). The relationships between the real and virtual variables are then defined as:

$$\begin{aligned} r' &= r, \\ p' &= \frac{p}{s}, \\ s' &= s, \\ dt' &= \frac{dt}{s}, \end{aligned} \quad (2.79)$$

then, equation of motions with respect to the real variables are written as:

$$\frac{dr'_i}{dt'} = s \frac{dr_i}{dt} = \frac{p_i}{m_i s} = \frac{p'_i}{m_i}, \quad (2.80)$$

$$\frac{dp'_i}{dt'} = s \frac{d(\frac{p_i}{s})}{dt} = \frac{dp_i}{dt} - \frac{p_i}{s} \frac{ds}{dt} = -\frac{\partial U(r'^N)}{\partial r'_i} - \frac{s' p'_s}{Q} p'_i, \quad (2.81)$$

$$\frac{1}{s} \frac{ds'}{dt'} = \frac{s}{s} \frac{ds}{dt} = \frac{s' p'_s}{Q}, \quad (2.82)$$

$$\frac{d(s' \frac{p'_s}{Q})}{dt'} = \frac{s}{Q} \frac{dp_s}{dt} = \frac{1}{Q} \left( \sum_{i=1}^N \frac{(p'_i)^2}{m_i} - \frac{3N}{\beta} \right), \quad (2.83)$$

The above equations of motion become simpler by the definition of thermodynamic friction coefficient ( $\xi = \frac{s' p'_s}{Q}$ ) which was introduced by Hoover:

$$\frac{dr_i}{dt} = \frac{p_i}{m_i}, \quad (2.84)$$

$$\frac{dp_i}{dt} = -\frac{\partial U(r^N)}{\partial r_i} - \xi p_i, \quad (2.85)$$

$$\frac{d\xi}{dt} = \frac{1}{Q} \left( \sum_{i=1}^N \frac{(p_i)^2}{m_i} - \frac{3N}{\beta} \right), \quad (2.86)$$

$$\frac{1}{s} \frac{ds}{dt} = \frac{d \ln s}{dt} = \xi. \quad (2.87)$$

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Finally, the Nosé-Hoover Hamiltonian for an extended system can be written as:

$$\mathcal{H}_{\text{Nosé-Hoover}} = \sum_{i=1}^N \frac{p_i^2}{2m_i} + U(r^N) + \frac{\xi^2 Q}{2} + \frac{3N}{\beta} \ln s, \quad (2.88)$$

where, the total energy  $\mathcal{H}_{\text{Nosé-Hoover}}$  is conserved.

### 2.4.7 Radial distribution function

The radial distribution function (*rdf* or  $g(r)$ ) is a valuable tool to evaluate the spatial distribution of particles around a reference particle. Essentially, *rdf* reveals the probability of finding a particle at a certain distance from another particle [230]. Depending on the simulated system in molecular dynamics, *rdf* applied to an atom, molecule, or molecular clusters. Widely used in molecular dynamics simulations, the radial distribution function provides valuable information such as insight into particle interaction potentials [231], structure analysis [232], molecular orientation [233] and more. To compute  $g(r)$  for a given reference particle  $i$  within a fluid system, the distribution of other particles (such as  $j$ ) is determined relative to  $i$ . However, this distribution requires statistical averaging due to varying positions experienced by fluid atoms, defined by:

$$g(r) = \frac{\langle \rho(r) \rangle}{\rho_v}, \quad (2.89)$$

where  $r = |r_i - r_j|$  and  $\rho_v$  is number density of particle  $i$  within volume  $4\pi r^2 dr$ . In this dissertation, *rdf* is used to calculate the solvation shell around mono/divalent ions.

### 2.4.8 Energy minimization

In mathematics for a multivariate function like  $f$  that depends on multiple independent variables  $x_i \in \{x_1, x_2, \dots, x_n\}$ , minimization refers to determining a set of these independent variables at which  $f$  reaches its minimum value, that is:

$$\frac{\partial f}{\partial x_i} = 0 \quad (2.90a)$$

$$\frac{\partial^2 f}{\partial x_i^2} > 0. \quad (2.90b)$$

In molecular dynamics, the initial configuration of a simulated system might not necessarily correspond to an optimized conformation in terms of energy. Thus, energy minimization is carried out to discover a configuration for the simulated system that matches an optimized conformation. The objective of energy minimization is to identify a local minimum within the energy landscape.

This algorithm iteratively adjusts the position of each particle  $r$  to minimize the potential energy function  $U(r)$ . Mathematically, the set of the positions  $r^*$  minimizing  $U(r)$  is shown as [234, 235]:

$$r^* = \underset{r}{\operatorname{argmin}} U(r). \quad (2.91)$$

This optimization technique utilizes various algorithms such as gradient descent and conjugate gradient methods to modify particle positions until arriving at a local minimum in the potential energy landscape. The resulting configuration ideally represents a stable conformation or a minimum energy state for the simulated system. [236, 237]. In this Ph.D. thesis, energy minimization is carried out initially in each simulation to ensure that the system is free from steric clashes or improper geometry. This step helps relaxing the structure while gradually ramping up the temperature.

## 2.5 Material and geometry

The main materials utilized in this study involve calcite, representing the surface of the mineral, and water, which mimics the fluid phase. Water interacts directly with calcite and also serves as a solvent, including mono- and divalent ions. The objective of this section is to provide an elaborate description of the calcite and water used in molecular dynamics simulations.

### 2.5.1 Hexagonal indices

In crystallography, the structure of a crystal is expressed based on the spatial arrangement of its atoms, each occupying a specific point in a three-dimensional Cartesian coordinate system. Thus, each point of a crystal lattice can be represented by a linear combination of primitive lattice vectors such as:

$$\mathbf{R} = n_1 \mathbf{a} + n_2 \mathbf{b} + n_3 \mathbf{c}, \quad (2.92)$$

where,  $n_1, n_2$  and  $n_3$  are integer numbers which are multiplied by linearly independent lattice vectors  $\mathbf{a}$ ,  $\mathbf{b}$  and  $\mathbf{c}$ . Miller indices, shown by  $(hkl)$ , represent the planes where the crystal axes intersect at points  $\frac{\mathbf{a}}{h}$ ,  $\frac{\mathbf{b}}{k}$  and  $\frac{\mathbf{c}}{l}$ . Essentially, Miller indices  $(hkl)$  are integer numbers that indicate planes orthogonal to reciprocal lattice vectors, defined as:

$$\mathbf{r}_{hkl} = h\mathbf{a}^* + k\mathbf{b}^* + l\mathbf{c}^*, \quad (2.93)$$

where,  $\mathbf{a} \cdot \mathbf{a}^* = 0$ ,  $\mathbf{b} \cdot \mathbf{b}^* = 0$  and  $\mathbf{c} \cdot \mathbf{c}^*$  represent orthogonality between lattice vectors and their Miller counterparts. However, for the hexagonal and rhombohedral lattice structure, an additional index, denoted as  $i$ , is introduced to aid in distinguishing between crystal planes more effectively. The relation between the index  $i$  and other Miller indices is defined as:

$$i = -(h + k). \quad (2.94)$$

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Calcite has a rhombohedral structure [238] and its crystal structure can be defined by hexagonal indices ( $hkl$ ). The unit cell of calcite is identified by  $a = b = 4.990\text{\AA}$  and  $c = 17.061\text{\AA}$ ,  $\alpha = \beta = 90^\circ$  and  $\gamma = 120^\circ$  [239]. Figure 2.13 depicts the rhombohedral structure of the calcite unit cell.

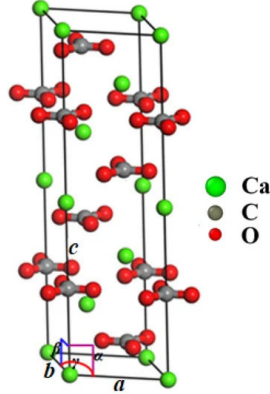


Figure 2.13: Illustration of rhombohedral structure of calcite unit cell [240]

### 2.5.2 Calcite neutral plane

Calcite can be analyzed across various crystallographic planes, each characterized by specific molecular structures. For example, cleaving calcite along planes like  $(1000)$  and  $(10\bar{1}1)$  results in surfaces terminated by either calcium (Ca-terminated plane) or carbonate ( $\text{CO}_3^{2-}$ -terminated plane). This cleavage generates dipoles, highlighting the diverse termination points within the crystal structure. Conversely, cleaving along  $(10\bar{1}4)$  plane provides a smooth and neutral surface. Moreover, various cleaved planes exhibit varying surface energies, depending on the molecular configuration formed on the cleaved surface. This variability in surface energies among different planes underscores the diverse stability associated with each crystallographic surface in calcite. Among various calcite planes, the  $(10\bar{1}4)$  emerges as the most stable, exhibiting consistently low surface energy in both hydrated and unhydrated conditions. The remarkable stability of the  $(10\bar{1}4)$  plane has been confirmed experimentally with Atomic Force Microscopy [241] and scanning electron microscopy (SEM) [242]. Simultaneously, theoretical studies confirm stability of  $(10\bar{1}4)$  plane [243–245] in terms of surface energy. Table 2.1 illustrates a comparative analysis of surface energy across various calcite crystallographic planes. Figure 2.14 depicts side views of various calcite crystallographic planes: (a)  $(0001)$ , (b)  $(1000)$ , (c)  $(1120)$ , (d)  $(1011)$ , and (e)  $(1014)$  [246].

In this Ph.D. thesis, the cleavage plane chosen for calcite is the  $(10\bar{1}4)$  plane, identified as the most stable surface under ambient conditions [241, 244]. The  $(10\bar{1}4)$  plane includes  $\text{Ca}^{2+}$  and  $\text{CO}_3^{2-}$  atoms that form a charge-neutral surface.



Table 2.1: Comparative analysis of surface energies across various calcite crystallographic planes

Calcite plane	$(\frac{J}{m^2})$ [79]	$(\frac{J}{m^2})$ [83]	$(\frac{J}{m^2})$ [84]	$(\frac{J}{m^2})$ [85]
(10 $\bar{1}$ 4)	0.86	0.23	0.60	0.59
(0001)Ca	1.44	1.6	0.97	0.97
(0001)CO <sub>3</sub>	1.44	1.6	0.99	0.99
(10 $\bar{1}$ 0)	1.37	0.52	1.59	0.97
(10 $\bar{1}$ 1)Ca	1.49	-	1.03	1.23
(10 $\bar{1}$ 1)CO <sub>3</sub>	1.49	-	1.08	1.14
(11 $\bar{2}$ 0)	1.66	0.5	1.43	1.39

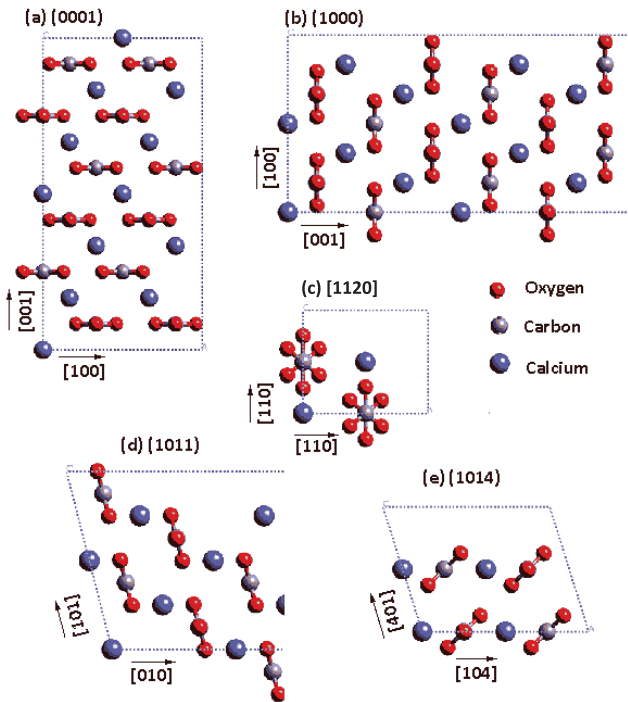


Figure 2.14: Side views of different calcite cleaved planes: (a) (0001), (b) (1000), (c) (1120), (d) (1011), and (e) (1014). The planes (0001) and (1011) are depicted with a doubled unit cell along  $a$  direction, as the dipole perpendicular to the slab has been removed. Figure adapted from [246]

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However, cleaving along alternate planes results in surfaces terminated either by a layer of calcium ions or by carbonate ions, consequently yielding surfaces with positive or negative charges. These polar surfaces tend to adsorb ions or undergo reconstruction to eliminate dipole moments, rendering them unstable.

### 2.5.3 Potential models for water

Water has been extensively studied and remains a focal point in scientific literature due to its importance and complexity. The primary focus in theoretical investigations since the advent of molecular simulations has been to define the force field of water, describing the natural characteristics of water. Numerous potential models have emerged based on experimental data and quantum mechanical calculations [247, 248], exhibiting different performances [249, 250]. The most widely used water models are classical potentials, known for being rigid and non-polarized, including SPC [251], SPC/E [252] and transferable interatomic potential series like TIP3P [253], TIP4P [254] and TIP5P [255]. There exist flexible models (i.e., flexible bond lengths, bond angles, and dihedral angles) and polarizable models, capable of altering the electron-cloud distribution. Some of these models include AIMD1 [256], AIMD2 [257], QM-4MM [258], QM-4TIP5P [258] and QM-230TIP5P [259]. These models are specifically designed to account for the dynamic nature of water molecules.

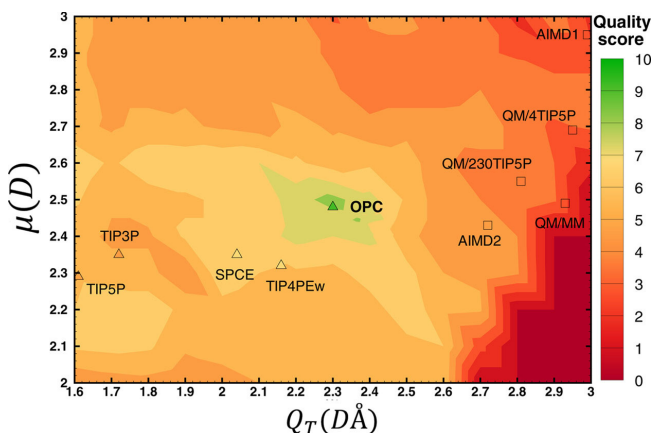


Figure 2.15: Assessment of different water models capability to account dipole ( $\mu$ ) and quadrupole ( $Q_T$ ) moments. Adjusting the charge distribution in three- and four-point classical models (OPC) yields promising results [260]

In a comprehensive study conducted by Izadi et al. [260], various water models, ranging from classical to flexible polarized, were investigated. The evaluation focused on the ability of different models to capture dipole ( $\mu$ ) and quadrupole ( $Q_T$ ) moments, as these two electrostatic moments have a strong effect on the liquid phase structure of water and its diagram behavior [258,

261–263]. The results indicate that the models that incorporate flexibility and polarization based on quantum mechanics scored relatively low, as illustrated in Figure 2.15. Nonetheless, improving the charge distribution in the three- and four-point models (Optimal Point Charge or OPC) led to improved outcomes. This implies that despite extensive efforts to assess classical rigid water models, there is still considerable room for improvement. Moreover, while polarizable models are considerably more computationally expensive [264], they do not consistently offer higher accuracy compared to classical models. Thus, the selection of water models should prioritize accuracy in reproducing specific properties. The water models utilized in this Ph.D. thesis are SPC/E [252], SPCE/FW [252] and TIP3P [253]. These three-point models were chosen due to their high accuracy in predicting the density and low computational cost.

## 2.5.4 Potentials for mono/divalent ions

In an earlier section (1.3), it was explained that within subsurface reservoirs, the adsorption of polar components found in oil on the surface of carbonate rock leads to the development of an oil-wet behavior in carbonate rock. [265], while calcite naturally exhibits hydrophilic characteristics. On the other hand, when aqueous phases containing mono/divalent ions, commonly referred to as brine water, are introduced to oil-wet rock, it leads to the detachment of oil. Namely, introducing brine water into an oil-wet system allows the carbonate rock surface to revert to a hydrophilic state. This phenomenon was initially introduced a long time ago [266, 267], evolving and gaining further understanding over time [268–270]. This approach serves as the foundation for a technology known as smart water flooding, which has the potential to significantly increase the total oil recovery up to 50-70% [72]. However, conventional methods generally allow the extraction of only 30-35% [271] of the hydrocarbons available in the reservoir.

Despite the extensive effort made to understand the physical and chemical processes involved in smart water flooding within carbonate reservoirs [272–274] and numerous mechanisms interpreting this phenomena from different angles [275–278], there is still a gap in exploring the molecular interactions among carbonate rock, crude oil and brine water. This Ph.D. thesis also aims to shed light on some molecular aspects of the interactions among calcite, crude oil and brine water within subsurface carbonate reservoirs. To achieve this goal, I utilized molecular dynamics simulation, providing high-resolution insights into the phenomenon across both time and space. Within this framework, two distinct compositions of brine water, along with crude oil, were introduced to interact with a calcite slab. Formation water (FW) comprising  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{Ca}^{2+}$  and low saline water (LSW) containing  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  were used as brine water in molecular dynamics simulations. However, crude oil composed of Toluene, Decane, and Benzoic acid served as a representative of crude oil. Different potentials are utilized to model interatomic interactions in the aqueous phases and crude oil. The interatomic potentials for  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{Ca}^{2+}$  are defined using Optimized Potentials for Liquid Simulations-All-Atom (OPLS-AA) [279], while the potential proposed by Williams et al. [280] controls

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the interatomic potentials for  $\text{SO}_4^{2-}$ . Additionally, the interactions between the oil components are modeled by OPLS-AA [279].

## Chapter 3

# Summary of papers and outlook for future works

This chapter summarizes the articles that contribute to the main research topic outlined in Chapter 1. This Ph.D. thesis includes three articles where I am the first author. The papers and proceedings are attached at the end of the thesis in chronological order. I wrote the papers and performed simulations using SAFT and molecular dynamics, which involved coding, simulations, data collection, and visualizations. My supervisors and co-authors provided input to the articles through discussions and added their comments before submission of the article and during the journal review process.

In-house models and equations of state based on Statistical Association Fluid Theory (SAFT) and Perturbed-Chain Statistical Association Fluid Theory (PC-SAFT) have been developed for some years at the Department of Geosciences, University of Oslo [281–284]. The former model was developed with the FORTRAN programming language, and the latter model was developed in the MATLAB environment. These two in-house models are currently under continuous development and advancement. Before starting this Ph.D. project, the SAFT equation of state had been applied to various studies such as (a) using the SAFT1 equation of state to predict the phase behavior and estimate the density of the aqueous phase in a ternary mixture consisting of  $\text{CO}_2$ - $\text{SO}_2$ - $\text{H}_2\text{O}$  across a wide range of temperatures and pressures [281], and (b) using SAFT1-RPM to predict the properties of a quaternary mixture consisting of  $\text{CH}_4$ - $\text{CO}_2$ - $\text{H}_2\text{O}$ - $\text{NaCl}$ , incorporating Coulombic and polar forces [282]. The PC-SAFT model had also been utilized for two different projects prior to this Ph.D. A project predicting the phase behavior of asphaltene in crude oil [283] and one predicting the phase behavior of  $\text{CO}_2$  interacting with brine water ( $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$ ) [284]. Furthermore, some extensions of PC-SAFT had been integrated into the Matlab Reservoir Simulation Toolbox (MRST) [285, 286].

This Ph.D. work systematically explores the molecular aspects of the rock-fluid interface. The first part involves developing a tool to predict the macroscopic behavior of confined fluids influenced by solid minerals by examining molecular interactions at the nanoscale. This is achieved through the development of a thermodynamic model based on the SAFT framework, with relevant parameters computed through molecular dynamics simulations. Papers I and II tackle the topic of one- and two-dimensional confinements, respectively. In particular, both papers employ pure water to mimic the confined fluid, with the calcite 10 $\bar{1}$ 4 plane serving as the nanoscale slab. Paper I adopts PC-SAFT for one-dimensional confinement, while Paper II employs SAFT2 for two-dimensional confinement. To the best of our knowledge, this is the first time that equations of state inspired

### 3. Summary of papers and outlook for future works

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by the SAFT framework have been developed to systematically consider the impact of solid confinement on the properties of a confined fluid. In a subsequent part of the Ph.D., molecular dynamics simulations were used to investigate the rock-oil-brine interface. In line with the rock-fluid interface, in Paper III, I investigated the rock-oil-brine interface to gain a comprehensive understanding of molecular interactions through molecular dynamics simulations. Although there are numerous mechanisms to interpret the consequences of smart water flooding (i.e., injection of low-salinity water during oil recovery), many lack microscopic examinations. Understanding the oil displacement process during smart water injection requires consideration of both macroscopic observations and microscopic mechanisms. In this study, the molecular dynamics simulation setup includes aqueous water (water + mono/divalent ions), oil (Toluene + Decane + Benzoic acid) and the calcite neutral plane ( $10\bar{1}4$ ) to study the rock-oil-brine interface at the molecular scale. The molecular insights gained from this work may pave the way for future improvements in smart water flooding, a widely used technique in enhanced oil recovery (EOR). The summary of the articles and key findings are described in the following sections.

#### 3.1 Development of PC-SAFT for one-dimensional confinement

##### 3.1.1 Paper I:

Extension of PC-SAFT Equation of State to Include Mineral Surface Effect in Fluid Properties Using Molecular Dynamics Simulation

This paper uses the capability of PC-SAFT equation of state (EoS) to quantify the effect of carbonate rock on the physicochemical properties of a fluid confined at the mineral-fluid interface. Molecular dynamics simulations were employed to compute confinement parameters (section 2.3.5) necessary for the execution of PC-SAFT. Although PC-SAFT displays promise in modeling associating and polar fluids at a bulk scale, it has not yet addressed the impact of mineral confinement on fluid properties. This study develops PC-SAFT to determine the properties of water confined at the  $10\bar{1}4$  calcite interface.

##### 3.1.2 My contribution

Previous versions of PC-SAFT models before this Ph.D. project overlooked the effect of mineral confinement on fluid properties, treating both bulk and confined fluids similarly with identical parameters for the Helmholtz free energy. However, under confinement, the molecular arrangement of fluids differs on the basis of the governing thermodynamic conditions, chemistry, and the size of the mineral confinement. These variations determine the deviation of fluid properties from those observed in bulk. In this study, I used the MATLAB environment to incorporate the effect of solid calcite into the water properties using the PC-SAFT equation of state. The required confinement parameters were then

computed with the molecular dynamics simulations. For conducting molecular dynamics simulations, I used LAMMPS which is the classical molecular dynamic program from Sandia National Laboratories.

### 3.1.3 Method

To study the effect of confinement on fluid properties, a simulation domain was established including a calcite nanoslab and water. Calcite is dominant in carbonate reservoirs, and water is a known associating fluid found in the crude oil composition. Within the established setup, a calcite nanoslab was introduced into water along the  $z$ -axis from one side, serving as a suitable starting point to evaluate our novel approach.

After adjusting the setup, the next step involved defining new parameters for PC-SAFT to enable its distinction between confined water and bulk water. To derive the geometrical parameters necessary for this distinction, the approach outlined by Travalloni et al. [202] was utilized. Then, along with the previous developments for PC-SAFT, a code was developed within the MATLAB environment to define confinement parameters and Helmholtz free energy, specifically addressing the interactions between calcite and water. The new Helmholtz free energy is derived as a function of the confinement parameters, which need to be calculated for the successful execution of PC-SAFT. Calculating these confinement parameters was achieved through molecular dynamics simulation conducted for different water thicknesses at different temperatures.

### 3.1.4 Key findings

After collecting data from molecular dynamics simulations, the density and energy profiles of water were plotted along the  $z$ -axis at different temperatures and thicknesses of water. In the subsequent stage, the outcomes of the newly developed PC-SAFT model were compared with the results of molecular dynamics for Region II (layering zone). The following are the key findings of the work:

- The general perspective of the water density and energy profiles shows that both profiles start from zero at the calcite surface (Region III) and experience some large peaks within layering zone (Region II) and then stabilize in bulk-like zone (Region I). Different regions are marked in the density profiles depicted in Figure 3.1. Details of each region are also described in Figure 2.8.
- On closer examination, it becomes apparent that maintaining a fixed water thickness while increasing the temperature leads to a lower average density within both the layering zone and the bulk-like zone. Furthermore, maintaining a constant temperature while increasing the water thickness results in a higher average density within both Regions I and II.

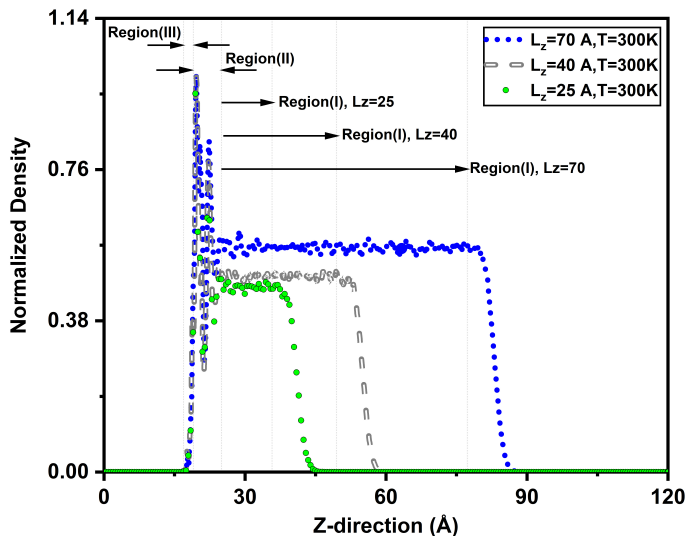


Figure 3.1: Illustration of the density profile within region I and II at different  $L_z$  and  $T=300$  K. The density is normalized between 0 and 1, which allows comparing the average density trends. The greatest and lowest average densities occur at  $L_z = 70$  Å and  $L_z = 25$  Å, respectively [201].

- It is a promising alignment between the PC-SAFT modeling and the molecular dynamics findings. Namely, maintaining a constant water thickness while increasing the temperature leads to a decrease in the average density within Region II. Conversely, maintaining a constant temperature while increasing the thickness of the water results in an elevated average density within Region II.
- Comparison between PC-SAFT and molecular dynamics simulations indicates that the relative error increases with the growth of water thickness at a constant temperature. Similarly, the relative error increases with increasing temperature at a constant water thickness.

## 3.2 Development of SAFT for two-dimensional confinement

### 3.2.1 Paper II:

Extension of SAFT Equation of State for Fluids Confined in Nano-Pores of Sedimentary Rocks Using Molecular Dynamics Simulation



This paper demonstrates how SAFT2 EoS effectively captures the long-range interactions of calcite nanoslabs from opposing sides, affecting the macroscopic behavior of confined water. Calculating the confinement parameters required for SAFT2 execution is performed through molecular dynamics simulations. As two hydrophilic calcite nanoslabs begin competing to attract water molecules, this interaction results in unique deviations in water properties owing to the interplay of non-homogeneous attractions from both sides.

### 3.2.2 My contribution:

Previous studies before this Ph.D. project had utilized SAFT1 and SAFT1-RPM to investigate the phase behavior of aqueous solutions and electrolytes under reservoir pressure and temperature conditions, overlooking the possible influence of mineral confinement on the properties of the confined fluid. The previous approach in Paper I introduced a calcite wall on one side, emphasizing the calcite-water interaction on that side, while assuming water-water interactions approach bulk interactions on the opposite end. However, Paper II focuses on water confined within a two-dimensional confinement. To address this, a new framework of SAFT is required to consider the amplified attraction arising from opposing walls across a longer range, compared with that of Paper I. Put it differently, this novel model should capture the long-range interactions between hydrophilic calcite slabs and water. Therefore, SAFT2 [287, 288] was chosen as the suitable framework for development, due to its improved square-well width ( $\lambda$ ), enabling it to effectively model long-range interactions. Furthermore, given that SAFT2 was specifically designed to model multivalent ions, it could serve as a suitable platform for future developments, potentially adapting it to simulate the interaction between rock, oil and brine water. Finally, the new SAFT2 formalism was coded in the FORTRAN language and integrated into the existing SAFT model. The required confinement parameters were calculated by molecular dynamics simulations, conducted with the package LAMMPS.

### 3.2.3 Method:

I established a setup in which water is encapsulated within two calcite nanoslabs cleaved along the (10 $\bar{1}$ 4) plane. Adding the effect of two-dimensional confinement to the SAFT2 equation of states involves a two-step process i) to calculate the confinement parameters; and ii) to develop the Helmholtz free energy. Both may vary depending on the thermodynamic conditions and confinement size. In fact, the Helmholtz free energy is a function of confinement parameters, which will be determined through molecular dynamics simulations for various pore sizes and under different thermodynamic conditions.

### 3.2.4 Key findings:

After the molecular dynamics results were collected, the density and energy profiles of encapsulated water were plotted with respect to the width of the

### 3. Summary of papers and outlook for future works

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calcite nanopore at different temperatures. The following are the key findings:

- In each density and energy plot, three distinct regions become apparent. Closest to the calcite surface on both sides lies Region III (forbidden zone), where both plots register zero values. Moving outward, Region II (layering zone) shows prominent peaks, indicating the structured water layers adsorbed onto the surface of calcite nanoslabs. The density and energy trends from both sides converge in the middle, forming the boundaries of Region I (bulk-like zone). Figure 3.2 represents the molecular visualization of water molecule arrangements along with relevant density profiles within different regions. More descriptions are provided in Figure 2.6.
- Density profiles, plotted for Region II (layering zone) and Region I (bulk-like zone), respectively, showing distinct behaviors. In the bulk-like zone, where the pore size is kept constant, the density decreases with rising temperature, resembling the behavior of bulk water. This trend implies that the density within Region I is predominantly governed by water-water interactions, as higher temperatures lead to an increased distance between water molecules, resulting in lower density.
- On the contrary, within the layering zone, an increase in temperature results in a larger density. This observation can be interpreted as water molecules inside Region I form a more dense network compared to those in Region II. As the temperature rises the distance between water molecules in the bulk-like zone increases, expanding the water network. Thus, some water molecules move into the empty cavities formed in Region II. To be specific, the existing gaps between adsorbed water molecules are filled with newly introduced ones, leading to higher density values at high temperature.
- At a constant temperature, as the pore size grows, the average density within the layering zone and central zone rises. The density within the bulk-like zone rises as the widening pore approaches conditions similar to bulk water. Additionally, the increase within the layering zone is attributed to the strengthening of water-water interactions, which compete with the calcite-water interactions. Therefore, the increase in pore size results in a higher average density both within the layering zone and within the bulk-like zone.
- At a constant temperature, a unique characteristic is evident in the density profile as the pore size decreases and reaches  $L_z = 1.5$  nm. This deviation is attributed to the overlapping attraction potentials from both walls, specifically in terms of the calcite-water interaction. For  $L_z = 1.5$  nm, water molecules experience a significantly confined space in the central zone, intensifying calcite-water interactions in comparison to water-water interactions. Thus, the water molecules inside the central zone are predominantly influenced by the porewall attractions on both sides.

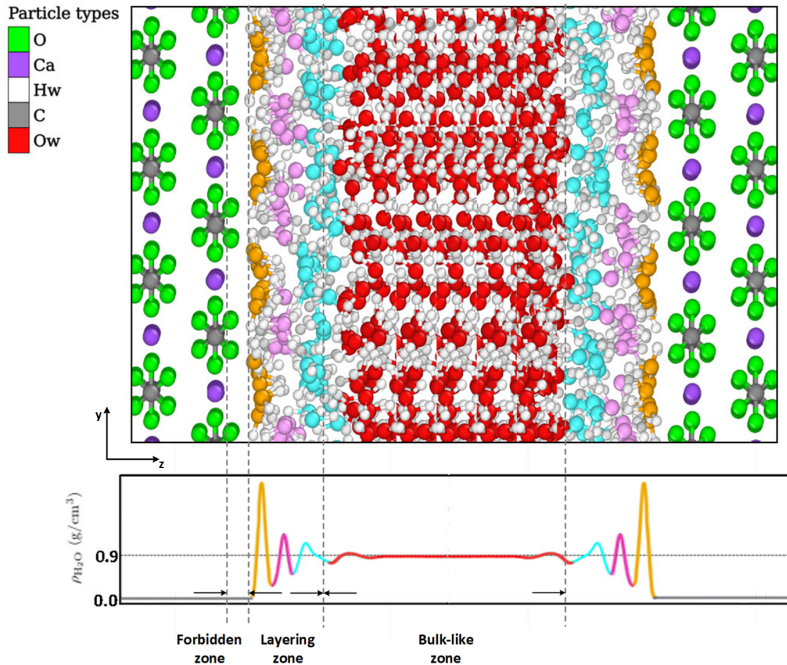


Figure 3.2: Cross-sectional view of the calcite-water-calcite system. Water atoms are colored by red (oxygen) and white (hydrogen). Within the calcite structure, carbon, oxygen and calcium atoms are gray, green and purple, respectively. The colors of oxygen atoms in the three layers seen from the calcite surface are orange, pink, and turquoise, respectively. To the bottom, the water density is plotted along  $z$ -axis, with line segments colored after the layer number. Ovito was used for visualization.

- The SAFT2 results were compared with molecular dynamics, revealing a good agreement at high temperature ( $T = 400$  and  $450$  K). However, there is a noticeable increase in the absolute relative error at low temperatures. To address this issue, a new CF parameter was introduced. CF is defined as the fraction representing the density ratio within Region II and I, denoted as  $\frac{\rho_{RegionII}}{\rho_{RegionI}}$ . The introduced CF is aimed to enhance the alignment between molecular dynamics and SAFT2 simulations for low temperatures.

## 3.3 Underlying mechanisms driving smart water flooding

### 3.3.1 Paper III:

Drivers of Low-Salinity Effect in Carbonate Reservoirs Using Molecular Dynamics Simulations

This paper investigates the molecular aspects of low-salinity water (LSW) injection, an effective technique in enhanced oil recovery (EOR). The findings of this study contribute to better understand the effective mechanisms governing oil displacement after injection of low-salinity water into the rock-brine-oil system.

### 3.3.2 My contribution

Despite the proven success of low-salinity water injection, the fundamental mechanism driving oil displacement within the rock-brine-oil system remains uncertain. The challenge lies in connecting macroscopic observations with molecular scale mechanisms. To address this challenge, a suitable tool is required to examine the rock-oil-brine interface at the molecular scale. In this regard, molecular dynamics simulation is chosen as a computational tool to generate high resolution data in terms of time and space. In this study, in addition to 1014 plane of calcite as a solid phase, three different fluid layers are modeled to mimic the rock-oil-brine interface. To be specific, I modeled two layers of brine water, one with higher salinity referred to as formation water (FW) and the other with lower salinity, named low salinity water (LSW). Additionally, an oil layer was modeled, consisting of hydrocarbon, aromatic and resin components. These simulated fluid layers were mounted above the 1014 surface of nanoslab calcite. The molecular dynamics simulations in this study were conducted with LAMMPS.

### 3.3.3 Method

In the simulation box, I configured a setup, including calcite nanoslab with a thickness of 16.7 Å positioned at the bottom. Directly above the calcite, there is a 5 Å thick layer of formation water consisting of H<sub>2</sub>O, Na<sup>+</sup>, Cl<sup>-</sup>, and Ca<sup>2+</sup>. Above this, a 10 Å wide layer of oil is placed. Lastly, the uppermost fluid in the simulation box is a 20 Å thick layer of low saline water, composed of H<sub>2</sub>O, Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup>, and SO<sub>4</sub><sup>2-</sup>, situated above the oil layer. It is essential to note that the brine water data was selected from experimental results reported by Zhang and Sarma [289], while the oil composition was derived from the SARA test, including toluene (37%), decane (44.7 %) and benzoic acid (18.3%). All molecular dynamics simulations were conducted using LAMMPS.

### 3.3.4 Key findings

In order to explore the preference of various species for settling on a thin calcite-brine film, the density profiles of different ions and water along the *z*-axis were

plotted. Following the data collection from molecular dynamics simulations:

- The profile of water density explicitly illustrates the adsorption of two water monolayers onto the calcite surface.
- Following the water monolayers, density profiles of monovalent ions are observed. The peak of  $\text{Na}^+$  ions was found within the adsorbed water layers, whereas the peak of  $\text{Cl}^-$  ions appeared after the adsorbed water layers.
- The density profiles of the divalent ions including  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ , and  $\text{SO}_4^{2-}$  exhibit a peak farther from the calcite surface, immediately following the monovalent ions.
- The radial distribution functions plotted for different ions show that all mono- and divalent ions are hydrated with respective diameters of 2.45 Å, 2.35 Å, 1.95 Å, 2.35 Å and 1.75 Å for  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$ ,  $\text{SO}_4^{2-}$ .
- Analysis of the brine water density profile in different time steps and temperatures indicates that at  $T=300$  K, the oil displacement occurs gradually in two distinct steps. On the contrary, at  $T = 360$  K, the transition occurs immediately, complete with the detachment in a single step. More precisely, the initiation of the transition at  $T = 300$  K is delayed, while at  $T = 360$  K, it has a shorter duration.
- The dynamics of different ions shows distinct behaviors. Monovalent ions ( $\text{Na}^+, \text{Cl}^-$ ) settle within compact water layers on the calcite surface, while divalent ions exhibit varied movements. Initially,  $\text{Ca}^{2+}$  ions are close to the surface and migrate away over time, whereas  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ , initially distant, move closer to the calcite surface, following oil displacement. Figure 3.3 illustrates the arrangement of  $\text{Na}^+$  and  $\text{Cl}^-$  above the calcite surface, leading to the displacement of the oil layer.
- Examining the charge density profile at different time steps and temperatures reveals large oscillation trends near the calcite surface, indicating the formation of an electrical double layer (EDL) immediately after the calcite surface.
- As long as the oil layer adheres to the calcite-brine interface, the electrical double layer profile remains zero across the oil phase. The observed discontinuity between the head and tail of the charge density profile, where the charge density trend reaches zero, underscores that neither mono- nor divalent ions diffuse into the organic components of the oil layer.
- Over time, the discontinuity in the charge density profile is compensated by detachment of the oil layer from the calcite-brine interface. More precisely, the detachment of the oil occurs concurrently with the bridging of the gap in the charge density profile.

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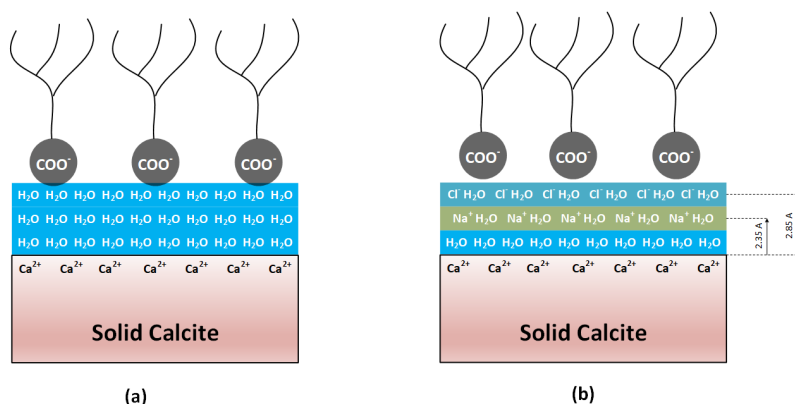


Figure 3.3: The sketch depicts settlement of Na<sup>+</sup> and Cl<sup>-</sup> in close proximity to the surface, resulting in the formation of a double electrical layer. In (a) black balls represent benzoic acid in the oil layer adhere to the calcite surface via formation water. In (b) the oil layer separates from surface after Na<sup>+</sup> and Cl<sup>-</sup> have settled.

- Similar to the trends observed in the density profile, at T=360 K, the gap in the charge density profile is filled more rapidly than at T=300 K. This gap compensation explicitly indicates oil detachment from the calcite-brine interface, which experiences a delay at T=300 K compared to T=360 K.
- Upon analysis of the results, it is apparent that there is minimal change in the positions of Na<sup>+</sup>, Cl<sup>-</sup> and H<sub>2</sub>O with temperature variations. On the contrary, the positions of Mg<sup>2+</sup>, Ca<sup>2+</sup>, and SO<sub>4</sub><sup>2-</sup> exhibit variations with temperature, indicating a dynamic response to changes in temperature.

### 3.4 Conclusions

The interfaces between rocks and fluids are pivotal in determining the reactivity and fate of fluids confined within subsurface reservoirs and aquifers. Understanding the complex nature of these interfaces requires a comprehensive study of the relationship between macroscopic observations and molecular interactions, as explored partly in this Ph.D. thesis. This complexity is due to the dynamic behavior of the rock-fluid interface across time and space, which closely links chemical reactions, species transport, and the physicochemical properties of both rocks and fluids.

One example that illustrates the aforementioned complexity is the varying behavior of water when solid calcite is introduced from opposite sides compared to just one side. The distinct nature of the governing interactions at the molecular level prompted the use of the PC-SAFT and SAFT2 models, each employed

to respectively capture diverse attractions induced by the calcite slabs. This methodology proves relevant for quantifying the impact of other minerals on different fluids, although to varying extent.

Furthermore, in the comparison between SAFT-based models and molecular dynamics, a divergence emerges when confined water approaches bulk water properties. This discrepancy exists between the predictions of SAFT-based models and outcomes of molecular dynamics. This analysis suggests that SAFT-based models, tuned to predict the properties of confined water, effectively distinguish between confined and bulk fluids. However, the increased discrepancy at higher temperatures, specifically for the PC-SAFT, may be attributed to the limitations inherent in the PC-SAFT model. To elaborate, molecular dynamics simulations utilize the SPC/E model for water molecules. The decreasing accuracy of this chosen water model with increasing temperature may introduce errors in the PC-SAFT predictions during the computation of confinement parameters. While this limitation may be valid for SAFT2, its impact is likely less pronounced due to a lower threshold of maximum temperature, compared to PC-SAFT.

At the second research topic, the introduction of a correction factor, CF, to improve the alignment between SAFT2 and molecular dynamics results, particularly at low temperatures, highlights that beyond the calcite-water interactions, other factors may control the properties of confined fluid. In other words, at lower temperatures and smaller confinement dimensions, the impact of the confinement constraints is more pronounced. This finding provides a foundation for further exploration into how additional constraints (e.g. geometry of confinement, layering patterns, and the mutual interaction of different regions) impact the characteristics of confined fluids.

Upon comparing the findings of the first and second research, it is evident that the density of confined water remains consistently lower than that of the bulk, regardless of whether it is subject to one- or two-dimensional confinement. However, confinement on one side offers more room for water molecules from a front not exposed to calcite, mitigating the influence of calcite-water interactions. To put it differently, the dual front of calcite-water interactions induced by hydrophilic calcite surfaces, reinforces the calcite-water interactions. This principle remains valid for both layering and bulk-like zones.

Variations in the density of water under confinement underscore the impact of the confinement on accurately predicting the physiochemical properties of the confined fluid. This aspect is often overlooked by commonly used equations of state, employed for the calculation of physiological properties. Consequently, these oversights contribute to inaccuracies in predicting the phase behavior of confined fluid.

In the third research topic, we employed the LAMMPS software to conduct molecular dynamics simulations, aligning with the rock-fluid interface. Our aim was to investigate the mechanisms that influence the detachment of oil from the rock-brine interface during low-salinity water injection. Molecular dynamics simulations, known for their capability to offer high-resolution data, effectively

### 3. Summary of papers and outlook for future works

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capture the early stage interactions occurring at the rock-oil-brine system. We examined how both mono- and divalent ions contribute to the detachment of oil. This was achieved by analyzing the profile of mass density and charge density along with the radial distribution function at different temperatures.

The findings reveal the formation of a hydrate shell around mono- and divalent ions. The first molecules observed above the calcite surface are water molecules, forming structured layers approximately 2 Å away from the calcite surface. Thus, neither mono- nor divalent ions adsorb on the calcite surface directly. In essence, the first water monolayer acts as a bridge between the calcite surface and other ions.

Moreover, divalent ions such as  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ , and  $\text{SO}_4^{2-}$  are located at a greater distance from the calcite surface compared to monovalent ions. This distinctive ordering of mono- and divalent ions above the calcite mineral results from the energy penalty associated with the solvation shell of each ion. This ordering provides compelling evidence of the ions' preference to bind to the calcite surface. Simply put, monovalent ions exhibit a stronger affinity for the calcite surface compared to that of the divalent counterparts, as monovalent ions diffuse into the structured water layers, while divalent ions remain positioned farther from the calcite surface.

It is reasonable to attribute the formation of an electrical double layer to the distribution of monovalent ions above the calcite surface. This association becomes apparent as the development of the electrical double layer coincides with the settling of  $\text{Na}^+$  and  $\text{Cl}^-$  near the calcite surface, at around 2.5 Å. On the contrary, the divalent ions remain at a greater distance, approximately 7-10 Å, and shift their position with temperature. However, the positions of monovalent ions exhibit minimal variation with temperature.

The oil detachment process occurs gradually in a few steps at 5 ns and 10 ns when  $T=300$  K, while it takes place within a single step at 10 ns for  $T=360$  K. This observation can be interpreted as the impact of temperature and kinetic energy on the efficiency of low-salinity water in the separation of the oil layer from the rock-brine interface.

The presence of an oil layer adhering to the rock-brine interface was identified by discontinuity between the head and tail of the charge density profile, as discussed earlier. As time progresses, this gap is simultaneously filled with the displacement of oil. At both  $T = 300$  K and  $T = 360$  K, the bridging of the gap temporally overlaps with the detachment of the oil layer from the rock-brine interface. Thus, the expansion of the electrical double layer coincides temporally with the displacement of the oil layer. The temporal overlap mentioned was also confirmed by the mass density profile. This molecular-scale observation supports the hypothesis suggesting the expansion of the electrical double layer as the main cause of oil detachment from the rock-brine interface.



## 3.5 Outlook

Throughout this Ph.D. work, numerous compelling ideas emerged during meetings and scientific discussions with supervisors and colleagues. These concepts sparked research questions and prompted the need for further research. Despite my interest, time constraints prevented me from delving deeper into many of these interesting concepts. These unexplored ideas stand as a testament to the wide range of research possibilities. Although we are actively working on some ideas, their inclusion in this dissertation awaits completion. As my Ph.D. journey concludes, several promising research avenues will remain unexplored, inviting future exploration and inquiry. Here, I present a list of scientific research topics related to this Ph.D. work that deserve further consideration.

### 3.5.1 Thermodynamic Modeling

In this Ph.D., my focus was on the calcite cleavage surface ( $10\bar{1}4$ ), which is chemically hydrophilic. However, the effect of other minerals (e.g. silicate and clay) and hydrophobic surfaces on confined fluid remains unexplored. Furthermore, it is worth studying other available planes of calcite, each of which has specific characteristics and charge distribution.

We modeled water molecules in liquid state in all case studies mentioned here. It is possible to build a model for the gas phase confined within a nanopore, by adjusting the thermodynamic conditions [290–292]. This model could pave the way for certain environmental challenges, such as storage of  $\text{CO}_2$  and  $\text{H}_2$  in geological formations. Investigating the molecular aspects of rock- $\text{CO}_2$  and rock- $\text{H}_2$  interactions is an essential study that can be conducted using similar techniques presented in this thesis.

A brief review indicates that the literature lacks sufficient attention to a molecular-based equation of state capable of quantifying and predicting the amount of required ions dissolved in low saline water injection [274, 293]. Given the ability of SAFT-based equations of state in modeling ionic solutions and the advances made to incorporate rock effects into confined fluid properties, it would be worth developing an SAFT-based equation of state for predicting the optimized quantity of ions required in low saline water [294–296].

### 3.5.2 Machine Learning: An Alternative to Molecular Dynamics

Molecular simulations like molecular dynamics provide high resolution data that allow the study of different processes at the nanoscale. However, their computational cost remains a challenge [297]. To address this challenge, neural network models can be executed along with MD simulations to learn the trend of molecular dynamics outcomes [298, 299]. Then, the trained network can be used to intra- and extrapolate for margins in which molecular dynamics data is not available. This approach has the potential to save time and cost.

#### 3.5.3 Oil Displacement by Low-Salinity Water Injection

The thickness of the water film placed between the rock surface and the crude oil can determine the oil-wet or water-wet behavior of the rock [300]. A thick water film maintains water-wet conditions, whereas a thin film, prone to instability, may break, leading to the adsorption of polar oil components onto the rock surface. Additionally, the stability of the water film is influenced not only by its thickness but also by the disjoining pressure [301, 302]. Therefore, employing molecular dynamics to investigate the rock-oil-brine system with varying water film thicknesses while simultaneously monitoring the disjoining pressure would be a useful approach.

In our study, temperature displayed dual characteristics. On the one hand, temperature variations influenced the regime of oil detachment and the positioning of divalent ions. On the other hand, changes in temperature had minimal impact on the locations of  $\text{Na}^+$  and  $\text{Cl}^-$  ions in the confined water layer. Further investigations across a broader temperature range are recommended to fully understand the influence of temperature on the efficiency of smart water injection.

Wettability alteration of the carbonate rocks in subsurface reservoirs is dictated by chemistry of mineral surface and interacting fluid both. Regardless of computational cost, it would be worth examining a rock-oil-brine system with different brines interacting with different mineral surfaces.

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# Papers



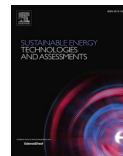
Paper I

# **Extension of PC-SAFT equation of state to include mineral surface effect in fluid properties using molecular dynamics simulation**

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## Extension of PC-SAFT equation of state to include mineral surface effect in fluid properties using molecular dynamic simulation

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### ABSTRACT

In the vicinity of fluid-mineral interfaces a transition zone exist in which the order and packing of the molecules differ from that of the bulk phase where the distribution of intermolecular forces exhibit a more homogenous form. To develop an understanding of the thermodynamic properties in the fluid-mineral interface molecular dynamic (MD) simulation was conducted for the water-calcite system. To predict the water properties near the calcite wall, we have defined a contribution for Helmholtz energy extended from PC-SAFT equation of state (EOS). The new energy contribution depends on the confinement parameters i.e. potential of fluid-wall interaction, confinement degree, bulk density, and fraction of confined molecules estimated by MD simulation. The outcomes of MD simulation exhibit the layering transition of water on the water-calcite interface. In addition, MD simulation confirm the energy deviation within the layering transition zone, where the calcite adsorbs the water molecules. In this approach, the modified PC-SAFT showed a good agreement with MD observations. The results of this study can contribute to a better understanding of fluid behavior at the fluid-mineral interface. In addition, this technique is a valuable tool that can be used to estimate solubility limits in multicomponent fluid processing and pipeline transport.

### Introduction

Energy has a significant role in social and economic developments. As the population grows, the demand for energy consumption increases. To mitigate the environmental impacts of the greenhouse gases, development of renewable energy resources is the prevalent solution. However, achieving the sustainable solutions with low impact on environment is a long-term plan. On the other hand, current renewable supplies are not enough to keep up with the energy demand and the need to traditional energy resources would remain. In order to achieve low carbon intensive systems, optimized methods in thermodynamic assessment of hydrocarbons play a significant role. Improved recovery from oil and gas reservoirs and cost-effective design of downstream facilities requires accurate knowledge of phase behavior and thermodynamic properties [1,2]. Equation of states (EOS) are suitable tools performing the thermodynamic properties calculation and phase behavior analysis. The EOSs define a mathematical relationship between the pressure (P), volume (V) and temperature (T). Then, all thermodynamic properties are computable with known relation between P, V and

T. Most of the EOSs can be classified in three main categories i.e. virial, cubic and molecular-based. The virial EOS of high order are precise enough to cover a wide range of fluid types but they are not efficient because they need a large empirical database for convergence [3]. The most widely used EOSs in engineering applications are cubic EOSs which originally introduced by Van der Waals [4]. The conventional cubic EOSs although predict the behavior of simple components precisely but they suffer from lack of accuracy in describing the complex molecules and mixtures having strong intermolecular forces.

The molecular based EOSs so-called SAFT-type EOSs are constructed based on the statistical associating fluid theory and they formulate dispersive and associative interactions upon Barker-Henderson and Wertheim theories [5,6]. Furthermore, SAFT has shown great success in the simulation of polar fluids with non-ideal intermolecular interactions [7–10].

The interfacial effect between minerals and fluids is a non-ideal interaction and its significant role in thermodynamic modeling has been recognized [11]. On one hand, it is imperative to develop our understanding about fluid-mineral governing interactions for precise assessment of fluid recovery from geological media. On the other hand,

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Nomenclature	
A	Helmholtz free energy [kcal]
a	Intensive Helmholtz free energy [kcal/mol]
$E_{\text{conf}}$	Configurational energy [kcal]
$E_{\text{w}}/k$	Dispersion energy parameter [K]
$F_p$	Local distribution of the molecules inside the interface region
$F_{\text{pr}}$	Fraction of the confined molecules in the square well of interface region
H	Hamiltonian [kcal/mol]
k	Boltzmann constant
$K_E$	Kinetic Energy [kcal/mol]
L	Length of the water bulk mounted above calcite [ $\text{\AA}$ ]
$M_{\text{int}}$	Internal partition function
m	Particle mass [kg]
$m^{\text{seg}}$	Segment number
N	Total number of particles
p	Momentum [kg.m/s]
$P_E$	Potential energy [kcal/mol]
Q	Partition function
r	Position [m]
T	Temperature [K]
V	Volume [ $\text{\AA}^3$ ]
<b>Greek Letters</b>	
$\alpha$	Number of adsorbed water molecules to the calcite surface
$\sigma'$	Segment diameter [ $\text{\AA}$ ]
$\sigma$	Average molecular diameter [ $\text{\AA}$ ]
$\lambda$	Brogie wavelength [ $\text{\AA}$ ]
$\epsilon$	Attractive potential of molecule-wall interaction [kcal/mol]
$\epsilon^{A_i B_i}$	Association energy parameter [K]
$\rho$	Density under confinement [ $\text{kg}/\text{m}^3$ ]
$\kappa^{A_i B_i}$	Association volume
$\delta$	Square well width [ $\text{\AA}$ ]
$\mu$	Chemical potential [kcal/mol]
<b>Subscripts and Superscripts</b>	
ass	Association
conf	Configurational
conf-ff	Configurational due to fluid–fluid interaction
conf-fw	Configurational due to fluid-wall interaction
diss	Dissociation
f	free
ff	Fluid-Fluid
fw	Fluid-Wall
hs	Hard sphere
i,j	counter
int	Internal
max	maximum
z	Z-axis

cubic EOSs are not suitable candidates to capture the molecular interactions of fluid-mineral. In this regard, SAFT-type EOSs with some modifications and tunings are probably able to capture the fluid-rock mutual interactions. However, an experimental data set illustrating fluid-rock interactions is required for such SAFT modifications.

Herein, Molecular Dynamic (MD) simulation is introduced to provide insights on confined fluid properties. This approach considers the simulation outcomes as pseudo experimental data to develop a new model [12]. The molecular simulation inspired by MD is able to simulate the fluid-mineral interface with known chemistry. MD simulations have emerged as a suitable technique to study the interfacial effects in systems containing complex fluids [13]. Recently, the study of fluid-rock interface with MD simulation has gained numerous contributions in the literature [14–16]. Kirch et al. [17] have studied the mutual effect of calcite interface and electrolyte ions (Na, Cl, and Ca) on water structure with MD modeling and Nuclear Magnetic Resonance (NMR). They illustrated that the strong ordering of surface water on calcite interface inhibits the adsorptions of chemical species. Ricci et al. [18] investigated the water-calcite interface with Atomic Force Microscopy (AFM) experiments and MD simulation. With MD simulation, they observed a shorter residence of  $\text{Ca}^{2+}$  ions than  $\text{Na}^+$  ions on the calcite surface, and they validated this finding with AFM experiment.

Few studies have looked at the impact of a mineral on the interface characteristics, and even fewer studied have utilized MD modeling to modify the EOS in which interface properties are computed. This research not only uses MD simulation to investigate the function of a particular mineral, such as calcite, on interface characteristics, but it also offers a method for calculating confinement parameters and incorporating them into Perturbation-Chain SAFT (PC-SAFT) [19] to measure interface properties.

In this study, we added calcite ( $\text{CaCO}_3$ ) wall effect into the PC-SAFT, which led to the definition of confinement parameters. We modeled the water-calcite interface with MD technique to estimate the confinement parameters. Calcite (1014) surface was chosen to represent a carbonate rock (oil reservoir rock) because calcite is the most abundant and

ubiquitous mineral in large carbonate reservoirs. Water, considered to be pure, is also one of the petroleum constituents with strong polar behavior. The estimated confinement parameters by MD were replaced in the modified PC-SAFT. Finally, PC-SAFT results were compared with the MD outcomes.

The remainder of this paper is organized as follows. In Section 2, we describe the theoretical method for PC-SAFT modification and details of MD simulation. In Section 3, the modified PC-SAFT model is validated with MD results. In Section 4, we summarize the list of findings and conclusions.

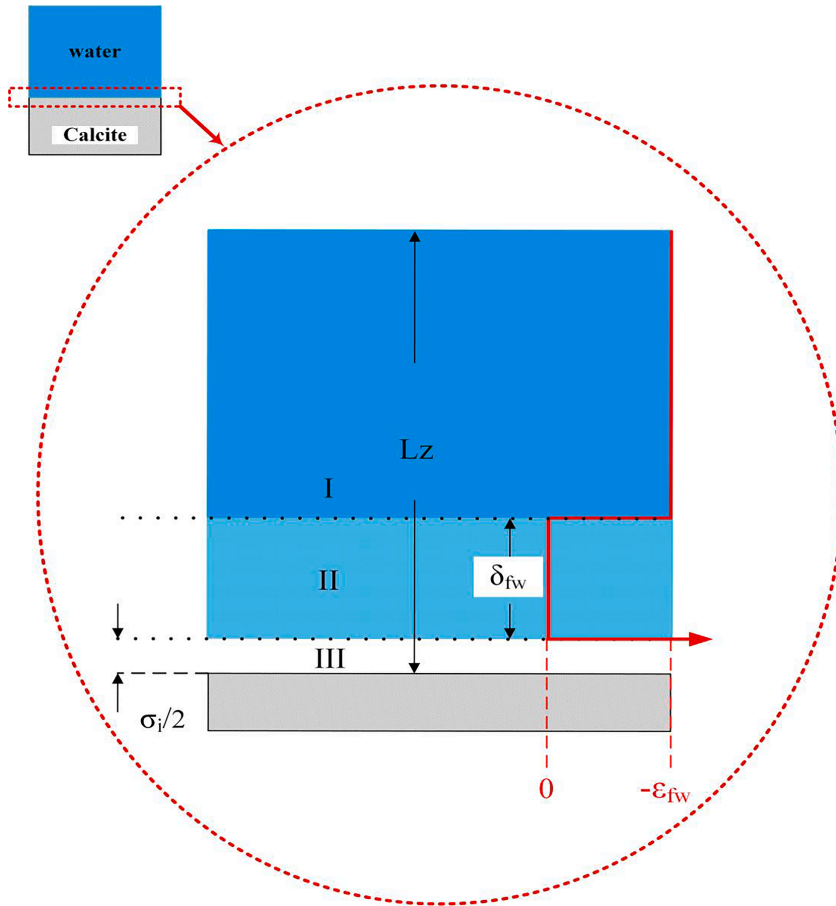
## Theoretical background

### Modification on PC-SAFT equation of state

Figure 1 displays the scheme of the interfacial confinement between water and calcite. Three different regions are visible in this sketch. Region I displays the bulk region where water-water interactions govern the intermolecular interactions. Here,  $L_z$  is the distance from the water bulk top layer to the calcite surface. The thickness of  $L_z$  were 25  $\text{\AA}$ , 40  $\text{\AA}$  and 70  $\text{\AA}$  in MD simulations. Region II with thickness of  $\delta$  is the surface-adsorbed zone where the water-calcite interactions are dominant interactions. Region III is free of any water molecule because its thickness ( $\sigma_i/2$ ) is less than half of the water molecules diameter ( $\sigma_i/2 \leq 0.5 \text{\AA}$ ) [20]. In other words, the thickness of this region is very narrow such that no water molecule could reside there. Within the confined geometry presented in Fig. 1, homogeneous and heterogeneous phase interactions mainly control the fluid phase behavior. The interactions in homogeneous and heterogeneous phases apply to the water-water and water-calcite, respectively.

Equation (1) shows a square-well potential, which estimates the interaction between the water molecules, where  $r_{ij}$  is the distance between two molecules,  $\epsilon_{ij}$  is the depth of the square well,  $\delta_{ij}$  is the relevant width of square well, and  $\sigma_{ij}$  is defined as the mean molecular diameter for water.





**Fig. 1.** Illustration of the confinement within water-calcite interface. Three different regions are visible here. Region I is the bulk region where molecular interactions are governed by water-water interactions.  $L_z$  is the distance from the water bulk top layer to the calcite surface, which is assumed to be 25 Å, 40 Å and 70 Å in MD simulations. Region II is the surface-adsorbed region where the molecular interactions are governed by water-calcite interactions and its thickness is shown by  $\delta$ . Region III is forbidden zone, which is supposed to include no water molecule. This region, marking with  $\sigma$ , is very narrow such that the center of mass of water molecules cannot reside here.

$$u_{ij}(r_{ij}) = \begin{cases} \infty & r_{ij} < \sigma_{ij} \\ -\epsilon_{ij} & \sigma_{ij} < r_{ij} < \sigma_{ij} + \delta_{ij} \\ 0 & r_{ij} > \sigma_{ij} + \delta_{ij} \end{cases} \quad (1)$$

Similarly, water and calcite molecules are supposed to interact through a square well, which is defined in equation (2):

$$u_i(l_i) = \begin{cases} \infty & l_i < \frac{\sigma_i}{2} \\ -\epsilon_{fw,i} & \frac{\sigma_i}{2} < l_i < \frac{\sigma_i}{2} + \delta_{fw} \\ 0 & l_i > \frac{\sigma_i}{2} + \delta_{fw} \end{cases} \quad (2)$$

According to equation (2),  $\epsilon_{fw,i}$  moves toward infinite within region III. Therefore, the landing of the water molecules in this narrow region is not probable. Hereafter,  $L_z/(0.5\sigma_i)$  is called length-ratio (L-R), showing the dimensionless water thickness in the water-calcite system.

In this context, we used Travalloni et. al.[21], approach to modify PC-SAFT EOS. To modify PC-SAFT equation of state, it is required to

start from the original definition of partition function, because partition function provides a theoretical platform to derive the thermodynamic properties. General definition of partition function is given in equation (3) [22]:

$$Q(N, V, T) = \left( \frac{M_{int}^N}{\lambda^{3N} N!} \right) V_f^N \exp \left( \int_{-\infty}^T \frac{E_{conf}}{kT^2} dT \right) \quad (3)$$

On the left side of equation (3) are the total number of particles (N), the system volume (V), and the temperature (T). On the right side,  $M_{int}$  is the internal partition function,  $\lambda$  is the de Broglie thermal wavelength,  $E_{conf}$  is configurational energy and  $k$  is the Boltzmann constant. The general definitions of Helmholtz free energy and chemical potential are written as:

$$A(N, V, T) = -kT Q(N, V, T) \quad (4)$$

$$\mu = \left( \frac{\partial A}{\partial N} \right)_{T,V} \quad (5)$$

The term of Helmholtz energy for water-water interaction in the homogeneous phase (region I) can be defined with equations (1), (3), and (4). To complete the thermodynamics of the system, it is required to add the wall effect contribution into the partition function. Equation (6) includes the effect of the calcite wall on water-calcite interface. As can be observed, the configurational energy contribution has been split into fluid–fluid and fluid–wall:

$$Q(N, V, T) = \left(\frac{M_{int}^N}{\lambda^{3N} N!}\right) v_f^N \exp\left(\int_{\infty}^T \frac{E_{conf-ff}}{kT^2} dT\right) \exp\left(\int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT\right) \quad (6)$$

In equation (6),  $E_{conf-ff}$  and  $E_{conf-fw}$  denote contributions of fluid–fluid and fluid–wall interactions, respectively. The first three terms in the right hand side of equation (6) correspond to the Helmholtz free energy in the bulk phase and the last term applies to the Helmholtz free energy within the interface confinement. In other words, equation (3) is modified to equation (6) by adding a fluid-wall contribution. Substitution of Helmholtz free energy in bulk phase gives:

$$Q(N, V, T) = \exp\left(-\frac{A^f}{kT}\right) \times \exp\left(\int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT\right) \quad (7)$$

$$= \exp\left(-\frac{A^f}{kT}\right) \times \exp\left(-\frac{A^{fw}}{kT}\right)$$

$A^f$  in equation (7) shows the Helmholtz free energy in the bulk phase. Additionally, the integral product of the second component in the right hand side of equation (7) has been replaced with  $A^{fw}$ , which stands for Helmholtz free energy for water-calcite interaction.

The natural logarithm of equation (7) gives:

$$\ln Q(N, V, T) = -\frac{1}{kT} (A^f + A^{fw}) \quad (8)$$

In equation (9), the terms of Helmholtz free energy corresponds to the calcite wall effect has been presented separately:

$$\left(\frac{A^{fw}(N, V, T)}{kT}\right) = \left(-\int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT\right) \quad (9)$$

Now, the partition function for water-calcite interface can be defined as a list of different terms, which contribute to total Helmholtz energy.

$$\ln Q(N, V, T) = -\frac{1}{kT} (A^{hs} + A^{disp} + A^{assoc} + A^{fw}) \quad (10)$$

According to PC-SAFT, the Helmholtz contribution for bulk ( $A^f$ ) can be broken down into hard-sphere ( $A^{hs}$ ), dispersion ( $A^{disp}$ ), and association ( $A^{assoc}$ ). It is worth to note that, in this simulation, water is assumed completely pure, namely no cation and anion exit in water bulk. Table 1 shows the pure component parameters of water used in PC-SAFT EOS [23].

Where  $m^{seg}$  is the segment diameter,  $E_{ij}/k$  is the dispersion energy parameter,  $\epsilon^{A_i B_j}$  is the association energy parameter,  $\kappa^{A_i B_j}$  is the association volume and  $\sigma'$  is the segment diameter determined using the formula in Table 1.

To make an intensive term, N is added to the denominator, which gives:

$$\ln Q(N, V, T) = \tilde{a}^{hs} + \tilde{a}^{disp} + \tilde{a}^{assoc} + \tilde{a}^{fw} \quad (11)$$

Equation (11) expresses the partition function in terms of well-defined Helmholtz energy contributions. To estimate  $A^{fw}$ , we have

applied equation (12) which uses  $F_p$  to relate the energy parameter of water-calcite to configurational energy [21]:

$$E_{conf-fw} = -NF_p \epsilon_{fw} \quad (12)$$

In equation (12),  $\epsilon_{fw}$  is the energy parameter associated with water-calcite interaction.  $F_p$  also is defined as:

$$F_p = F_{pr} + (1 - F_{pr}) \left(1 - \exp\left(\frac{-\epsilon_{fw}}{kT}\right)\right) \left(1 - \frac{\rho}{\rho_{max}}\right)^\theta \quad (13)$$

According to Travalloni et al. [21],  $\theta$  and  $F_{pr}$  are confinement degree and fraction of the water molecules in the square well. The equations (14) and (15) present  $\theta$  and  $F_{pr}$  definitions, based on the depicted assumptions in Fig. 1:

$$F_{pr} = \frac{\left(L_z - \frac{\sigma}{2}\right) - \left(L_z - \frac{\sigma}{2} - \delta\right)}{\left(L_z - \frac{\sigma}{2}\right)} \quad (14)$$

$$\theta = \frac{L_z}{\delta + \frac{\sigma}{2}} \quad (15)$$

where,  $L_z$  is length of water bulk mounted over calcite wall,  $\delta$  is width of the square well, and  $\sigma$  is average diameter of the water molecules.

In order to compute the Helmholtz free energy incorporating calcite-wall effect,  $\epsilon_{fw}$ ,  $\rho_{max}$ ,  $\theta$  and  $F_{pr}$  must be calculated in advance using MD simulation. In the next step,  $F_p$  is computed using confinement parameters mentioned before. Calculated  $F_p$  is put into equation (12) and the results are plugged into equation (9). The integral product of  $E_{conf-fw}$  is then used to calculate  $A^{fw}$  in equation (9). Equation (10), which sums up the Helmholtz species, yields the Helmholtz free energy corresponds to the interface confinement.

#### MD simulation

The MD simulation applies the Born-Oppenheimer approximation to model the dynamics of the multi-particle systems built upon a certain thermodynamic ensemble [24]. In this approximation, Newton's law of motion governs the dynamic of the nuclei corresponding to the atoms or molecules. Therefore, the non-relativistic Hamiltonian becomes an implicit function of nuclei positions and momentums [25]:

$$H(p, r) = K_E + U = \sum_{i=1}^N \frac{p_i^2}{2m_i} + U(r_1 + r_2 + \dots + r_i + \dots + r_N) \quad (16)$$

Where,  $p_i$  and  $r_i$  are set of particle momenta and positions,  $K_E$  is kinetic energy,  $U(r)$  is potential energy,  $m_i$  is particle mass, and N is the total number of particles.

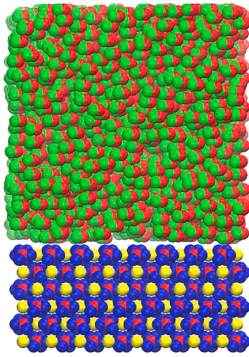
We used the open source LAMMPS software as the classical molecular dynamic code for molecular dynamic simulation [26]. The Newtonian equation of motions developed by the velocity Verlet algorithm adopts the time step of 1 fs for all simulations. Each MD simulation was executed with a constant temperature. The temperature itself was updated through a loop in the LAMMPS code.

The developed force field by Zhao et al. [27] defined the internal forces between 480 calcite molecules. These molecules are sorted into 6 layers along (1014) a perfect calcite surface. The SPC/E [28,29] model described the internal interactions among the molecules of water bulk. Fig. 2 shows the calcite-water layout in the simulation box. As it is seen, we have built a molecular system including a water bulk mounted above the calcite slab along the z-direction. In the simulation box, water bulk was prepared with three different lengths along the z-axis: 25 Å, 40 Å, and 70 Å. For both the x and y directions, the boundary conditions were periodic. The boundary condition for the z-direction was set to be constant, and a reflecting wall was inserted above the water bulk to avoid atom loss.

To wrap the molecules of the calcite slab and water bulk, we applied

**Table 1**  
PC-SAFT parameters for pure water.

$m^{seg}$	$\sigma'$ [Å]	$E_{ij}/k$ [K]	$\epsilon^{A_i B_j}$ [K]	$\kappa^{A_i B_j}$
1.2047	*	353.95	2425.7	0.0451
* $\sigma = 2.7927 + 10.11 \exp(-0.01775 \times T) - 1.417 \exp(0.01146 \times T)$ , T is the temperature in [K]				



**Fig. 2.** Illustration of water-calcite system for MD simulation. The calcite slab includes 6 layers sorted along the (1014) plane and overlaps with water bulk on xy plane. The water bulk has extended along the z-axis with 25 Å, 40 Å and 70 Å thickness.

PACKMOL [30] that compacts the molecules with a certain distance such that the structure of molecules remains intact. Running the minimize function with conjugate gradient algorithm lets the molecules remain at a reasonable distance and the energy flood during the simulation run is avoided. The equilibration process in each simulation is fulfilled by initializing the particles velocity with a set temperature. Then, the equilibration followed by Nose-Hoover NVT thermostat until 3 ns in which temperature remains constant at  $T = 300$  K, 400 K and 500 K. Finally, LAMMPS measured the thermodynamic properties by averaging over total run time.

## Results and discussion

### Density profile at constant length ratio

Figure 3 illustrates the profile of water density inside the layering zone and bulk phase. The length-ratio (L-R) and temperature, respectively in each row and column, are constant. From left to right the simulation temperature increases from 300 K to 400 K and 500 K while from top to bottom the L-R decreases from 140 to 80 and 50. The density plot has oscillatory behavior near the calcite-wall so-called layering zone. In fact, the layering zone and bulk imply regions II and I according to the zone classification in Fig. 1.

In the first row with  $L-R = 140$ , when  $T = 300$  K, the density experience the longest peak in region II and flatten at bulk density inside region I. However, the shortest peak in region II and minimum density inside region I belongs to  $T = 500$  K. Simultaneously, the density values at  $T = 400$  K remain between  $T = 300$  K and  $T = 500$  K. Compared with the first row, the same regime is observed in the second and third row for  $L-R = 80$  and  $L-R = 50$ , respectively. It means, with constant L-R, the highest density inside region I and II belongs to  $T = 300$  K. Whilst the lowest density in region I and II corresponds to  $T = 500$  K. Therefore, for a constant L-R, the density inside the region I and region II varies with respect to the mean distance between the water molecules. In other words, with constant length-ratio,  $T = 300$  K, 400 K and 500 K provide the minimum, medium and maximum mean distance among the water molecules, which respectively leads to maximum, medium and minimum density in region I and II.

### Density profile at a constant temperature

The first, second and third column in Fig. 3 display density profile at constant temperature and different L-R values. A deceptive point that

one may notice at first glance is the ascending behavior of the density profile from top to bottom. Namely, the longest and shortest peak in region II occur at  $L-R = 50$  and  $L-R = 140$ . Within region I from top to bottom, on the other hand, the density trend of  $L-R = 140$ , lays on higher values than  $L-R = 80$  and  $L-R = 50$ . In Fig. 3, this regime is repeated in all columns.

For ease of comparison at constant temperature and variable L-R, the depicted density profiles in Fig. 3, have been normalized between 0 and 1. Fig. 4a–c display the variation of normalized density with respect to the L-R at constant temperature. In Fig. 4a–c, one can visually compare the size of the marked area showing average density. For example, at  $T = 300$  K the smallest area belongs to  $L-R = 50$  compared with  $L-R = 80$  and  $L-R = 140$ . It means,  $L-R = 140$  and  $L-R = 50$  make the max and min average density at  $T = 300$  K while the relevant density for  $L-R = 80$  remains larger than  $L-R = 50$  and smaller than  $L-R = 140$ . This regime is replicated in Fig. 4b and c. Therefore, with fixed temperature, the min and max length-ratio provide minimum and maximum average density within region II and I, respectively.

This fact is consistent with the definition of interface confinement within the water bulk and calcite-wall. To be specific, reduction in confinement size reduces the density, and raising the confinement size provides density growth. In our simulation,  $L-R = 140$  is the maximum confinement and gives larger water density than  $L-R = 80$  and  $L-R = 50$ . The maximum density is potentially achieved in a water-calcite system with an infinite length-ratio ( $L-R = \infty$ ) or a water bulk without the presence calcite-wall. Even though  $L-R = 140$  and  $L-R = 50$  give the greatest and lowest average density within regions II and I, how the local peaks inside region II are interpreted remains a mystery.

In fact, the adsorbed water molecules on the calcite-wall are apparent in the local peaks of region II. On the one hand, the number of water molecules adsorbed to the calcite surface is controlled by the calcite's attraction. On the other hand, the average attraction force inside region II, is the consequence of a trade-off between the calcite-wall attraction and the water bulk attraction. It means that thin layers of water are more attracted to the calcite-wall than thicker ones. Additionally, it may be said that  $\alpha_{50} > \alpha_{80} > \alpha_{140}$  where  $\alpha$  represents the number of water molecules within the first adsorbed layer, and the subscripts express the L-R values. Consequently, the extension of the water bulk along the z-axis increases the waterside's average attraction force and decreases water adsorption on the calcite-wall, and reducing the water length, on the other hand, results in a notable local peak of density inside region II. To sum up, the highest local density is achieved at the first adsorbed layer when the lowest confinement is used. However, as seen in Fig. 4a–c, the average density under minimum confinement remains minimal.

### Energy behavior with respect to L-R and temperature variation

Figure 5 demonstrates the total energy profile inside region II and I for different length-ratios and temperatures. The vertical columns display the energy behavior at fixed temperature and  $L-R = 140$ , 80 and 50. The horizontal rows express the energy variation at constant L-R and  $T = 300$  K, 400 K and 500 K. Moving from left to right where  $L-R = 140$ , one observe the decay in the absolute energy values such that  $E_{300K} > E_{400K} > E_{500K}$ . The same pattern is noticed in the second and third row, which means at constant length-ratio, higher temperature causes lower energy inside the layering zone and bulk.

From left to right, comparison of the energy profiles with the density trends in Fig. 3, reveals that max and min density within region II and I corresponds to the maximum and minimum energy respectively. For example, in the first row of Fig. 3 one notices  $\rho_{300K} > \rho_{400K} > \rho_{500K}$ . It means with  $T = 300$  K the water molecules stand at shorter distance than  $T = 400$  K and  $T = 500$  K. Therefore, with constant L-R, the higher the temperature the lower the total energy.

Moving from top to bottom, one observes the length of local peaks within region II increases, whereas the widths of the curves narrow

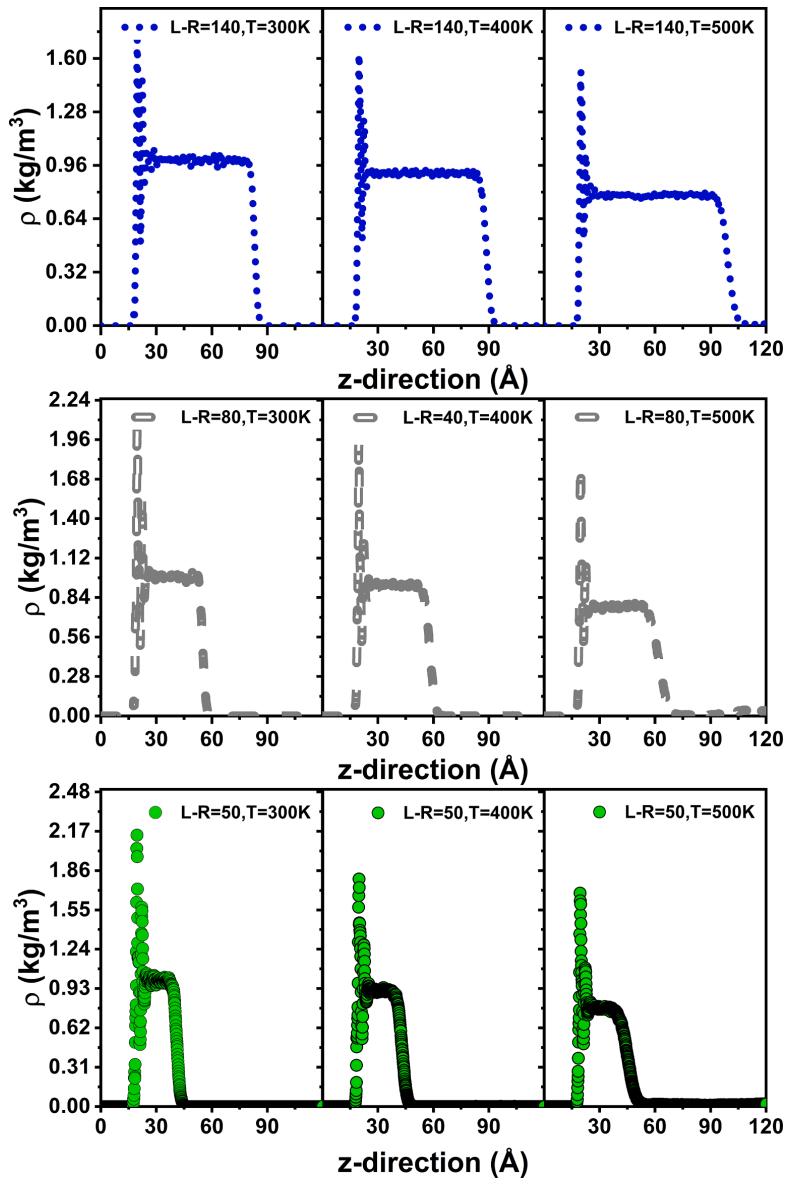
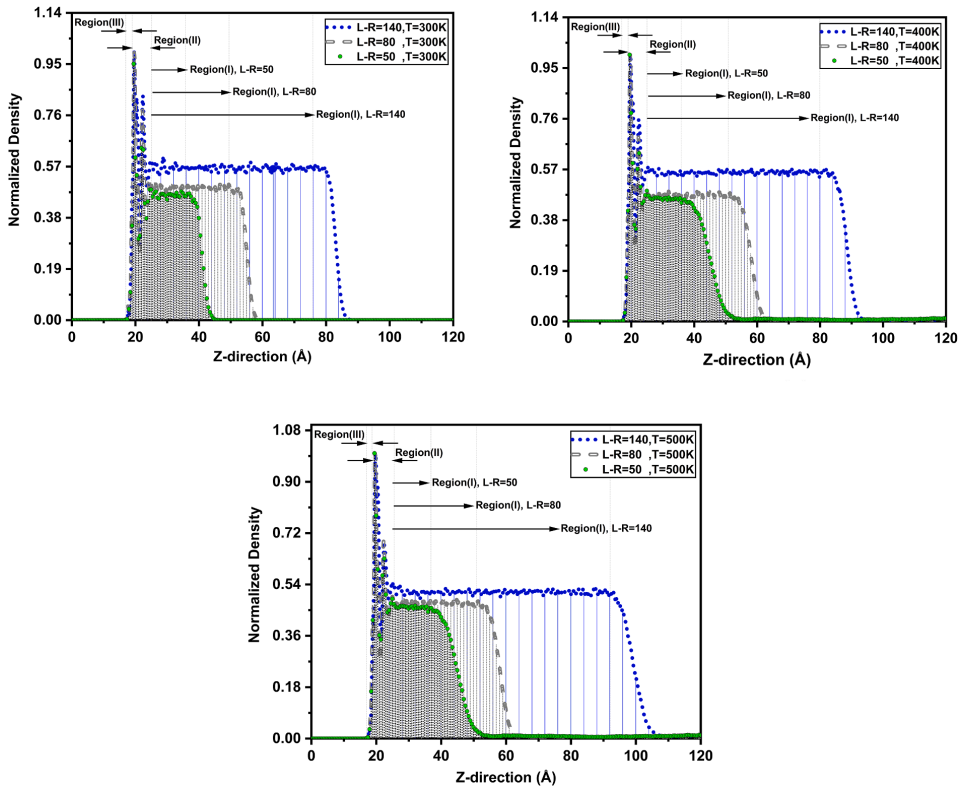


Fig. 3. Illustration of the density profile inside region I and II at several length-ratios and different temperatures. The plotted curves in each row represent the density profile at constant L-R, while each column presents the density profile at fixed temperature. From left to right the simulation temperature increases from 300 K to 400 K and 500 K. The L-R, from top to bottom, decreases from 140 to 80 and 40.

down. This energy pattern provides smaller average energy for smaller confinement and vice versa. For example, in the last column of Fig. 5 where  $T = 500$  K, the absolute value of the integral over  $L-R = 50$  trend corresponds to the minimum average energy. Whereas the absolute value of integral over  $L-R = 140$  illustrates the maximum average energy. Therefore, with  $T = 500$  K, the reduction in length-ratio reduces the absolute average total energy, i.e.,  $E_{140} > E_{80} > E_{50}$ . This pattern is

observed in the first and second columns.

To sum up, the stronger effect of the calcite attraction forces on thin bulk of water leads to the higher adsorption at the first adsorbed layer of water molecules over calcite-wall. High adsorption at the first adsorbed layer results short intermolecular distance. When the intermolecular distance at the first adsorbed layer diminishes, the length of the local peaks for density and energy increases. Whilst, thick bulk of water have



**Fig. 4.** Illustration of the density profile within region I and II at different L-R and constant temperature. The density is normalized between 0 and 1, which allows comparing the average density trend. The integral of the density inside region I and II is shown by the darkened regions beneath the trends (blue > gray > green). The greatest and lowest average densities at constant temperature, according to the shaded area under the curve, are L-R = 140 and L-R = 50, respectively. In addition, the marked up regions depict the schematic thickness of regions I, II, and III. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

stronger intermolecular attractions and cancels out the effect of the calcite attraction. Hence, the density within the first adsorbed layer over the calcite-wall decreases. The reduction in density within the first adsorbed layer shortens the length of the local peaks for density and energy. Therefore, the shorter the water bulk the larger the local peak in density, but the smaller the average density. In addition, high and low values of average density correspond to the high and low values of average total energy, respectively. Therefore, with fixed L-R and variable temperature, the molecule–molecule distance controls the density and energy. Nevertheless, with variable L-R and fixed temperature, the balance between molecular attraction forces of calcite-wall and water bulk controls the density and energy.

*Comparison of PC-SAFT and MD simulation*

In section 2.1, the confinement parameters were introduced by equations (13), (14) and (15). We applied MD simulations to estimate the introduced confinement parameters. Table 2 presents calculated confinement parameters under different confinement sizes and temperatures. In this table, the potential of the water-calcite interaction ( $\epsilon_{fw}$ ) was calculated by the integral of the energy over the layering zone [31]. The fraction of confined molecules ( $F_{pr}$ ) and confinement degree ( $\theta$ ) were determined according to the defined formula in equations (14)

and (15).

To estimate the bulk density ( $\rho_{max}$ ), we simulated water in MD without the presence of the calcite-wall. Because, at a known temperature, the density of water without the presence of the calcite-wall is maximum. Hence, water was simulated with MD at T = 300 K, 350 K, 400 K, 450 K, and 500 K which the results were tabulated in Table 3.

Table 3 displays simulation (MD and PC-SAFT) and laboratory results for water density without the presence of calcite-wall. To be specific, Table 3 reports the reliability of MD and PC-SAFT for predicting the water density without the presence of calcite-wall. The columns |RE-1| and |RE-2| show the absolute relative errors for MD and PC-SAFT, respectively. As shown, for a specific range of temperature, the obtained results from MD and PC-SAFT are reliable, although the absolute relative error increases with temperature rise.

Table 4 listed the predictions of MD and modified PC-SAFT for the interface layer within region II. One can compare Table 4 with Table 3 at relevant temperatures. As seen, because of the calcite-wall presence, the reported densities in Table 4 are smaller than the relevant ones in Table 3.

The plot in Fig. 6 compares the modified PC-SAFT with MD results at different temperatures. The diamond, circle and square exhibit the MD results at L-R = 50, 80 and 140, respectively. In addition, blue, red and green curves are representative of modified PC-SAFT predictions L-R =

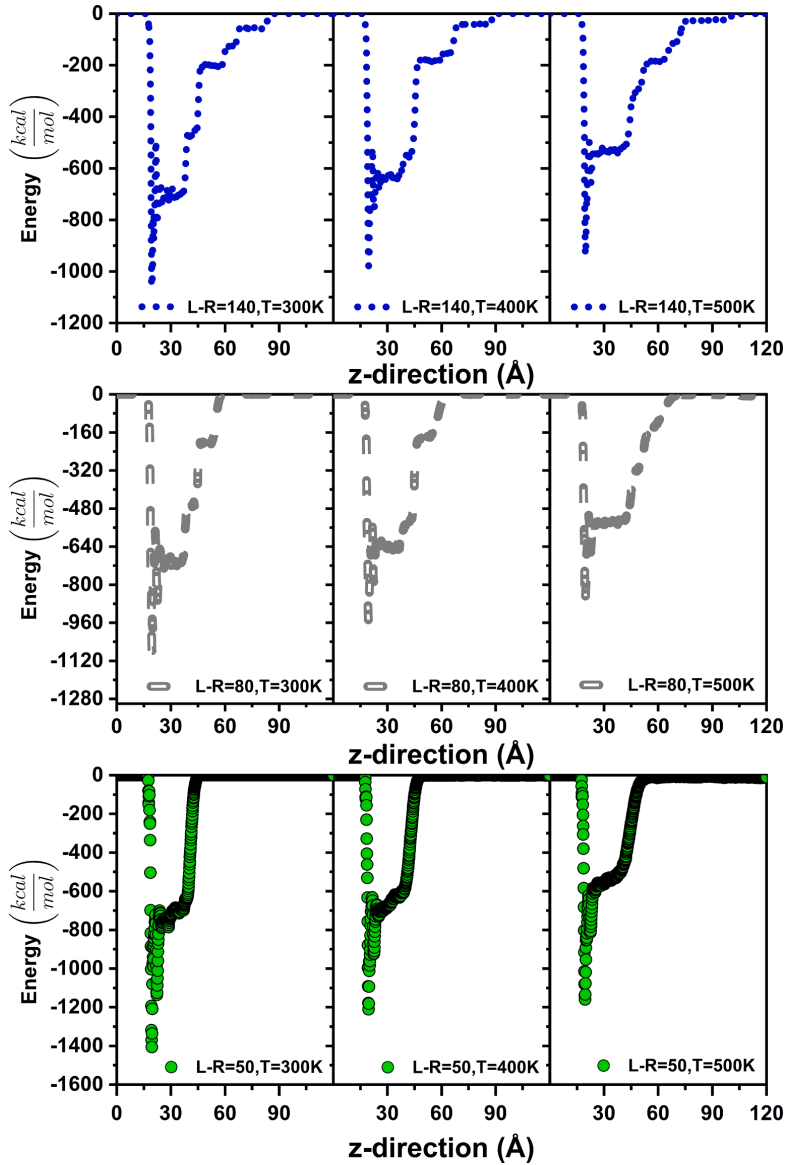


Fig. 5. Illustration of the energy profile inside region I and II at several length-ratios and different temperatures. The plotted figures in each row and column represent the energy trend at constant length-ratio (L-R) and temperature respectively. From left to right the simulation temperature increases from 300 K to 400 K and 500 K while from top to bottom the L-R decreases from 140 to 80 and 50.

50, 80, and 140. At the bottom of the plot box, the profile of absolute relative error shows the deviation of modified PC-SAFT from MD results. To be specific, dashed, dotted and doubled lines are the trajectory of relative error at L-R = 50, 80 and 140, respectively. The vertical axis at the left is the density ratio, including the bulk density in the denominator, which implies  $\rho_{max}$ .

As seen in Fig. 6, when L-R increases at a fixed temperature, both MD and PC-SAFT predict larger fractions of  $\rho/\rho_{max}$  [33]. This means with a

fixed temperature, by growth in confinement size, the confined density ( $\rho$ ) increases which leads to a reduction of the gap between  $\rho$  and  $\rho_{max}$ . This fact also satisfies the mathematical limit in equation (13), which says, by extending the water length above the calcite-wall ( $L_z \rightarrow \infty$ ), the density within the layering zone approaches the bulk density ( $\rho = \rho_{max}$ ). Substitution of  $\rho = \rho_{max}$  in equation (13) gives homogeneous distribution within the region II ( $F_p = F_{pr}$ ).

In addition, when the temperature rises for a fixed L-R, the MD

**Table 2**

Estimated confinement parameters with MD simulations. The  $\epsilon_{fw}$ ,  $\rho_{max}$ ,  $F_{pr}$  and  $\theta$  respectively present potential of fluid-wall interaction, bulk density, fraction of confined molecules and confinement degree.

T = 300 [K]						
L-R	$\epsilon_{fw}$ [kcal]	$\rho_{max}$ [kg/m <sup>3</sup> ]	$\delta$ [Å]	$F_{pr}$	$\theta$	
50	-3248.525	957.650	5.6	0.229	3	
80	-2686.685	973.203	5.9	0.149	6	
140	-2695.768	982.393	6.1	0.087	10	
T = 400 [K]						
50	-3023.907	888.010	5.6	0.229	3	
80	-2511.321	898.869	5.9	0.149	6	
140	-2497.062	905.682	6.1	0.087	10	
T = 500 [K]						
50	-2722.839	770.170	5.6	0.229	3	
80	-2246.411	774.076	5.9	0.149	6	
140	-2271.883	780.998	6.1	0.087	10	

**Table 3**

List of the water density at different temperatures without the presence of calcite-wall. This table compares the laboratory data with the outcomes of MD and PC-SAFT. The columns |RE-1| and |RE-2| display the absolute relative error for MD and PC-SAFT, respectively.

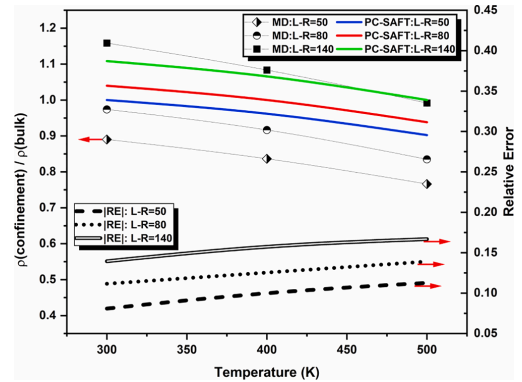
Liquid water density						
T [K]	Laboratory [32] [kg/m <sup>3</sup> ]	MD [kg/m <sup>3</sup> ]	PC-SAFT [kg/m <sup>3</sup> ]	RE-1  %	RE-2  %	
300	996.499	1000.003	990.490	0.352	0.603	
350	973.693	970.383	973.365	0.339	0.033	
400	937.465	923.463	952.634	1.494	1.618	
450	890.319	861.221	926.686	3.268	4.085	
500	831.302	791.007	893.784	4.847	7.516	

**Table 4**

Comparison between MD outcomes as a pseudo experiment and modified PC-SAFT for region II. As it is seen, when the temperature is fixed, PC-SAFT prediction grows with growth in L-R. While with constant L-R, PC-SAFT prediction decreases with temperature growth.

Region (II): Liquid water density						
T K	MD [kg/m <sup>3</sup> ]			Modified PC-SAFT [kg/m <sup>3</sup> ]		
	L-R = 50	L-R = 80	L-R = 140	L-R = 50	L-R = 80	L-R = 140
300	890.251	899.404	916.439	990.569	990.586	990.621
400	836.394	846.519	857.083	952.708	952.725	952.750
500	766.145	771.005	784.565	893.907	893.908	893.930

predicts a smaller ratio of  $\rho/\rho_{max}$ , and relevant |RE| has increased. In other words, under a fixed confinement size, going up in temperature increases the gap between confined density and  $\rho_{max}$ . The behavior of the absolute relative error in Table 3 is consistent with the profile of |RE| in Fig. 6. Regarding the |RE| profile at the bottom, two factors result in smaller errors, i.e., the larger confinement and lower temperature. The former moves the properties of the confined water toward the properties of the water bulk, as discussed already. The latter refers to the accuracy of chosen model for water in MD simulation because the accuracy of SPC/E model deteriorates at high temperatures [34]. According to the hypothesis of SPC/E model, the water molecule is fixed-charge, rigid, and non-polarized with an on-plane location. However, in reality, the “charge-distances-angle” parameters for the water molecules fluctuate routinely, affecting the molecule’s electrostatic, and therefore the consequence bulk properties. Because of high temperature, the limitations of SPC/E model to predict the water properties increases because i) at increasing temperatures, the spatial fluctuation of



**Fig. 6.** Graph compares the predictions of MD and modified PC-SAFT at T = 300 K, 400 K and 500 K. The diamond, circle and square exhibit the MD results at L-R = 50, 80 and 140. The blue, red and green curves are representative of modified PC-SAFT predictions at L-R = 50, 80 and 140. In the bottom of plot box, the profile of absolute relative error shows the deviation of modified PC-SAFT from MD results. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

“charge-distances-angle” rises. Therefore, the legitimacy of “simple 3-point charge” models diminishes ii) as temperature rises, the non-polarized assumption loses its validity due to increasing collision between the molecules. As a result, SPCE’s ability to forecast water characteristics at high temperatures has deteriorated [35].

**Summary and conclusions**

To develop our understanding for confinement within fluid-rock interface we simulated water-calcite system with three different thickness of water bulk: L-R = 140, 80 and 50. In our numerical experiments, we observed that going down in water thickness at a fixed temperature, provides smaller density and energy within the water-calcite interface. Furthermore, with a constant L-R, low temperature give rise in density and energy within the layering zone. Then, we concluded that at constant L-R mean distance between water molecules controls the density and energy trend. Whereas at constant temperature the attraction forces of calcite control the density and energy profile. To develop a thermodynamic model for predicting the density change due to calcite-wall presence, we defined a new contribution for Helmholtz free energy in PC-SAFT. Then, the introduced confinement parameters: potential of fluid-wall interaction ( $\epsilon_{fw}$ ), bulk density ( $\rho_{max}$ ), fraction of confined molecules ( $F_{pr}$ ) and confinement degree ( $\theta$ ) were adjusted against MD calculations. The prediction of modified PC-SAFT were validated with MD and good agreement was observed. The uncertainty of the modified PC-SAFT increases with reduction in confinement or temperature.

In conclusion, MD simulation demonstrates that at the water-calcite interface, a smaller L-R provides a lower density at given temperature while low temperatures increase density and energy with a given L-R. Furthermore, the density, energy, and geometry of confinement at the layering zone influence the derived contribution for Helmholtz free energy. Finally, as a result of the addition of introduced Helmholtz energy to PC-SAFT, one may anticipate the interface properties in good agreement with MD results.

**CRedit authorship contribution statement**

**S. Ahmadi G.:** Conceptualization, Methodology, Software, Validation, Writing – original draft, Visualization, Formal analysis, Investigation, Writing - review & editing. **S. Abdolahi:** Software, Validation,

Investigation. **R. Miri**: Supervision, Writing - review & editing. **H. Hellevang**: Supervision, Writing - review & editing.

### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Paper II

# **Extension of SAFT Equation of State for Fluids Confined in Nano-pores of Sedimentary Rocks Using Molecular Dynamics Simulation**

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# Extension of SAFT equation of state for fluids confined in nano-pores of sedimentary rocks using molecular dynamic simulation

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## ABSTRACT

Confined fluids in nano-mineral pores show notably different thermodynamic behavior compared with those of the same fluid in bulk. We have extended an equation of state (EoS) inspired by statistical association fluid theory (SAFT) to incorporate the fluid-mineral effect into the pure fluid properties confined in the nanopore. The established EoS is coupled with a Helmholtz free energy contribution which is a function of confinement characteristics: the potential of fluid-mineral interaction, bulk-like density and CF. The novel fitting parameter CF relies on the local properties of confined fluid and measures the density fraction within the layering and bulk-like zones, i.e.,  $CF = \rho_{\text{layering zone}} / \rho_{\text{bulk-like zone}}$ . The first-principle molecular dynamics (MD) simulation was utilized to estimate the confinement parameters. At  $T = 300$  K, 350 K, 400 K, and 450 K, the NVT ensemble was applied to simulate slit-pore calcite with a continuous and homogeneous surface in contact with water, with pore widths ranging from 1.5 nm to 5 nm. After running each NVT ensemble for 6 ns, the energy and density of confined water were analyzed, and a deviation was discovered with different behavior from what had previously been reported. Coupling CF parameter with proposed EoS improves the absolute relative errors (ARE) at low temperatures up about 50%, leading to a good agreement between modified SAFT EoS and MD results. The methodology described here may be extended to include a mixture of associating fluids such as those found in oil composition and implemented in all SAFT versions.

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## 1. Introduction

The prediction of phase diagrams and thermodynamic properties of fluids entrapped in confined spaces (i.e., diameters between 1 nm and 10 nm) is of wide practical interest as it appears in many applications, including heterogeneous catalysis [1], enhanced oil recovery (EOR) from shale reservoirs [2], carbon capture and storage (CCS) [3], hydrogen storage [4], geochemistry [5] and geophysics [6]. Confined fluids have distinct dynamical and structural characteristics so that their physical properties and phase behavior noticeably deviates from corresponding bulk phase. In fact, as the size of the confinement decreases and approaches the molecular dimensions of the trapped fluid (i.e., sizes comparable to the mean free path), the free thermal motion of fluid molecules is disrupted, which in turn creates different and unique thermodynamic properties. Experimental and numerical studies have shown that, depending on the intermolecular forces, confined fluids can exhibit specific interface-induced struc-

tures (i.e., molecular-scale arrangement, layering and orientation) which consequently results in interfacial regions of reduced density, saturation pressure and critical pressure. Anyhow, laboratory measurements of the confined fluids phase behavior are time-consuming and expensive and limited to a narrow temperature and pressure window.

Generally speaking, the size, shape and type of the intermolecular forces define the state and thermophysical properties of fluids. Standard engineering EoSs of the Van der Waals type (cubic type EoSs) are common choices for phase equilibria calculations of simple fluids in the bulk phase. The most important intermolecular forces incorporated in such EoSs are van der Waals attractions along with weak electrostatic forces due to dipoles, quadrupoles, etc. For more complex fluid-wall interactions with strong molecular forces, the simple repulsive reference term in engineering EoSs is not sufficient, and the predictability of fluid properties and phase equilibria (especially the subcooled liquid phase) is poor. To this end, Zarragoicoechea and Kuz [7,8] modified van der Waals EoS [9] to show the shift in critical pressure and temperature. The resulting EoS, however, failed to predict the critical density of the confined fluid accurately. Derouane [10] modified the van der

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salinity implying improvement in calcite surface hydrophilicity. S. Ahmadi G. et al. [29], used MD simulation to study the water-calcite interface. They developed an EoS inspired by Perturbation-Chain SAFT (PC-SAFT) to predict the water properties near the calcite-wall, and the results were promising. There are even fewer who have developed a well-defined match parameter that is consistent with the confined fluid characteristics [30]. In the current study, first, we used statistical thermodynamics to build a model that represented the Helmholtz free energy of confined fluid as a function of nanopore characteristics. The necessary parameters for the developed Helmholtz are then calculated using MD simulation. In MD simulation, the surface (10 $\bar{1}$ 4) of calcite was chosen as the mineral surface to interact with pure water as the associated fluid. Finally, we presented a physical coefficient that very closely matches predictions of the modified SAFT with MD results. The rest of this paper will be structured as follows: The theoretical background is given in Section 2. Sections 2.1 and 2.1.1 discuss the EoS and SAFT key characteristics. Section 2.2 contains details on the MD simulation. Finally, in Sections 3 and 4, the study's findings are reviewed and summarized.

## 2. Theoretical background

In this section, the Helmholtz energy term related to fluid–solid interaction inside a slit shape calcite nanopore is derived based on statistical mechanics. Then, the theoretical aspects of MD simulation are discussed in detail.

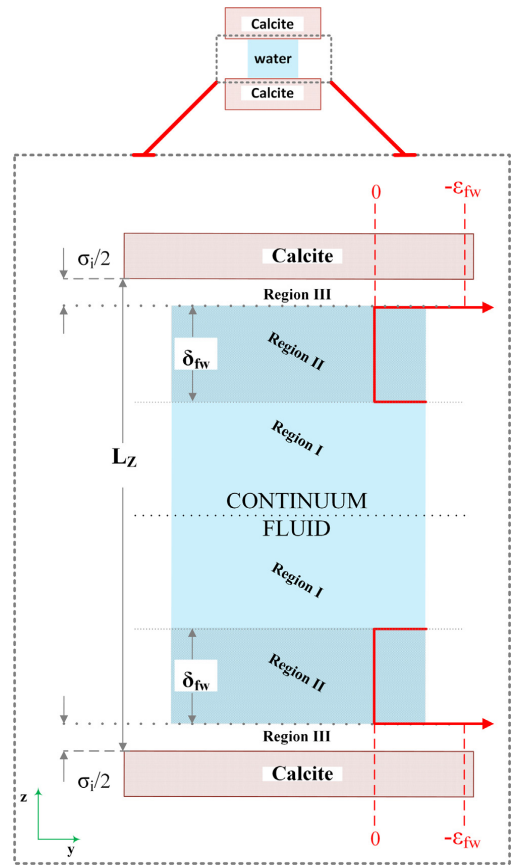
### 2.1. Equation of state (EoS)

Equation of state has a crucial role in describing phase behavior and chemical equilibria in geochemical processes. Recent developments in statistical mechanics have introduced a molecular-based EoS, which models associating fluids and complex interactions accurately. The molecular-based EoS inspired by statistical association fluid theory (SAFT) [31,32] formulates all types of molecular interactions with a sum of corresponding Helmholtz energy. Unlike PVT EoS, which utilizes complex mixing rules and unphysical binary coefficients, one can model a fluid–solid interaction with a definition of Helmholtz energy for fluid–solid interaction. The following section describes the details of the Helmholtz free energy derivation.

#### 2.1.1. Basic formulation of the Helmholtz free energy for confined fluids

This section presents an overview of a model formulation based on the generalized van der Waals partition function [33]. The supplemental information includes an in-depth explanation that may be referred to. Fig. 1 illustrates the conceptual framework used to model water confined in a calcite nanopore. As shown, the confinement is divided into three regions depending on the type of molecular interaction.

Region I (bulk-like) is the closest Region to the pore center and furthest from pore-walls, such that the interactions between pore-wall and water molecules are minimal and can be neglected. In other words, within Region I, water–water interactions provide the main contribution to the configurational energy of the system. Region II (layering zone), which surrounds Region I and lies between a bulk-like and a forbidden region, is dominated by water–calcite interactions. The thickness of Region II is shown with  $\delta_{fw}$ . The nearest Region to the pore-wall is Region III, the intermediate zone between Region II and calcite slabs. The forbidden zone with a thickness of  $\sigma_i/2$  displays an empty margin adjacent to the pore-walls with no water molecule inside. The mean diameter of water molecules is represented by  $\sigma_i$ . Thus, the thickness of Region



**Fig. 1.** Simulation geometry illustration including water molecules sandwiched within the slit shape calcite nanopore. In this sketch,  $L_z$  denotes the width of the nanopore. The pore volume has been divided into three different regions based on the interactions between different molecules. Region I is the nearest Region to the pore center and furthest from the calcite-wall. Region II is a layering zone where the dominant molecular interaction is water–calcite interaction. The thickness of Region II is shown with  $\delta_{fw}$  at the top and bottom. Region III, with a thickness of  $\sigma_i/2$  presents a vacant margin adjacent to the nanopore walls with no water molecule inside.

III is sufficiently thin that no water molecule center of mass dwells there ( $\sigma_i/2 \leq 0.85$  [Å]).  $L_z$  is the distance between the pore-walls representing the confinement width and thickness of water settled within calcite slabs. In fact, summing the length of bulk-like, double layering and double forbidden zones gives the total length of the  $L_z$ . The fluid–fluid molecular interactions are assumed to interact through a square well potential:

$$u_{ij}(r_{ij}) = \begin{cases} \infty & r_{ij} < \sigma_{ij} \\ -\epsilon_{ij} & \sigma_{ij} < r_{ij} < \sigma_{ij} + \delta_{ij} \\ 0 & r_{ij} > \sigma_{ij} + \delta_{ij} \end{cases} \quad (1)$$

where,  $r_{ij}$  is molecule–molecule distance,  $\epsilon_{ij}$  is the square well depth,  $\delta_{ij}$  is the square well width, and  $\sigma_{ij}$  is the mean molecular diameter. The parameters of pure water utilized in SAFT2 are listed in Table 1 [34].

**Table 1**  
SAFT2 parameters for pure water.

$v^{00}$ [ml/mol]	$u^0/k$ [K]	$\Lambda$	$\phi/k$ [K]	$\kappa$
9.8307	311.959	1.5369	1481.41	0.04682

As can be seen,  $v^{00}$  segment volume,  $u^0/k$  segment energy,  $\Lambda$  segment diameter,  $\phi/k$  association energy and  $\kappa$  association volume are SAFT2 parameters for pure water. Similarly, the fluid and solid molecules interact through a square well potential of the following form:

$$u_{fw}(L) = \begin{cases} 0 & L < L_z - 2\sigma_i - 2\delta_{fw} \\ -\varepsilon_{fw} & L_z - 2\sigma_i - 2\delta_{fw} < L < L_z - 2\sigma_i \\ \infty & L > L_z - 2\sigma_i \end{cases} \quad (2)$$

As seen,  $L$  is the longitudinal position of a fluid molecule inside the pore.

The first condition in this potential function relates to Region I, which has a zero square well potential. The second depicts Region II, where water and calcite molecules interact with  $-\varepsilon_{fw}$  square well potential. Region III is subjected to the last condition, in which the energy level is so high that no water molecule may settle there.

We begin by defining the partition function to develop a meaningful term for Helmholtz free energy that incorporates the pore wall effect.

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} \right) V_f \exp \left( \int_{\infty}^T \frac{E_{conf}}{kT^2} dT \right) \quad (3)$$

For a system including  $N$  particles with mass  $m$ , the canonical partition function,  $Q$ , is defined as presented in Eq. (3) [33,35]. Where  $q_{int}$  is the internal partition function,  $\lambda$  is de Broglie thermal wavelength,  $k$  is Boltzmann constant and  $T$  is the absolute temperature. In Eq. (3),  $E_{conf}$  and  $V_f$  denote the configurational energy and free volume, respectively. (supplementary information, section A and B). As observed in Eq. (3), the lower limit of the integral depicts high temperature ( $T \rightarrow \infty$ ) when fluid behavior approaches ideal gas behavior, while the upper limit of the integral represents the actual fluid situation. Once the partition function is established, we may express the Helmholtz free energy as:

$$A_{N,V,T} = -kTQ_{N,V,T} \quad (4)$$

Eqs. (3) and (4) are sufficient to model Region I dominated by water-water interactions. However, the thermodynamic description of the system is incomplete since it does not include the interaction between the water molecules and the calcite-wall. As previously stated, no water molecule resides within Region III, where no water-water and nor water-calcite interaction exists. In order to model the thermodynamics of Region II with water-calcite dominant interaction, a definition for Helmholtz free energy of water-calcite interaction must be derived. To this end,  $E_{conf}$  is split into fluid-fluid and fluid-wall species:

$$E_{conf} = E_{conf-ff} + E_{conf-fw} \quad (5)$$

replacing the recently defined  $E_{conf}$  in Eq. (5) with a similar term in Eq. (3) gives Eq. (6):

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} \right) V_f \exp \left( \int_{\infty}^T \frac{E_{conf-ff}}{kT^2} dT \right) \exp \left( \int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT \right) \quad (6)$$

The first three components in Eq. (6) define Helmholtz for water-water interaction, whereas the last term defines Helmholtz for water-calcite interaction.

$$Q_{N,V,T} = \exp \left( -\frac{A_{ff}}{kT} \right) \exp \left( -\frac{A_{fw}}{kT} \right) \quad (7)$$

Eq. (7) explains the partition function with respect to the Helmholtz free energy, where the natural logarithm gives:

$$\ln Q_{N,V,T} = -\frac{1}{kT} (A_{ff} + A_{fw}) \quad (8)$$

When Eqs. (8) and (7) are compared, the independent definition of the water-calcite Helmholtz contribution may be formulated as follows:

$$\left( \frac{A_{fw}}{kT} \right) = \left( -\int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT \right) \quad (9)$$

Substituting  $A_{ff}$  in Eq. (8) with the appropriate contributions yields a complete description for the thermodynamics of water confined in calcite pore:

$$\ln Q_{N,V,T} = \left( \frac{-1}{NkT} \right) (A^{hs} + A^{dis} + A^{chain} + A^{ass} + A^{ion} + A^{fw}) \quad (10)$$

The superscripts of Helmholtz species in Eq. (10) refer to the hard-sphere, dispersion, chain, association, ionic and fluid-wall interactions. The closed-form expression of the partition function with respect to the residual molar Helmholtz species is stated as below:

$$\ln Q_{N,V,T} = \left( \frac{-1}{NkT} \right) (a^{hs} + a^{dis} + a^{chain} + a^{ass} + a^{ion} + a^{fw}) \quad (11)$$

The ion species ( $a^{ion}$ ) in Eq. (11) is zero because the water is assumed pure and devoid of any ions. A bulk fluid's configurational energy is proportional to the fluid-fluid interactions occurring across the system whereas, for the confined fluid, an  $E_{conf}$  must account for the fluid-wall interactions as well. According to Eq. (2), the fluid and pore wall molecules interact through a square well. Extending the concept of  $E_{conf}$  to include fluid-wall interactions while assuming the pairwise potential for intermolecular interactions results in (supplementary information, section C):

$$E_{conf} = -\frac{N}{2} N_c \varepsilon_{ff} - N_p \varepsilon_{fw} \quad (13)$$

In Eq. (13),  $N_c$  represents coordination number and  $N_p$  is defined as:

$$N_p = N \times CF \quad (14)$$

and the following formula should be used to calculate the CF parameter:

$$CF = \frac{\rho_{RegionII}}{\rho_{RegionI}} \quad (15)$$

According to Eq. (15), the ratio density at different regions designates the CF parameter. The proposed CF carries a physical notion and depends on the properties of the fluid confined in the mineral pore. In addition to a conceptual basis, the newly defined parameter in Eq. (15) establishes a relationship between  $E_{conf}$  and the density ratio of confined fluid at various regions. From the above analysis, one can write the expression of the chemical potential of Region II as the derivative product of the partition function (supplementary information, section D):

$$\mu = kT \left( \ln(\lambda^3) - \ln \left( \frac{1}{\rho} - \frac{1}{\rho_{max}} \right) - \left( \frac{\varepsilon_{ff}}{kT} - 1 \right) - \left( \frac{\varepsilon_{fw}}{kT} \right) \right) \quad (16)$$

## 2.2. Molecular Dynamic (MD) simulations

Molecular dynamic simulation [36] was performed to investigate the structural configuration of confined water and calculate  $\rho$ ,  $\rho_{\max}$ ,  $\epsilon_{\text{fw}}$  and  $CF$  factor. A comprehensive approach for MD simulation is described in the next section.

### 2.2.1. Nanopore geometry

Fig. 2 illustrates the initial configuration of the water-calcite system inside the simulation box. The simulation box includes the mobile phase (water molecules) and immobile phase (calcite nanopore). The immobile phase is composed of two parallel calcite slabs, which enclose the water molecules with a rectangular segment normal to the  $z$ -axis. To study the effect of the pore size, we used several nanopores with fixed lengths and different widths. The pore walls were extended along the  $x$  and  $y$  axes with a length of 4 nm and 20 nm, respectively. Along the  $z$ -axis, the width of the nanopore remains fixed for each pore and varies between 1.5 nm, 2 nm, 3 nm, 4 nm, and 5 nm for various realizations. The distance between the opposing wall edge atoms identifies the pore width. The parallel calcite slabs are, composed of 6 layers of  $(10\bar{1}4)$  cleaved calcite surface with rhombohedral structure,  $R\bar{3}c$  space group, and unit cell parameters of  $a = b = 4.988 \text{ \AA}$ ,  $c = 17.061 \text{ \AA}$ ;  $\alpha = \beta = 90^\circ$ ,  $\gamma = 120^\circ$  [37]. The calcite was cleaved along the  $(10\bar{1}4)$  surface because this plane is the most stable surface of cal-

cite [38]. The water molecules were sandwiched within the nanopore with the PACKMOL [39] software.

### 2.2.2. Simulation details

The Large-scale Atomic/Molecular Massively Parallel Simulator (LAMMPS) [40] was used to run all molecular dynamic simulations. For calcite, the force field was obtained from the model developed by Raiteri et al. [41]. The SPC/Fw [42] water model, consistent with Raiteri's model, was employed to model water molecules. The long-range electrostatic interactions were calculated by the particle-particle-particle-mesh method (PPPM) [43] with a relative tolerance of  $10^{-5}$ . The periodic boundary conditions were specified for all directions, namely  $x$ ,  $y$  and  $z$ -axes. According to Raiteri's model, the cut-off 9Å was used for all short-range potentials with a taper function applied over the last 3Å. The simulation begins with the minimize function, which reduces energy by maintaining the molecules at a reasonable distance. Then, the simulation run continues with the canonical ensemble (NVT), at  $T = 300 \text{ K}$ ,  $350 \text{ K}$ ,  $400 \text{ K}$  and  $450 \text{ K}$ . The Nose-Hoover [44] thermostat was used to regulate the temperature. Each simulation took 6 ns to complete (1 ns for equilibrium and 5 ns for data production).

### 2.2.3. Model parameter extraction

To determine the Helmholtz free energy at a specific pore size and a certain temperature, primarily the confinement parameters,

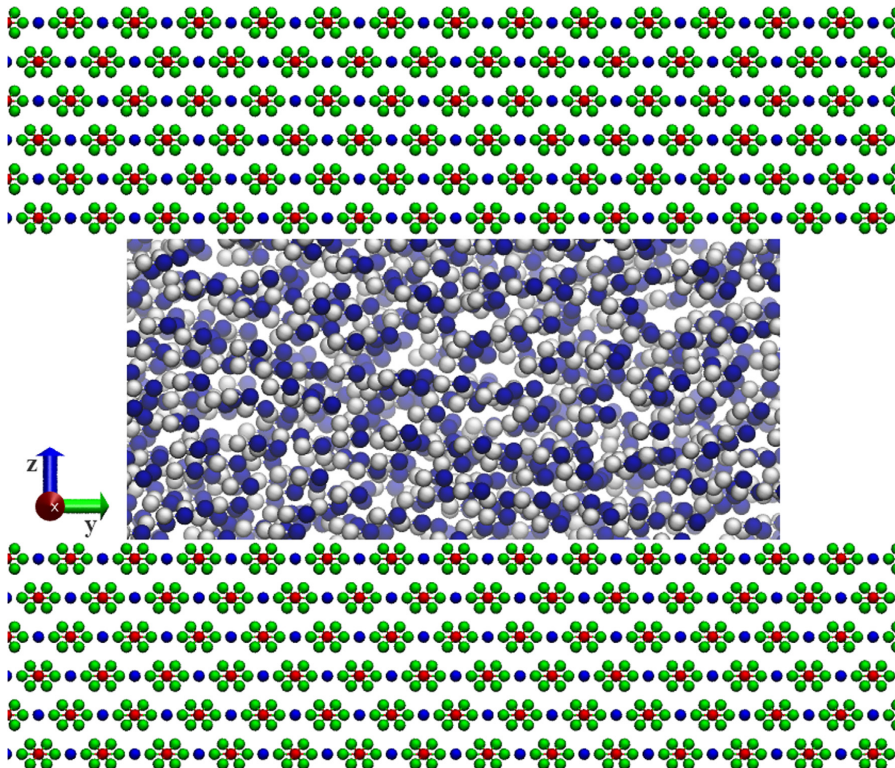
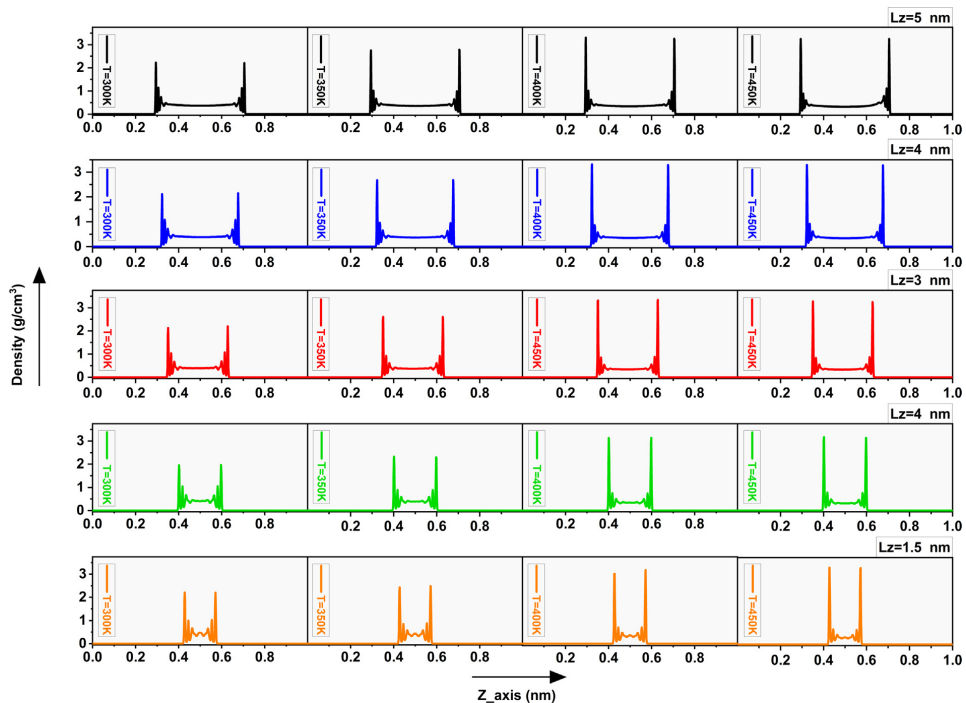


Fig. 2. Illustration of water molecules entrapped within the slit-shaped calcite nanopore, along  $y$  and  $z$ -axes. The calcite layers were cleaved along the surface  $(10\bar{1}4)$  with a fixed length of 20 nm. Along the  $z$ -axis, the pore width varies between 1.5 nm, 2 nm, 3 nm, 4 nm and 5 nm to make different pore sizes.



**Fig. 3.** Illustration of density profile inside Region I and Region II at several pore sizes and different temperatures. The plotted figures in each row and column represent the density profile at constant  $L_z$  and temperature, respectively. From left to right, the simulation temperature increases from 300 K to 450 K, while from top to bottom, the  $L_z$  increases from 1.5 nm to 5 nm.

i.e.,  $\rho$ ,  $\rho_{\max}$ ,  $\varepsilon_{fw}$  and CF factor, should be determined. In Fig. 1,  $\delta_{fw}$  represents the thickness of the layering zone inside the calcite nanopore. In order to compute  $\delta_{fw}$ , the margins of Region II must be specified. The terminus of Region III, where  $z = \sigma_i$ , is the bottom band for Region II. The top band coincides with the commencement point of Region I, where the density trend stabilizes after significant fluctuations. According to the general sketch of density profile in Figs. 3 and 4, after prominent peaks at Region II, the position in which the density experience 110% of the minimum density at the bulk-like zone is assumed the endpoint of Region II. Based on this assumption, which clarifies the thickness of  $\delta_{fw}$ , the integral product of density and energy over  $\delta_{fw}$  gives the average density and average energy within the layering zone. It implies that the integral swipes the area under the curve from  $z = \sigma_i$  to the point where Region I and II intersect.

### 3. Results and discussion

In order to calculate the confinement parameters, MD simulations were conducted. The predictions of SAFT2 were then validated against MD results.

#### 3.1. Density profile at constant $L_z$

Table 2 lists the water density determined using experiment, MD and SAFT2. The reported water densities in Table 2 correspond to the water molecules, which lacks a slit calcite nanopore. Indeed, Table 2 compares the MD, and SAFT2 results to experimental data

obtained at  $T = 300$  K, 350 K, 400 K and 450 K. As seen, without the presence of calcite pore, MD, and SAFT2 predict the water density with a reliable absolute relative error.

Fig. 3 illustrates the density profile of water along the  $z$ -axis, which is confined inside the calcite nanopore at different  $L_z$  and temperatures. The plots at each row include the density profile at constant  $L_z$ , while the parallel columns show the density profile at a constant temperature. The  $L_z$  at the first row is 5 nm, decreasing to 4 nm, 3 nm, 2 nm, and 1.5 nm from top to bottom. From left to right, the temperature increases from 300 K to 350 K, 400 K and 450 K. The observed peaks and troughs coincide with the attractive potential of the parallel calcite-walls, providing two distinct layering zones within the nanopore. The layering zones correspond to the lower and upper walls in Fig. 2, showing the density profile within Region II. In other words, the large density oscillations at the left and right sides of the plots in Fig. 3 detect the boundary of Region II adjacent to the lower and upper walls in Fig. 2. In Fig. 3, the side density oscillations of each pore are considerably higher amplitude than the center ones, leading to a lower density than near the wall. The density trends from both sides then overlap at the middle, forming boundaries of Region I with lower density.

Fig. 4 compares the density profile along the  $z$ -axis at fixed confinement and different temperatures. For  $L_z = 5$  nm, 4 nm, 3 nm, 2 nm and 1.5 nm, the density decreases within the bulk-like zone and increases at the layering zone with raising the temperature. To be specific, at each confinement, the color sequence of curves within the bulk-like zone starts from blue at the bottom and reaches red at the top, indicating that low temperature leads to higher density. This observation is similar to the thermodynamic



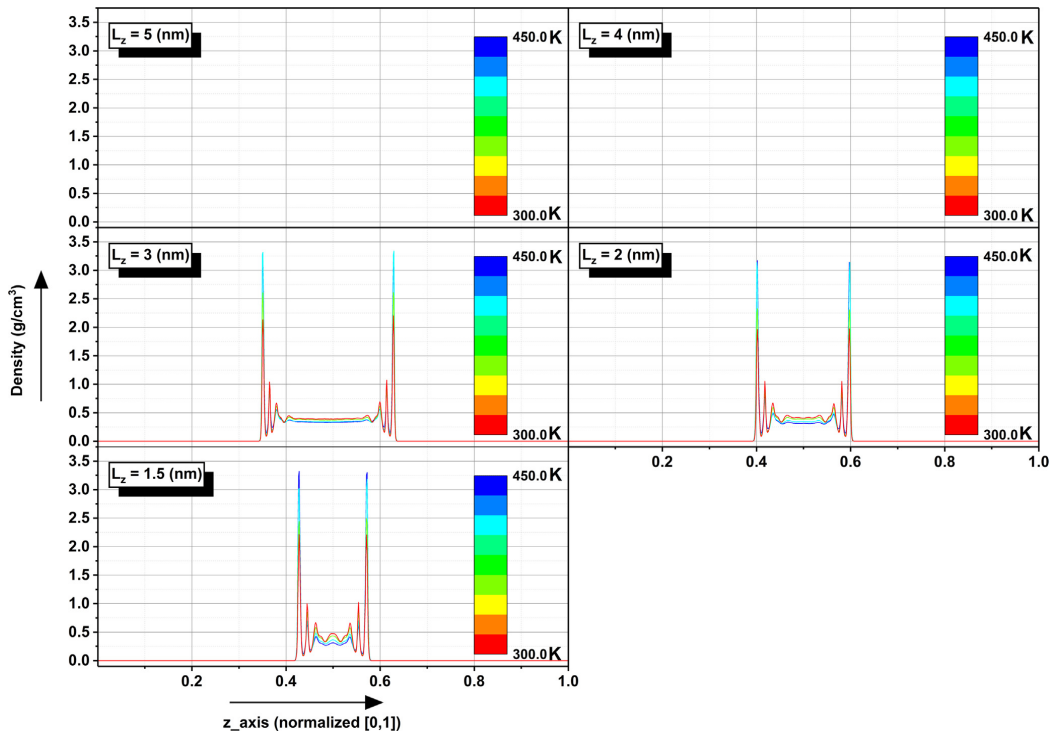


Fig. 4. Comparison of density profile inside Region I and Region II at fixed  $L_z$  and different temperatures. The cool-warm colors show the temperature variation. Within Region I, the density decreases by increasing the temperature. Inside Region II, higher temperature provides higher density values.

Table 2

List of the water density at different temperatures without the presence of calcite-wall. This table compares the laboratory data with the outcomes of MD, and SAFT2. The columns RE-1 and RE-2 display the relative error for MD and SAFT2, respectively.

T [K]	Liquid water density				
	Laboratory [kg/m <sup>3</sup> ] [45]	MD [kg/m <sup>3</sup> ]	SAFT2 [kg/m <sup>3</sup> ]	ARE-1 %	ARE-2 %
300	996.499	1000.003	996.779	0.351	0.028
350	973.693	970.383	973.567	0.339	0.013
400	937.465	923.463	936.508	1.494	0.102
450	890.319	861.221	890.234	3.268	0.954

behavior of water without the presence of a calcite pore, showing that the density inside Region I is controlled by the water-water molecule distance. In contrast, in the bottom-top view, the colors are sorted from red to blue within the layering zone as the temperature rises from low to high. The reason refers to detaching the water molecules from resided water molecules in Region I and joining the layering zone due to thermal expansion because the water molecules inside Region I have more freedom than those in Region II. Therefore, as the temperature rises, the distance between the water molecules in the bulk-like zone increases, resulting in a reduction in density.

On the other hand, a rise in temperature traps the water molecules in the layering zone, leading to an increase in density. For  $L_z = 1.5$  nm, the density behavior at the middle of pore space differs from the observed density trend for  $L_z = 5$  nm, 4 nm, 3 nm and 2 nm. In other words, for the confinements larger than  $L_z = 1.5$  nm, the density trend experience a minimum at the middle of slit-pore

calcite. However, for  $L_z = 1.5$  nm, the density trends overlap at the middle of the pore after some oscillations. For  $L_z = 1.5$  nm, although the density has not experienced a minimum, the density value at the center of the pore still remains less than the density peaks within the layering zone.

The distinct behavior of density trends within Regions I and II highlights diverse interactions within regions located inside the calcite nanopore. This categorial pattern actually supports our assumptions for Eqs. (1) and (2), which state that the dominant interactions in Regions I and II are water-water and water-calcite interactions, respectively.

In order to calculate the average density within Region II, the integral product of the density curve within the layering zone was estimated according to the mentioned approach in Section 2.2.3. Table 3 shows the results of the integral product at various temperatures within the layering zone. According to MD predictions in Table 3, with fixed temperature, the density

**Table 3**  
The average density within Region II, calculated with MD simulation.

Lz [nm]	MD [kg/m <sup>3</sup> ]			
	T = 300 K	T = 350 K	T = 400 K	T = 450 K
15	538.611	540.534	554.982	588.772
20	535.330	538.349	558.196	598.881
30	543.881	565.724	603.235	633.732
40	544.459	570.622	619.335	633.900
50	561.334	584.642	626.310	664.964

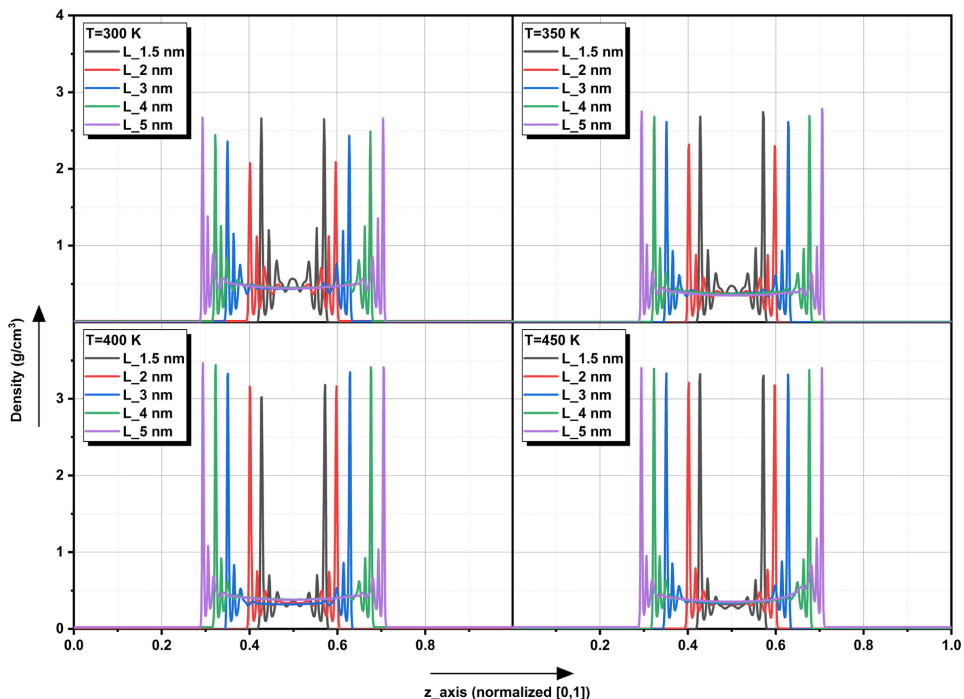
increases by increasing the pore size ( $L_z$ ). Namely, larger  $L_z$  provides a higher density value within the layering zone. In addition, at constant  $L_z$ , the density increases with the rise in temperature from 300 K to 450 K.

### 3.2. Density profile at a constant temperature

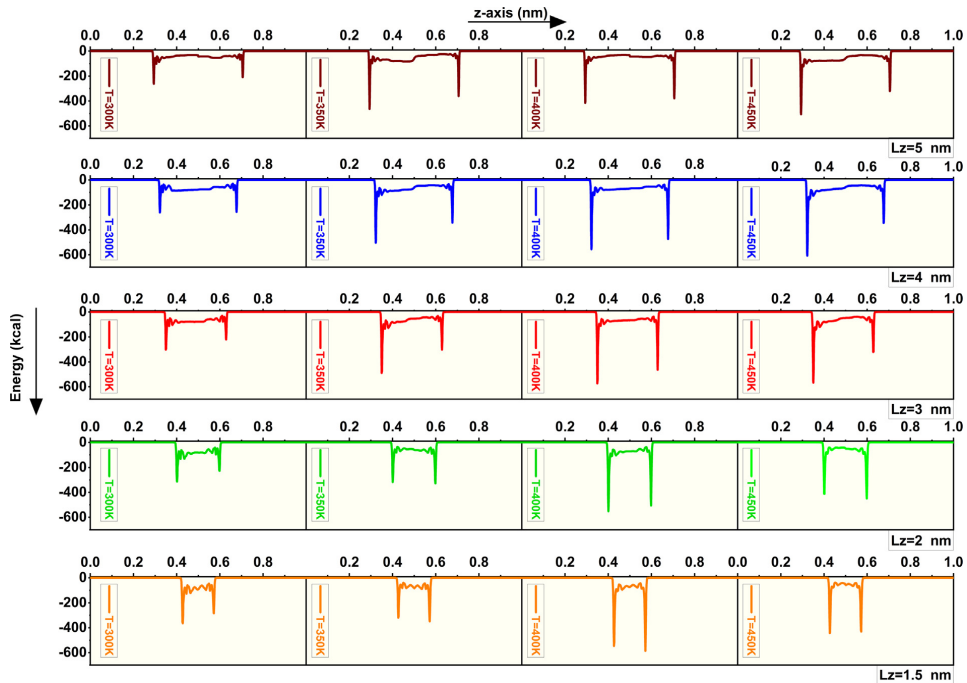
Fig. 5 shows the density profile at constant temperature and various  $L_z$ . The plots in Fig. 5 are presented versus normalized  $L_z$  so that various trends on a given axis may be easily compared. As seen at the top left corner, with  $T = 300$  K, pore size varies as  $L_z = 5$  nm to 4 nm, 3 nm, 2 nm, and 1.5 nm. Following the same  $L_z$  trend, the temperature increases to  $T = 350$  K,  $T = 400$  K, and  $T = 450$  K in the other plots. As can be observed, the area under the curve in Region I and Region II develops as  $L_z$  increases from 1.5 nm to 2 nm, 3 nm, 4 nm, and 5 nm at a fixed temperature. In other words, as the pore size rises and the temperature remains constant, the average density within the layering zone and central zone increases. This is owing to the integral product results, which

show that the average density of the layering zone and central zone grow with  $L_z$  size. Beyond the mathematical reason, it is expected that the average density within the layering zone approaches  $\rho_{\max}$  because when the pore size extends along the z-axis ( $L_z \rightarrow \infty$ ), the confined water behavior approaches bulk behavior.

As the pore sizes become narrower, the oscillations become less pronounced until  $L_z = 1.5$  nm, exhibiting a unique behavior, as seen in Figs. 4 and 5. Because the threshold of short-range potentials (i.e., cut-off) is set to 9 Å in MD simulations, causing the attractive potentials from both walls to overlap. In other words, for  $L_z = 1.5$  nm, all water molecules inside the pore space are affected by pore-wall attraction which leads to the disappearance of the bulk-like zone. To sum up, when an associating fluid such as water is confined within a calcite nanopore, different zones in the density profile arise due to the contest between water-water and water-calcite interactions. Because the water-calcite interaction is prominent inside the layering zone, the tiny pore sizes with tighter confined water are more influenced. It means that as the pore size



**Fig. 5.** Comparison of density profile at fixed temperature and different  $L_z$ . By increasing the  $L_z$  from 1.5 nm to 2 nm, 3 nm, 4 nm, and 5 nm, the area under the curve extends, which means the integral product results in a larger average density within Region II.



**Fig. 6.** Illustration of energy profile inside Region I and Region II at several  $L_z$  and different temperatures. The plotted figures in each row and column represent the energy trend at constant  $L_z$  and temperature, respectively. From left to right, the simulation temperature increases from 300 K to 350 K, 400 K and 450 K, while from top to bottom, the  $L_z$  decreases from 5 nm to 4 nm, 3 nm, 2 nm and 1.5 nm.

increases, the calcite-wall attraction over confined water diminishes and the average density within the layering zone approaches the bulk density. Therefore, the rise in pore size results in a larger average density within the layering zone.

### 3.3. Energy behavior

Fig. 6 displays the trend of the total energy at different  $L_z$  and temperatures. The parallel columns display the energy trend at constant temperature and  $L_z = 5$  nm, 4 nm, 3 nm, 2 nm, and 1.5 nm. The horizontal rows depict the energy variation along the z-axis at constant pore size and  $T = 300$  K, 350 K, 400 K and 450 K.

Within each row, the length of the energy peaks inside Region II increases by increasing the temperature. At the same time, the average energy is diminished within Region I. The average energies within Region II have been reported in Table 4 at different  $L_z$  and temperatures. To calculate the average energy amount, we utilized the same approach as the average density mentioned in Section 2.2.3. The general trend of energy follows the general profile in Fig. 3 and Fig. 4, although there are some deviations. The deviation refers to the fact that the average energy depends not only on intermolecular distance but also on the polarity of the surrounded molecules. Hence, reduction of intermolecular distances will not necessarily increase the average energy. As seen, inside Region I, far from the calcite-walls attractions, the water-water molecule

**Table 4**

Estimated confinement parameters with MD simulations. The  $\epsilon_{fw}$ ,  $\rho_{max}$  and CF respectively present the potential of water-calcite interaction, bulk-like density and fraction of confined molecules.

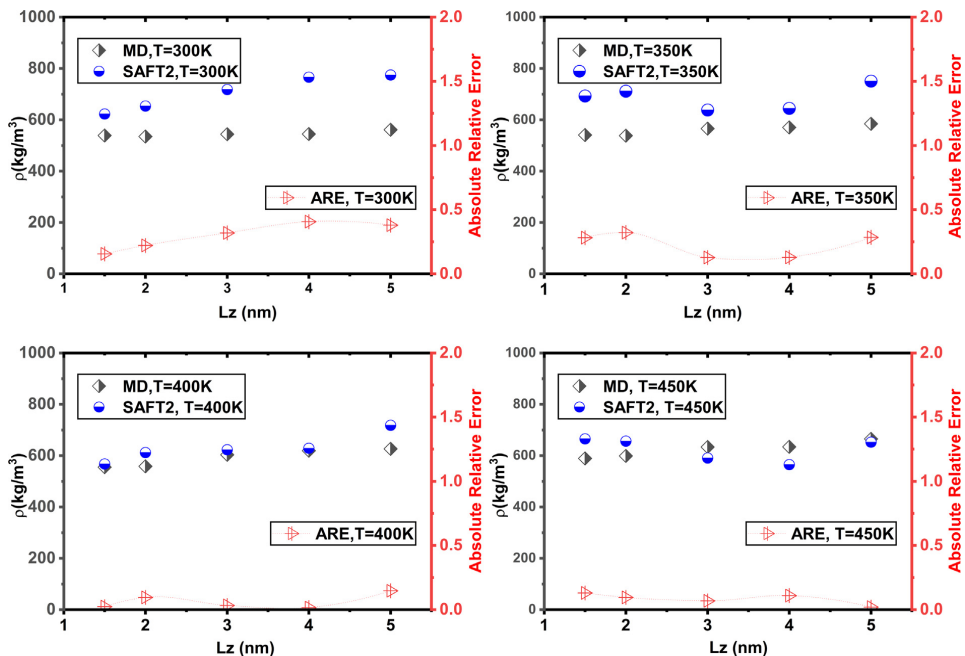
T = 300 [K]			
$L_z$ [nm]	$\rho_{max}$ [kg/m <sup>3</sup> ]	$\epsilon_{fw}$ [kcal/mol]	CF
1.5	1000.003	-104.812	1.265
2	1000.003	-97.054	1.274
3	1000.003	-80.955	1.352
4	1000.003	-68.595	1.358
5	1000.003	-66.359	1.418
T = 350 [K]			
1.5	970.383	-87.265	1.356
2	970.383	-82.545	1.355
3	970.383	-100.997	1.467
4	970.383	-99.374	1.479
5	970.383	-72.459	1.520
T = 400 [K]			
1.5	923.463	-118.846	1.621
2	923.463	-107.626	1.582
3	923.463	-104.772	1.694
4	923.463	-103.333	1.693
5	923.463	-80.896	1.684
T = 450 [K]			
1.5	861.221	-94.175	1.962
2	861.221	-96.512	1.821
3	861.221	-113.021	1.803
4	861.221	-119.647	1.737
5	861.221	-97.356	1.804

distance controls the density and energy. Whereas, within Region II, which is close to calcite-wall, water-calcite interaction and polarity of the molecules in the neighborhood control the total energy.

Raising the  $L_z$  causes a rise in the average energy within Region I. This is because when  $L_z$  increases, the confined water approaches the bulk behavior and water-water molecule distance decreases due to the growth in density. Namely, the calcite-wall shows a

**Table 5**  
Comparison of MD and modified SAFT2 at different  $L_z$  and temperatures within Region II.

$L_z$ [nm]	MD [kg/m <sup>3</sup> ]			
	T = 300 K	T = 350 K	T = 400 K	T = 450 K
15	538.611	540.534	554.982	588.772
20	535.330	538.349	558.196	598.881
30	543.881	565.724	603.235	633.732
40	544.459	570.622	619.335	633.900
50	561.334	584.642	626.310	664.964
$L_z$ [nm]	Modified SAFT2 [kg/m <sup>3</sup> ]			
	T = 300 K	T = 350 K	T = 400 K	T = 450 K
15	622.658	692.575	567.507	665.047
20	653.560	711.284	611.498	655.722
30	717.403	637.836	622.817	590.227
40	765.694	644.305	628.537	564.407
50	774.111	750.790	717.793	652.355
$L_z$ [nm]	Modified SAFT2-include CF coefficient [kg/m <sup>3</sup> ]			
	T = 300 K	T = 350 K	T = 400 K	T = 450 K
15	466.654	572.643	459.406	603.770
20	507.362	597.384	504.684	581.898
30	605.191	520.258	531.130	505.224
40	672.326	529.900	537.765	469.555
50	691.367	670.805	644.483	576.480



**Fig. 7.** The graph compares MD and modified SAFT2 predictions for T = 300 K, 350 K, 400 K, and 450 K. The diamond reflects MD findings, whereas the circles indicate modified SAFT2 results without taking the CF factor into account. The profile of absolute relative error at the bottom of each plot box depicts the divergence of modified SAFT2 from MD results. The Absolute Relative Error is higher with T = 300 K and T = 350 K, as can be observed.

stronger attraction to the thin water than the thick one. However, no consistent trend is detected within Region II. As can be seen, the average energy responds differently as the pore size rises at a constant temperature. This is because, inside Region II, the distance between water molecules does not determine the energy value, and other parameters, such as the polarity of the closed neighbors, come into play. Therefore, a larger pore size at a constant temperature necessarily does not give larger average energy.

The estimated confinement parameters with MD simulation are shown in Table 4. The  $\epsilon_{fw}$ ,  $\rho_{max}$  and CF respectively present the potential of water-calcite interaction, bulk-like density and fraction of confined molecules. The given values for  $\rho_{max}$  are identical to those calculated in Table 2 with MD.

### 3.4. Comparison of SAFT2 and MD simulation

Table 5 presents calculated confinement parameters under different confinement sizes and temperatures. Water was simulated using MD without the presence of the slit-pore calcite in order to calculate the bulk density. The integral of the energy distribution throughout the layering zone was utilized to calculate the potential of water-calcite interaction. The CF factor, or the fraction of confined molecules, was determined by  $\rho_{RegionII}/\rho_{RegionI}$ .

As indicated in Table 5, the calculated confinement parameters were entered into the modified SAFT2 to estimate the water density inside Region II. Table 5 shows the MD and modified SAFT2 projections for Region II. The graphs in Figs. 7 and 8 provide a comparison between the outcomes of MD and modified SAFT2. The vertical axis shows the Absolute Relative Error (ARE) on the right hand side of the graphs. It reflects the divergence of modified SAFT2 from the MD findings. The density values predicted by MD and

modified SAFT2 are shown on the vertical axis at the left hand side. It is important to note that the CF factor is applied to Fig. 8, while it is not applied at either temperature in Fig. 7. To be specific, the circles represent modified SAFT2 findings that were obtained without taking the CF factor into consideration, while the squares represent modified SAFT2 results that were obtained with the CF factor taken into account. The diamond represents MD results, while the triangles represent the ARE.

Fig. 7 shows that when  $T = 400$  K and  $T = 450$  K, the predictions of modified SAFT2 match well with MD. However, when  $T = 300$  K and  $T = 350$  K, the reported ARE is relatively high. The increase of ARE refers to the overestimation of modified SAFT2 at low temperatures. It means, at low temperatures, the coupled  $\epsilon_{fw}$  to Helmholtz term was not able to reduce the gap between modified SAFT2 and MD. Because, water molecules confined at low temperatures are in order and under the effect of additional confinement constraints such as layering patterns, confinement geometry and the mutual interaction of distinct regions, amongst others. Hence, the high temperature may reduce the impact of the confinement restrictions described above by raising the kinetic energy of the water molecules inside the pore and allowing them to move more freely within the pore. Thus, high temperature is able to diminish the constraint imposed on confined water. On the other hand, the error attributed to the water model owing to high temperature is negligible because in this simulation the maximum temperature does not exceed than 450 K.

Therefore, the SPC/Fw model fairly accurately predicts the thermodynamic properties of water in MD simulations. In order to compensate for the confinement effect at low temperatures, the contribution of  $\epsilon_{fw}$  could be improved by multiplying by a coefficient inspired by the thermodynamic property of the confined

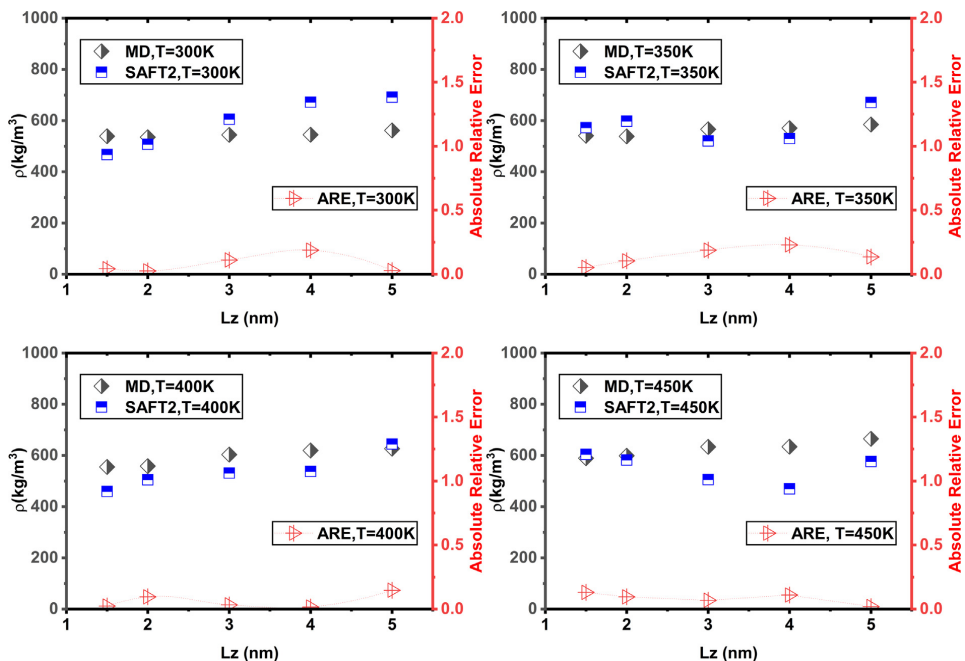


Fig. 8. The graph compares MD and modified SAFT2 predictions for  $T = 300$  K, 350 K, 400 K, and 450 K. The diamonds indicate the MD outcomes. The squares illustrate the results of the modified SAFT2 when the CF factor is taken into account. The profile of absolute relative error at the bottom of each plot box depicts the divergence of modified SAFT2 from MD results.

water. To be specific, the newly introduced coefficient CF in Eq. (15) was applied to improve the predictions of modified SAFT2 at low temperatures.

The application of the CF factor at  $T = 300$  K and  $T = 350$  K decreased the divergence between MD and SAFT2, as seen in Fig. 8. While at  $T = 400$  K and  $T = 450$  K, approximately the same results are repeated as Fig. 7. This behavior supports our argument that high temperature diminishes the additional confinement effects that arise at low temperatures.

Our results in Fig. 8 indicate the predictions of modified SAFT2 correspond very well with MD, by taking into account  $\epsilon_{fw}$  at  $T = 400$  K and  $T = 450$  K. According to the ARE trend in Fig. 8, the CF factor at  $T = 300$  K,  $T = 350$  K,  $T = 400$  K and  $T = 450$  K has narrowed the gap between MD and modified SAFT2.

#### 4. Summary and conclusions

We have applied MD simulations to capture the interactions between confined fluid and mineral-wall inside the nanopores. In this approach, several slit-pores of calcite with fixed length and variable width, i.e., 1.5 nm, 2 nm, 3 nm, 4 nm and 5 nm, were simulated. The water molecules were sandwiched in between the calcite slabs to interact with the rigid walls of the slit nanopore. To incorporate the calcite-walls (mineral) effect into the confined water (fluid) thermodynamic properties, we used first principles to derive a term for Helmholtz energy contribution extended from SAFT2. To calculate the Helmholtz term for water-calcite interaction, the confinement parameters of slit nanopore, namely  $\epsilon_{fw}$  and  $\rho_{max}$ , needed to be calculated in advance. The confinement parameters were then calculated by MD simulation. The predictions of modified SAFT2 were validated versus MD results. A newly defined physical parameter CF is incorporated with modified SAFT2 deriving from MD results. Coupling CF with proposed EoS reduced the ARE by roughly 50% at low temperatures, resulting in satisfactory agreement with MD at all temperatures.

In conclusion, inside the layering zone, the density and energy deviate from the bulk value owing to the attraction of the rigid pore walls. Temperature causes density in Region II to rise, whereas it causes density in Region I to drop. Because in the bulk-like zone, fluid-fluid interaction is predominant, while in the layering zone, the fluid-mineral interaction is dominant. The newly introduced physical parameter, the CF factor, demonstrates that the thermodynamic of the confined fluid in the nanoscale pore depends not only on the fluid-mineral interaction potential but also on the geometry, layering pattern, the mutual interaction of different regions, which is the consequence of the rise in the surface-to-volume ratio at the nanoscale. This finding paves the way for further study into how additional constraints influence the characteristics of associating confined fluids.

#### CRedit authorship contribution statement

**S. Ahmadi G.:** Conceptualization, Methodology, Software, Validation, Writing – original draft, Visualization, Formal analysis, Investigation, Writing – review & editing. **R. Miri:** Software, Supervision, Writing – review & editing. **P. Aagaard:** Supervision, Writing – review & editing. **H. Hellevang:** Supervision, Writing – review & editing.

#### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.molliq.2021.118045>.

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Corrigendum

Corrigendum to “Extension of SAFT equation of state for fluids confined in nano-pores of sedimentary rocks using molecular dynamic simulation” [J. Mol. Liquids (348) (2022) 118045]



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The authors regret to notify the Journal of Molecular Liquids that Fig. 4 from above-mentioned article was not entirely printed out. In other words, Fig. 4 should have five boxes, each containing the density profiles relevant to a specific  $L_z$ . However, as shown in the published article, the curves for  $L_z = 5$  nm and  $L_z = 4$  nm are missing.

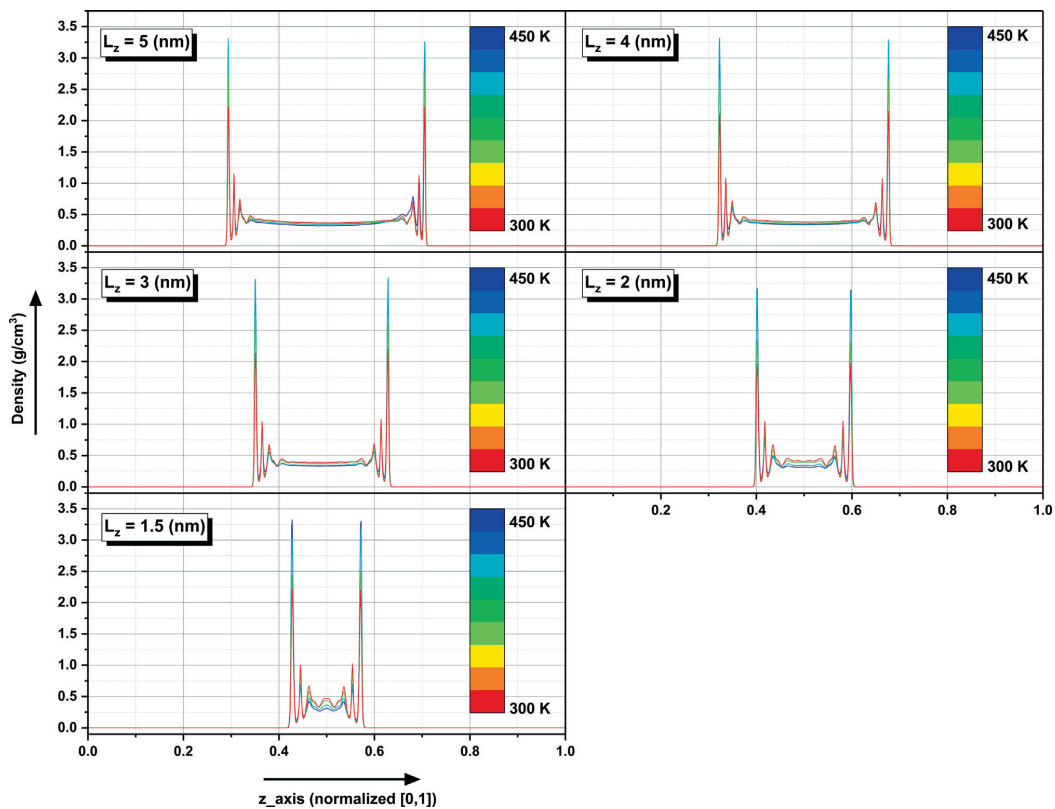
It is worth to note that Fig. 4 addresses a key aspect of the research work and the present published Fig. is considered as a critical error. The authors would appreciate if the editorial team could replace the previous version of Fig. 4 with a newly attached one and publish a Corrigendum in a forthcoming issue.

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The authors would like to apologise for any inconvenience caused.

1 **Supplementary Information**

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4  
5 **Extension of SAFT Equation of State for Fluids Confined in Nano-**  
6 **pores of Sedimentary Rocks Using Molecular Dynamic Simulation**

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30 **Section A: Partition Function**

31 The canonical partition function,  $Q$ , is defined as follows for a system of  $N$  identical particles of  
 32 mass  $m$ .

$$Q_{N,V,T} = \frac{q_{\text{int}}}{N!} \frac{1}{h^{3N}} \int \int dp^N dr^N \exp\left(-\frac{H(p^N, r^N)}{kT}\right) \quad (\text{A.1})$$

33

34 Where  $h$  represents Planck's constant,  $T$  denotes the temperature and  $k$  is the Boltzmann constant.  
 35 The factor  $N!$  vanishes when the particles are distinguishable. In Equation (A.1),  $q_{\text{int}}$  is the internal  
 36 partition function. The Hamiltonian  $H(p^N, r^N)$  represents the total energy of the system. The  
 37 Hamiltonian is defined as the sum of the system's kinetic and potential energies, as shown below.

$$H(p^N, r^N) = \sum_{i=1}^N \frac{|p_i|^2}{2m} + u(r^N) \quad (\text{A.2})$$

38

39 Thus we have

$$Q_{N,V,T} = \frac{q_{\text{int}}}{N!} \frac{1}{h^{3N}} \int dp^N \exp\left(-\frac{|p_i|^2}{2mkT}\right) \int_V \int dr^N \exp\left(-\frac{u(r^N)}{kT}\right) \quad (\text{A.3})$$

40

41 The analytical solution of the momenta integral product is as follows:

$$\int dp^N \exp\left(-\frac{|p_i|^2}{2mkT}\right) = (2\pi mkT)^{\frac{3N}{2}} \quad (\text{A.4})$$

42

43 In Equation (A.7),  $m$  is the mass of the particle and  $\pi=3.14$  is the result of the Gaussian integral.

44 Thus we have

$$Q_{N,V,T} = \frac{q_{\text{int}}}{N!} \frac{1}{h^{3N}} (2\pi mkT)^{\frac{3N}{2}} \int_V \int dr^N \exp\left(-\frac{u(r^N)}{kT}\right) \quad (\text{A.5})$$

45

46 The configuration integral  $Z$  is defined as the integral product of all positions:

$$Z_{N,V,T} = \int_V \int dr^N \exp\left(-\frac{u(r^N)}{kT}\right) \quad (\text{A.6})$$

47

48 the de Broglie thermal wavelength  $\lambda$  is defined as:

$$\lambda = \sqrt{\left(\frac{h^2}{2\pi mkT}\right)} \quad (\text{A.7})$$

49

50 Thus we have:

$$Q_{N,V,T} = \frac{q_{\text{int}}}{N!} \frac{1}{\lambda^{3N}} Z_{N,V,T} \quad (\text{A.8})$$

51

## 52 Section B: Configurational Energy

53 Once the partition function is determined, to calculate various thermodynamic properties from  
54 canonical partition function, the easiest starting point is the Helmholtz free energy:

$$A = -k_b T \ln(Q) \quad (\text{B.1})$$

55

56 To calculate the entropy  $S$ , one can write the Helmholtz free energy in differential form:

$$dA = \left(\frac{\partial A}{\partial T}\right)_{V,N} dT + \left(\frac{\partial A}{\partial V}\right)_{T,N} dV \quad (\text{B.2})$$

57

58 By Comparison of Equation (B.2) with characteristics function of  $A$  in Equation (B.3)

$$dA = -SdT - PdV \quad (\text{B.3})$$

59

60 The entropy  $S$  therefore can be written as:

$$S = -\left(\frac{\partial A}{\partial T}\right)_{V,N} = k \left[ \ln Q + T \left(\frac{\partial \ln Q}{\partial T}\right)_{V,N} \right] \quad (\text{B.4})$$

61

62 The internal energy  $U$  then can be written with respect to the  $A$ ,  $T$  and  $S$ :

$$A = U - TS \Rightarrow U = A + TS \quad (\text{B.5})$$

63

64 Substitution of  $S$  from Equation (B.4) into Equation (B.5) then gives:

$$U = -kT \ln Q + kT \ln Q + kT^2 \left(\frac{\partial \ln Q}{\partial T}\right)_{V,N} = kT^2 \left(\frac{\partial \ln Q}{\partial T}\right)_{V,N} \quad (\text{B.6})$$

65

66 Equation (B.7) can be used to determine the configurational energy, which is the difference  
67 between the internal energy of a real fluid and the internal energy of an ideal gas [29]:

$$E_{conf} = U_{N,V,T} - U_{N,V,T}^{ig} = kT^2 \left( \frac{\partial \ln Z}{\partial T} \right)_{V,N} \quad (\text{B.7})$$

68

69 When Equation (B.7) is substituted into Equation (A.8), the result is:

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} \right) V_f^N \exp \left( \int_{\infty}^T \frac{E_{conf}}{kT^2} dT \right) \quad (\text{B.8})$$

70

71 In Equation (B.7),  $V_f$  represents the free volume, namely the volume which is excluded by the fluid  
72 molecule and defined as follows:

$$V_f = V - \frac{N}{\rho_{max}} \quad (\text{B.9})$$

73

74 In Equation (B.9), The closed packed density is shown with  $\rho_{max}$ . Considering the calcite-wall  
75 effect let to split the into fluid-fluid and fluid-wall species

$$Q_{N,V,T} = \left( \frac{q_{int}^N}{\lambda^{3N} N!} \right) V_f^N \exp \left( \int_{\infty}^T \frac{E_{conf-ff}}{kT^2} dT \right) \exp \left( \int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT \right) \quad (\text{B.10})$$

76

77  $E_{conf-ff}$  and  $E_{conf-fw}$  represent the configurational energy for fluid-fluid and fluid-wall, respectively.

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89 **Section C: Configurational energy of fluid-wall interaction: pure fluid**

90 A bulk fluid's configurational energy is proportional to the fluid-fluid interactions occurring  
 91 across the system. On the other hand, for the confined fluid, an  $E_{conf}$  model must account for the  
 92 fluid-wall interactions. According to Equation (1), the fluid and pore wall molecules interact  
 93 through a square well. For a system with  $N$  molecules in volume  $V$  and temperature  $T$ , the  $E_{conf}$ ,  
 94 or average total interaction energy, is defined as

$$E_{conf} = \frac{N^2}{2V} \int u(r)g(r, \rho) dr \quad (C.1)$$

95

96 Where the intermolecular interaction energy  $u$  is assumed pairwise additive. By this hypothesis,  
 97 the interaction energy equals the sum of every single pair interaction as following:

$$u(r_1, r_2, \dots, r_N) = \sum_i \sum_j u(r_{ij}) \quad (C.2)$$

98

99 In Equation (C.1),  $g(\rho, r)$  is radial distribution function [32] which is defined as:

$$g(r) = \begin{cases} 0 & r_{ij} < \sigma_{ij} \\ \exp\left(\frac{\epsilon_{ij}}{kT}\right) & \sigma_{ij} < r_{ij} < \sigma_{ij} + \delta_{ij} \\ 1 & r_{ij} > \sigma_{ij} + \delta_{ij} \end{cases} \quad (C.3)$$

100

101 In Equation (C.3),  $r$  is the distance between two molecules,  $\sigma$  is the average molecule diameter,  
 102 and  $\delta$  is the width of the square well. To implement the integral product, we must substitute  $g(\rho, r)$   
 103 and  $u(r)$  in Equation (C.1). Assuming that  $g(\rho, r)$  inside the bulk and forbidden zone equal 1 and 0,  
 104 respectively, we get

$$\begin{aligned} E_{conf} &= \frac{N^2}{2V} \int u(r)g(r, \rho) dr \\ &= \frac{N^2}{2V} \int (u(r) \times g(r, \rho)) dr + \frac{N^2}{2V} \int (u(r) \times g(r, \rho)) dr + 0 \end{aligned} \quad (C.4)$$

105

106 Substituting the potentials from Equation (1) and (2) in the manuscript gives:

107

$$E_{conf} = \frac{N^2}{2V} \int (-\varepsilon_{ff} \times g(r, \rho)) dr + \frac{N^2}{2V} \int (-\varepsilon_{fw} \times g(r, \rho)) dr \quad (C.5)$$

108

109 Due to the water-calcite interaction, the 2 in the second component of Equation (C.5) decreases to

110 1. Thus, we have the following:

$$\begin{aligned} E_{conf} &= -\frac{N}{2} \varepsilon_{ff} \frac{N}{V} \int g(r, \rho) dr + \frac{N}{V} \varepsilon_{fw} \int g(r, \rho) dr \\ &= -\frac{N}{2} \varepsilon_{ff} \left( \frac{N}{V} C \right) + \left( N \frac{C'}{V} \right) \varepsilon_{fw} \\ &= -\frac{N}{2} N_C \varepsilon_{ff} + N_P \varepsilon_{fw} \\ E_{conf} &= -\frac{N}{2} N_C \varepsilon_{ff} + N_P \varepsilon_{fw} \end{aligned} \quad (C.6)$$

111

## 112 Section D: Chemical Potential

113 Chemical potential is defined as the amount of energy that may be absorbed or released when the

114 number of particles in a given species varies. Taking into account that the water in this

115 simulation is supposed to be pure, we have:

$$\mu = \left( \frac{\partial A}{\partial N} \right)_{T,V} \quad (D.1)$$

116

117 Equation (D.1) means the chemical potential equals the partial derivative of Helmholtz free energy

118 with respect to the number of moles. According to Equation (D.1), the chemical potential remains

119 constant as long as the corresponding natural variables, temperature and volume, are held constant.

120 To recall from Equation (B.1), once the partition function is determined, it is possible to calculate

121 the Helmholtz free energy as below:

$$A = -k_b T \ln(Q) \quad (D.2)$$

122

123 The chemical potential also is defined as:

$$\mu = -k_b T \left( \frac{\partial \ln Q}{\partial N} \right)_{T,V} \quad (D.3)$$

124

125 When Equations (D.1) and (D.2) are compared, it becomes clear that Equation (D.3) provides a  
 126 straightforward method for estimating the chemical potential from the partition function. Equation  
 127 (D.3) means the chemical potential equals the partial derivative of the natural logarithm of the  
 128 partition function with respect to the number of moles.

129 To derive a proper definition for  $A$ , we have:

$$A = -kT \ln \left( \left( \frac{V_f^N}{\lambda^{3N} N!} \right) \exp \left( \int_{\infty}^T \frac{E_{conf-ff}}{kT^2} dT \right) \exp \left( \int_{\infty}^T \frac{E_{conf-fw}}{kT^2} dT \right) \right) \quad (D.4)$$

130

131 Replacing the  $E_{conf-ff}$  and  $E_{conf-fw}$  with the energy per particle i.e.  $\mathcal{E}_{conf-ff}$  and  $\mathcal{E}_{conf-fw}$  gives:

$$\begin{aligned} A &= -kT \left( \ln \left( \frac{V_f^N}{\lambda^{3N} N!} \right) + \left( N \int_{\infty}^T \frac{\mathcal{E}_{conf-ff}}{kT^2} dT \right) + \left( N \int_{\infty}^T \frac{\mathcal{E}_{conf-fw}}{kT^2} dT \right) \right) \\ &= -kT \left( -3N \ln(\lambda) + \ln(V_f^N) - \ln(N!) + \left( N \frac{\mathcal{E}_{conf-ff}}{kT} \right) + \left( N \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \end{aligned} \quad (D.5)$$

132

133 Using the Stirling approximation to expand the factorial gives:

$$\begin{aligned} A &= -kT \left( -3N \ln(\lambda) + N \ln(V_f) - N \ln N - N + \left( N \frac{\mathcal{E}_{conf-ff}}{kT} \right) + \left( N \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= -NkT \left( -3 \ln(\lambda) + \ln V_f - \ln N - 1 + \left( \frac{\mathcal{E}_{conf-ff}}{kT} \right) + \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= NkT \left( \ln(\lambda^3) - \ln V_f + \ln N + 1 - \left( \frac{\mathcal{E}_{conf-ff}}{kT} \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= NkT \left( \ln(\lambda^3) + \ln \left( \frac{N}{V_f} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= NkT \left( \ln(\lambda^3) + \ln \left( \frac{N}{V_f} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \end{aligned}$$



$$A = NkT \left( \ln(\lambda^3) + \ln \left( \frac{N}{V_f} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \quad (D.6)$$

134

135 By plugging the definition of  $V_f$  from Equation (B.9) into Equation (D.6), we have:

$$\begin{aligned} A &= NkT \left( \ln(\lambda^3) + \ln \left( \frac{N}{V - \frac{N}{\rho_{\max}}} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= NkT \left( \ln(\lambda^3) + \ln \left( \frac{N}{\frac{N}{\rho} - \frac{N}{\rho_{\max}}} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ &= NkT \left( \ln(\lambda^3) - \ln \left( \frac{1}{\rho} - \frac{1}{\rho_{\max}} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \\ A &= NkT \left( \ln(\lambda^3) - \ln \left( \frac{1}{\rho} - \frac{1}{\rho_{\max}} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \end{aligned} \quad (D.7)$$

136

137 To derive a proper definition for  $\mu$  one can use the definition of chemical potential in Equation  
138 (D.1):

$$\mu = kT \left( \ln(\lambda^3) - \ln \left( \frac{1}{\rho} - \frac{1}{\rho_{\max}} \right) - \left( \frac{\mathcal{E}_{conf-ff}}{kT} - 1 \right) - \left( \frac{\mathcal{E}_{conf-fw}}{kT} \right) \right) \quad (D.8)$$

139



Paper III

# **Drivers of Low Salinity Effect in Carbonate Reservoirs Using Molecular Dynamics Simulation**

**Sajjad Ahmadi Goltapeh, Saeed Abdolahi, Jens Sigurd Jahren, Rohaldin Miri and Helge Hellevang**

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## Drivers of Low Salinity Effect in Carbonate Reservoirs Using Molecular Dynamic Simulation

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## ABSTRACT

Low salinity water (LSW) flooding has yielded promising results in improving the enhanced oil recovery (EOR) techniques in sandstone and carbonate reservoirs. Despite various studies and advances, the main mechanism behind the oil displacement in the rock-brine-oil system is unclear. To get a better understanding of the governing mechanisms, we used the molecular dynamic (MD) method to simulate a system including calcite-brine-oil under two different scenarios. At  $T=300$  K and  $T=360$  K each scenario is completed during 40 ns using a canonical ensemble. The results show that all mono/divalent ions are hydrated initially. Furthermore,  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{H}_2\text{O}$  molecules reside close to the calcite surface and their positions show little change at different time steps. However, the position of divalent ions is dynamic depending on the simulation time steps.  $\text{Ca}^{2+}$ , which is initially detected at 2.35 Å above the solid surface at  $T=300$  K and  $T=360$  K, migrates away by time. On the other hand,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  which are invisible up to  $t = 16$  ns even at the radius of 10 Å, move gradually toward the surface with time and consolidate their position after oil displacement. Namely, prior to oil displacement, a shift in  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{Ca}^{2+}$  locations is noticed, and the trend of double electric layer (EDL) is extended, which might be the cause of oil displacement. The findings of this study are applicable in the improvement of EOR technology, water resource treatment and contaminant transfer from geological systems, dealing with solid solutions such as ocean-soil systems.

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## 1. Introduction

Calcite, the most stable polymorph of calcium carbonate ( $\text{CaCO}_3$ ), is the mineral found in most geological systems. The behavior of calcite in the natural systems in contact with saline water is significantly dependent on the calcite surface chemistry. That is why extensive research studies have focused on the surface specifications of the calcite slab in an aqueous environment [1–4]. For instance, Fenter et al. [5] demonstrated that one or two monolayers of protonated hydroxyl groups are adsorbed onto the calcite surface depending on the pH value. They afterward measured the distance of the adsorbed monolayers from the calcite surface, which were 2.14 Å and 3.44 Å [6]. The saline water in contact with calcite may enforce new characteristics on the mineral surface. Due to this fact, some enhanced oil recovery (EOR) techniques are concerned with the properties of the calcite-saline water interface because water acts as a carrier to transport chemical agents to

the surface, and through this, it is possible to change the wettability and release oil.

Among the numerous EOR techniques, the low salinity water flooding (LSW) approach is inexpensive and additionally is suggested to be promising for both sandstones and carbonates reservoirs [7,8]. The LSW technique was first introduced by Bernard et al. [9] in 1967, who observed an increase in oil recovery when the concentration of NaCl brine remained within 0% to 1%. To this end, in the 1990s, a series of extensive experiments were carried out to assess Bernard's observations [10–12]. Lately, various mechanisms have been proposed to interpret the impact of the LSW, such as multi-component ion exchange (MIE) [13,14], osmotic pressure [15], fines migration [16], the extension of the electrical double layer [17], wettability alteration [18], etc.

Zhang et al. [19] investigated the wettability alteration in carbonate surface in contact with  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ . They reported that divalent anions show a more substantial effect on wettability alteration than their monovalent counterparts. On the other hand, Fathi et al. [20] reported a crucial role of  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ , and  $\text{SO}_4^{2-}$  in the

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wettability change of carbonates and represented about 10% improvement in oil recovery by eliminating the  $\text{Na}^+$  and  $\text{Cl}^-$  ions from seawater. Using experiment and modeling, Song et al. [21] pinpoint monovalent ions of LSW as the key factors of improved oil recovery in limestone reservoirs. In contrast, Zeng et al. [22] found that the absence of  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  had no influence on the adsorption of benzoic acid on the calcite surface. Moreover, Zhang et al. [23], within a series of long-term tests, declared that the oil recovery was greatly improved by fixing the  $\text{Ca}^{2+}$  and raising  $\text{SO}_4^{2-}$ . On the contrary, Karousi et al., by measuring the disjoining pressure for different systems, shows that the presence of  $\text{Mg}^{2+}$  ions in water containing  $\text{SO}_4^{2-}$  allows a more stable water film on the calcite surface. Yousef et al. [24] have studied the effect of water ions on the surface chemistry of carbonate reservoirs. Although they acknowledge that the driving mechanism of using LSW is dictated by wetting properties of the carbonate surface, they have declared that a comprehensive study is required to tune the ionic composition [25].

It seems the most complex element of the postulated EOR mechanisms is the link between macroscopic observations and molecular-scale mechanisms because the molecular features of the calcite-oil-brine interfaces remain a mystery. Although the role of the reactive ions such as  $\text{Na}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$  on calcite surface property change is inescapable [26,27], a deeper investigation of the calcite-oil-brine interactions is necessary to resolve the molecular scale ambiguities. In this regard, molecular dynamics (MD) simulations have emerged as a popular method to capture the underlying processes at the calcite-fluid interface at the nanoscale [28,29].

For instance, Kerisit and Parker used molecular dynamic simulation to represent the adsorbed water layer losing the hydrogen bond, causing density oscillation within the calcite-water interface [30]. Ahmadi G. et al. [31] studied the thermodynamic properties of the transition zone in the vicinity of the calcite-water interface with MD. According to this study, two fully ordered monolayers of water adsorb to the calcite surface, causing the density of the transition zone and bulk-like region to drop as the temperature rises. Using the MD results, they developed an equation of state inspired by Perturbation-Chain SAFT [32] to predict the thermodynamic properties of the confined interface at the calcite-water system. Zhao et al. [33] measured the contact angle between an n-decane nanodroplet and the surface of a calcite nanopore with classical MD simulation. Using numerous salinity concentrations, they demonstrated that the solid surface wettability is diminished after a certain concentration threshold. Koleini et al. [34] used MD to investigate the behavior of the brine water at the calcite-brine interface. They introduced two different brine water to the calcite surface, with total salinity of 46000 ppm and 189000 ppm. They believed that the divalent cation's contribution to EDL formation is reduced due to the high energy impact of the hydration shells encapsulating them. Although several studies investigated the role of the reactive ions such as  $\text{Na}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Cl}^-$  and  $\text{SO}_4^{2-}$  on oil displacement [26,27], there is still a lack of studies investigating the time dependency of ion distribution and charge density profile at the molecular scale.

There is growing evidence showing chemical interactions between crude oil and water in contact with the rock surface can considerably change the microscopic efficiency of the water flooding technique. In this study, we performed MD simulation to gain a better understanding of the molecular interactions between LSW and calcite solid surface within the thin brine film. A nanoscale version of calcite-oil-brine system is simulated with a calcite slab with neutral surface, high salinity brine (formation water), oil and LSW. The main objective is to track the changes in ion distribution and charge density over time.

## 2. Methodology

Two distinct simulation scenarios were defined, with each scenario executing the simulation at a specific temperature. In other words, the same composition as in scenario 1 with  $T=300$  K was examined at scenario 2 with  $T=360$  K. The following subsections summarize the utilized chemical components, physical geometry and detail of MD simulation.

### 2.1. Material

The rock surface is modeled by calcium carbonate in the form of a calcite slab. Formation water (FW), oil and LSW are inorganic and organic fluids interacting with the solid surface. Fig. 1 represents the initial configuration of the simulated system in the MD simulation box. As delineated, the calcite slab is regarded as a solid phase on the bottom side, while molecules of FW, oil and LSW on top of the calcite slab interact with each other and the solid surface. In this simulation approach, two different types of brine, namely FW (i.e.,  $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{Ca}^{2+}$ ) and LSW (i.e.,  $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ ) represent the high salinity and low salinity brine water adopted from Zhang and Sarma experimental study [35]. It is necessary to note that, FW and LSW, both are far from supersaturated conditions. The composition of oil was adjusted based on the SARA test including toluene (37%), decane (44.7%) and benzoic acid (18.3%). To be specific, the results of SARA test contains a mixture of saturated hydrocarbons, resins and aromatic compounds. Thus, toluene was chosen as an aromatic compound while decane and benzoic acid were selected as saturated hydrocarbon and resin, to mimic the oil model [36,37].

Table 1 summarizes the chemical composition of distinct components. It is worth noting that the number of elements in each scenario is calculated based on their density at a temperature of 300 K and pressure of 1 atm.

Table 2 shows the number of molecules utilized in MD simulation. To put it differently, Table 2 lists the number of molecules required to make the chemical compositions indicated in Table 1.

### 2.2. Geometry description

In this simulation, calcite with rhombohedral structure and cell parameters of  $a = b = 4.988$  Å,  $c = 17.061$  Å,  $\alpha = \beta = 90^\circ$ ,  $\gamma = 120^\circ$  [38] is representative of the mineral surface interacting with brine and

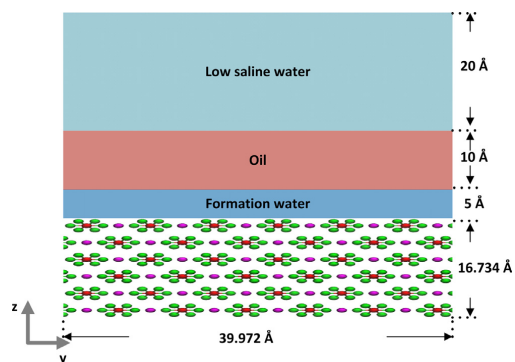


Fig. 1. The sketched geometry represents the schematic configuration of the system simulated with MD, which includes FW ( $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$ , and  $\text{Ca}^{2+}$ ), oil (toluene, decane, and benzoic acid) and LSW ( $\text{H}_2\text{O}$ ,  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$ , and  $\text{SO}_4^{2-}$ ) interacting with a calcite slab.

**Table 1**  
Composition for the brines [35] (FW and LSW) and oil phase, which are used in MD simulation.

Fluid									
Formation water <sup>2</sup>			Oil phase <sup>3</sup>			Low saline water <sup>1</sup>			
[ppm]			[weight%]			[ppm]			
Na <sup>+</sup>	Cl <sup>-</sup>	Ca <sup>2+</sup>	Toluene	Decane	Benzoic acid	Na <sup>+</sup>	Cl <sup>-</sup>	Mg <sup>2+</sup>	SO <sub>4</sub> <sup>2-</sup>
56,200	124,100	770	37	44.7	18.3	13,700	24,468	1620	3310

Notes: The density of low saline water, formation water and oil phase are as following:

(1)-Total density of Low saline water = 1.196 gr/cm<sup>3</sup>.

(2)-Total density of Formation water = 1.462 gr/cm<sup>3</sup>.

(3)-Total density of Oil phase = 0.938 gr/cm<sup>3</sup>.

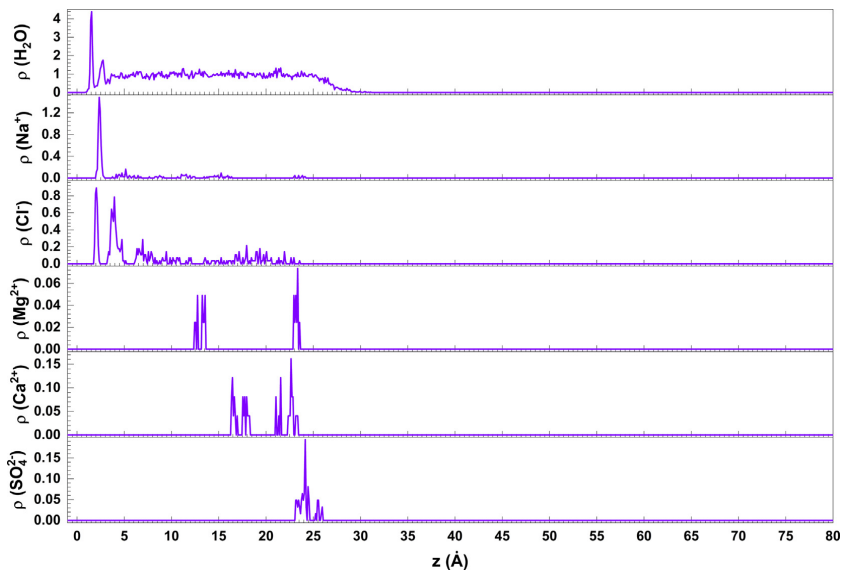
**Table 2**  
The number of molecules associated with each component at different, which are used in MD simulation.

Fluid												
Calcite slab	Formation water				Oil phase			Saline water				
[no. of molecules]	[no. of molecules]				[no. of molecules]			[no. of molecules]				
CaCO <sub>3</sub>	H <sub>2</sub> O	Na <sup>+</sup>	Cl <sup>-</sup>	Ca <sup>2+</sup>	Toluene	Decane	Benzoic acid	H <sub>2</sub> O	Na <sup>+</sup>	Cl <sup>-</sup>	Mg <sup>2+</sup>	SO <sub>4</sub> <sup>2-</sup>
12,000	276	18	26	4	38	29	14	1101	14	16	2	1

oil species. To this end, six atomic calcite layers were cleaved parallel along the plane (10 $\bar{1}$ 4)[39,40] to provide the 16.734 Å thickness along the z-axis, while the slab foundation with 41.183 Å × 39.972 Å lays on the xy-plane. A layer of FW including the 276 water molecules combined with mono/divalent inorganic ions mounted over the calcite slab using PACKMOL [41] to provide a thickness of 5 Å along the z-axis, as shown in Fig. 1. The next fluid phase is oil with a particular composition of organic compounds that adds 10 Å thickness to the top of FW. The LSW is placed on top of FW and oil, wherein 1101 water molecules are coupled with mono/divalent inorganic ions to create a 20 Å thickness above oil along the z-axis.

### 2.3. Details of MD simulation

All MD simulations in this work were conducted by Large Atomic/Molecular Massively Parallel Simulator [42] (LAMMPS). LAMMPS is an open-source MD code, which applies efficient parallel algorithms to simulate the thermodynamic ensembles in 2D and 3D, wherein the particles interact with various force fields. For two reasons, the calcite slab was treated as a rigid solid in this simulation. i) calcite slabs have a dynamic nature in reality that constantly reconfigure in response to their environment. ii) dissolution and chemical precipitation over calcite surface will alter the rock's morphology and thermodynamic equilibrium. For example,



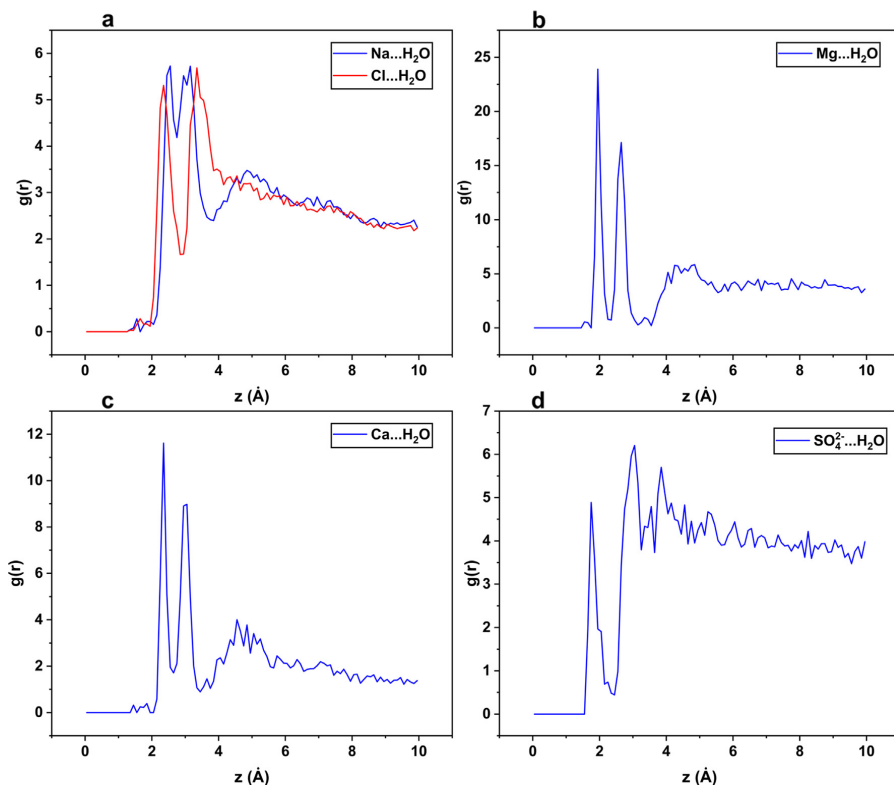
**Fig. 2.** The graph represents the mass density profile of H<sub>2</sub>O, Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup>, Ca<sup>2+</sup> and SO<sub>4</sub><sup>2-</sup> at T=300 K. The arrangement of Na<sup>+</sup> and Cl<sup>-</sup> layers above the calcite mineral is an appropriate testimony to the monovalent ion's tendency for binding to the calcite surface.

as brine salinity decreases, trapped organic molecules in the calcite crystal are expelled into the solution, which alters the history of the rocks. Therefore, by simulating a calcite slab as a rigid solid, we excluded the dynamics of the calcite surface restructuring in our study in order to avoid overly complicated simulation [43]. Here, the proposed force field by Xiao et al. [44] defines the interatomic potential between calcite particles. Parameters describing the force field are listed in [supplementary material](#). The three-sites rigid water model TIP3P [45] was employed to represent the force field between the water molecules. In order to model the interatomic potential of ions present in LSW and FW, two different protocols were utilized. Namely, the interatomic potential of  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{Ca}^{2+}$  were modeled using OPLS-AA [46] (Optimized Potentials for Liquid Simulations-All-Atom). Whereas the force field for  $\text{SO}_4^{2-}$  anion is determined by the potential developed by Williams et al. [47]. The geometric mixing rules were considered to calculate the cross-term interatomic potentials of different atoms. Additionally, OPLS-AA [46] force field controls the interatomic potential of oil components including decane, toluene and benzoic acid. The long-range electrostatic interactions were calculated by the particle-particle-mesh method [48] (PPPM) with a relative tolerance of  $10^{-6}$ . For determining all short-range potentials, on the other hand, a cut-off of 10 Å was applied. To prevent the molecule run away from the top of the simulation box, a

repulsive wall was embedded in the uppermost of the simulation box. The periodic boundary conditions were applied along the x and y-axes, while the boundary condition along the z-axis was considered fixed. The simulations were executed with the canonical ensemble (NVT) at  $T=300$  K and  $T=360$  K. In each simulation, the temperature was controlled using the Nose-Hoover [49] thermostat, which is one of the most accurate algorithms for modeling the NVT ensemble with classical MD simulations. The simulation run time for all scenarios are 45 ns, 5 ns for equilibration and 40 ns for production, with time step of 0.5 fs to achieve high resolution.

### 3. Results and discussion

The results of two defined scenarios, including low temperature ( $T=300$  K) and high temperature ( $T=360$  K), are analyzed and discussed in the following subsections. To begin, [Section 3.1](#) illustrates the formation of structured water layers on the uppermost layer of the calcite. Then, in [Sections 3.2](#), [3.3](#) and [3.4](#), we will explore the hydration of monovalent and divalent ions, as well as mass density and charge density profile. Finally, the evolution of ion distribution over time will be investigated and explained in [Section 3.5](#).



**Fig. 3.** At the last timestep of the simulation, the radial distribution function  $g(r)$  of mono/divalent ions with respect to the  $\text{H}_2\text{O}$  molecule at  $T=300$  K is plotted. The closest distances between  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$  and  $\text{SO}_4^{2-}$  and the first  $\text{H}_2\text{O}$  molecule are 2.45 Å, 2.35 Å, 1.95 Å, 2.35 Å and 1.75 Å, indicating that all of the existing mono/divalent ions are hydrated.



### 3.1. Calcite surface hydration

Fig. 2 depicts the density profile of different ions and water along the  $z$ -axis, the axis normal to the calcite surface. The density profile plotted in Fig. 2 helps evaluate the proclivity of various species to accumulate on a thin calcite-brine film. The depicted density profile explicitly demonstrates the adsorption of two water monolayers onto the calcite surface. In other words, the uppermost layer of calcite mineral is hydrated by a couple of highly structured water monolayers. Various ions density profiles immediately follow the structured water monolayers covering the calcite surface,

with much lower densities. The adsorption of water monolayers at the calcite mineral surface is consistent with de Leeuw and Parker's [50] observations. Fenter et al. [5] also reported hydration of the calcite surface when they used high-resolution X-ray to probe the calcite-water interface. Two structured layers of  $\text{Na}^+$  and  $\text{Cl}^-$  also are visible above the calcite mineral. As seen, the structured layer of  $\text{Na}^+$  is located within the fully ordered layers of adsorbed water. While the tight peak of  $\text{Cl}^-$  appeared after the fully ordered layers of adsorbed water. The arrangement of  $\text{Na}^+$  and  $\text{Cl}^-$  layers above the calcite mineral as a result of the energy penalty imposed by the ion solvation shell [51] is an appropriate testimony to the

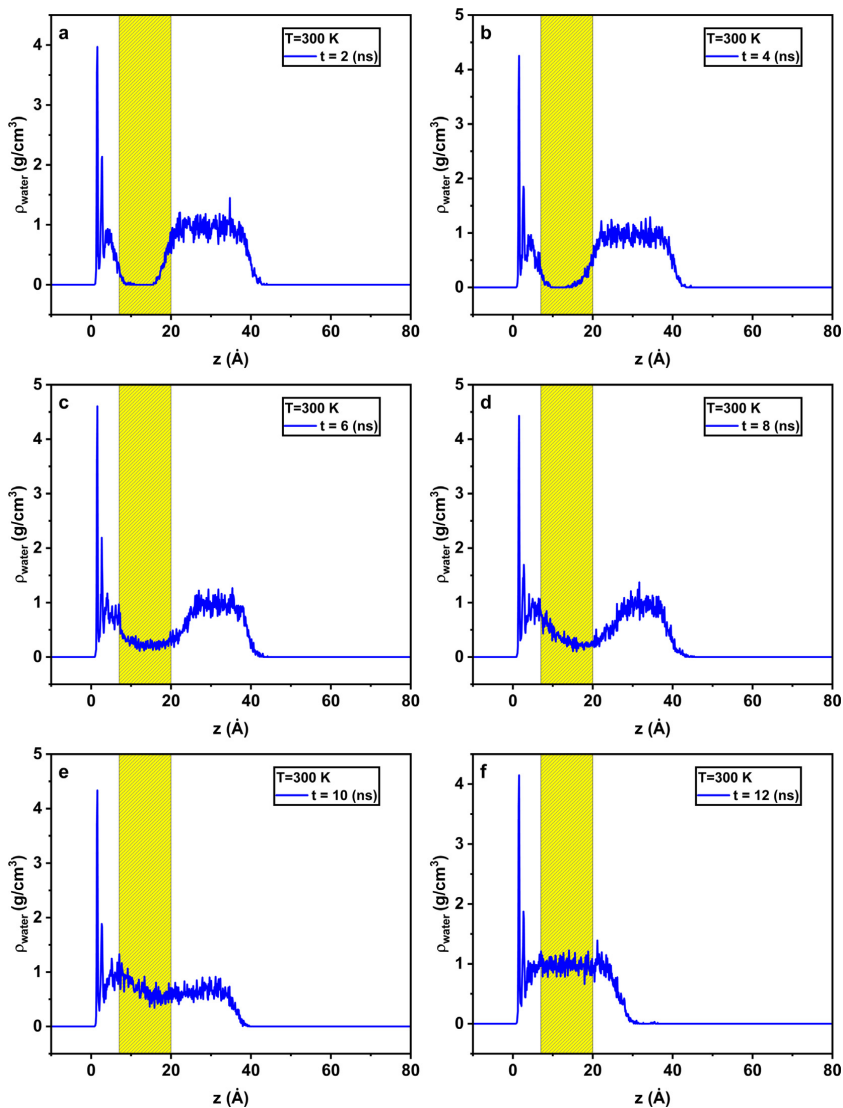


Fig. 4. Illustration of water density profile along the  $z$ -axis at  $T=300$  K at initial ( $t = 2$  ns and 4 ns), transition ( $t = 6$  ns, 8 ns and 10 ns) and completion stages ( $t = 12$  ns). The yellow shadow has highlighted the transition in the density profile.

ion's tendency for binding to the calcite surface. Furthermore, the appearance of the first monolayer of water at about 2 Å above the calcite surface indicates that neither  $\text{Na}^+$  nor  $\text{Cl}^-$  are directly adsorbed on the calcite surface. In other words, the first monolayer of water bridges between monovalent ions (herein,  $\text{Na}^+$  and  $\text{Cl}^-$ ) and calcite surface, as Koleini et al. [52] previously reported on this issue.

On the other hand, the divalent cations, i.e.,  $\text{Mg}^{2+}$  and  $\text{Ca}^{2+}$ , remain far from the calcite surface, presumably due to the higher energy penalty as reported by Chen et al. [53]. In addition,  $\text{SO}_4^{2-}$  stays far from calcite as divalent cations do. Section 3.5 will scrutinize the distribution of the divalent ions over time.

### 3.2. Hydration of ions

In the first and second scenarios, the hydration of the ions was initially explored. Specifically, the radial distribution function (rdf), also known as  $g(r)$ , was employed to calculate the distance between mono/divalent ions and molecules of water settled at a certain radius around the ions. Fig. 3 shows the radial distribution function for different ions at the last timestep and  $T=300$  K. As displayed, the adjacent  $\text{H}_2\text{O}$  molecules encircle  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$  and  $\text{SO}_4^{2-}$  at the radius of 2.45 Å, 2.35 Å, 1.95 Å, 2.35 Å and 1.75 Å, indicating that all of the existing mono/divalent ions are hydrated.

### 3.3. Evolution of water density profile over time

Figs. 4 and 5 show the water density profile at certain time-steps when  $T=300$  K and  $T=360$  K, respectively. The chosen snapshots in Figs. 4 and 5 demonstrate different stages in which the water density profile develops, including the initial, transition, and completion stages. In each plot box from left to right, a couple of structured water layers are observed near the solid surface, depicting the layering zone formed within the FW phase as reported in previous studies [54]. Following fully ordered water layers, a pit pattern in the water density profile represents the oil phase mounting above the FW. In fact, at the initial stage, the water density curve declines and experiences zero after some oscillation within FW. More precisely, within Fig. 4a-b and 5a-b, the position of the oil phase is distinguishable, where the curve touches zero and forms a pit-like appearance in the profile. On the right side of the plot box, the density profile rises again and LSW curve emerges on the tail of the water density profile.

As seen in Figs. 4c-d and 5c, a shift in water density profile commences, which is called transition hereafter. To be specific, when  $T=300$  K, the transition occurs in two steps ( $t = 8$  ns and  $t = 10$  ns) before reaching a complete density profile (completion stage) without a pit-like pattern, signifying the exit of the oil phase that was sandwiched between FW and LSW. Whereas, with  $T=360$  K, the transition of density profile is a one-step process, indi-

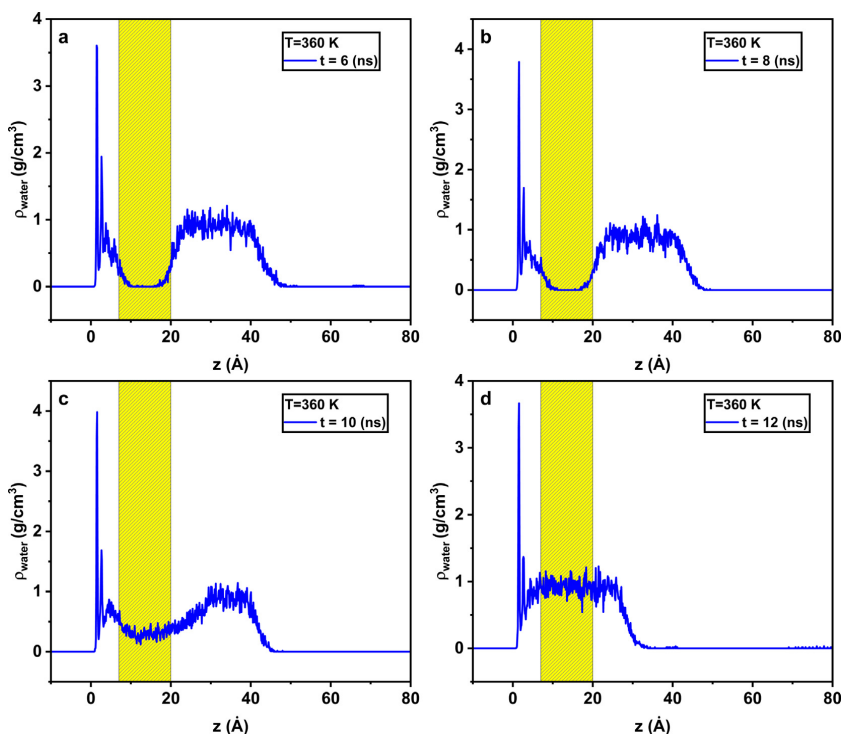
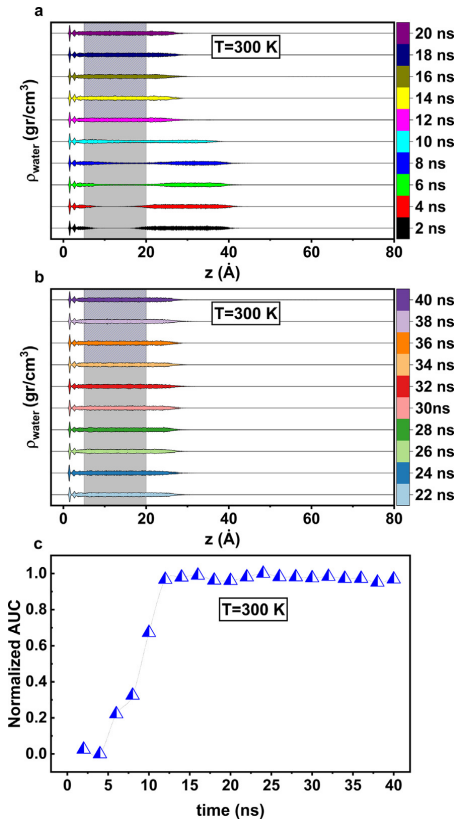


Fig. 5. Illustration of water density profile along the  $z$ -axis at  $T=360$  K at initial ( $t = 6$  ns and  $8$  ns), transition ( $t = 10$  ns) and completion stages ( $t = 12$  ns). The yellow shadow has highlighted the transition in the density profile.



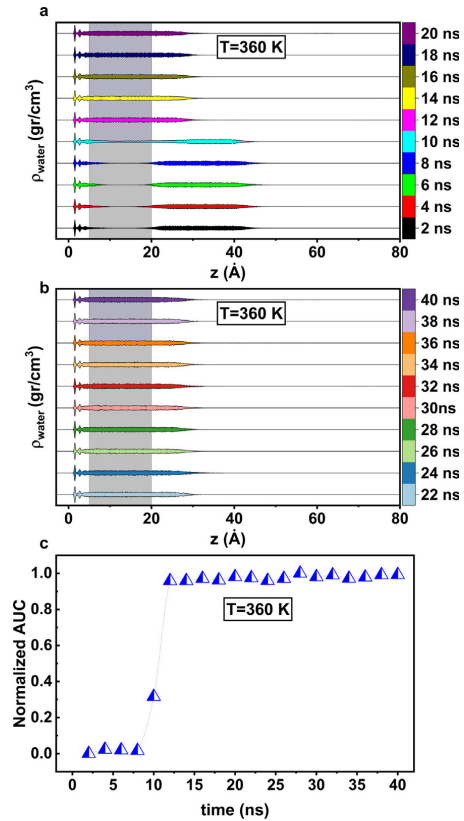
**Fig. 6.** Plots a-b show the evolution of the density profiles at T=300 K across different time steps. Plot c, depicts the behavior of the normalized area under the density curve (AUC), which is determined using the temporal evolution of the water density curve at T=300 K.

cating that the trapped oil phase has departed at  $t = 10$  ns. Finally, in Figs. 4f and 5d, where  $t = 12$  ns, the density profile of water is developed and no pit-like pattern is visible.

The evolution of the water density profile throughout all simulation time steps is demonstrated in Figs. 6 and 7. These figures provide a comprehensive view of the time evolution of the water density profile.

In Figs. 6 and 7, each density profile is merged with its vertical mirrored trend to indicate the intersection with the z-axis and take off from zero, marking the initial, transition and completion stages. The distinct colors assigned to each curve serve as a reference point to indicate the state of evolution at a certain time step.

As seen in Fig. 6a, before  $t = 8$  ns, the coexistence of FW, oil and LSW is apparent, addressing the initial stage. From  $t = 6$  ns to  $t = 12$  ns, the oil phase is displaced gradually within the transition stage, which results in the extension of the colored region. Beyond the  $t = 12$  ns, the colored regions in Fig. 6a-b remain almost unchanged, representing the completion stage. To precisely capture the boundaries of the different stages, the normalized area under the density curve (AUC) is calculated using a numerical integral product. Its evolution is then plotted over time in Fig. 6c. Using



**Fig. 7.** Plots a-b show the evolution of the density profiles at T=360 K across different time steps. Plot c, depicts the behavior of the normalized area under the density curve (AUC), which is determined using the temporal evolution of the water density curve at T=360 K.

AUC, one can easily trace the transition steps at T=300 K, which are  $t = 6$  ns,  $t = 8$  ns and  $t = 10$  ns.

On the other hand, when T=360 K, a distinction between FW, oil and LSW is traceable till  $t = 10$  ns in Fig. 7a. After the initial stage, the oil phase translates within  $t = 8-12$  ns and since then, the colored regions become stable in Fig. 7a-b, implying the completion stage. By following the profile of the AUC in Fig. 7c, one realizes that at T=360 K, the transition occurs at one step, i.e.,  $t = 10$  ns. A comparison of Fig. 6c and Fig. 7c reveals that at T=300 K, the breakthrough in normalized AUC occurs in three steps ( $t = 6$  ns,  $8$  ns, and  $10$  ns), whereas at T=360 K, the breakthrough appears at  $t = 10$  ns. Although both density profiles at T=300 K and T=360 K possess a stable profile after  $t = 12$  ns, the transition state at T=300 K occurs earlier than at T=360 K. Furthermore, at T=360 K, the transition stage, which coincides with oil displacement, is performed within one step.

To sum up, a one-stage transition at T=360 K implies a quick shift when compared to a three-stage transition at T=300 K. Namely, the transition at T=360 K begins with a delay and lasts for a shorter time. The observed breakthrough in Fig. 6c and Fig. 7c reveals microscopic changes in the organic and inorganic fluids interacting with the calcite surface.

### 3.4. Evolution of charge density profile over time

The local charge density is defined as a difference between the number of positive and negative charges. Thus, the charge density trend can indicate which charge is present and how it is distributed throughout the calcite surface.

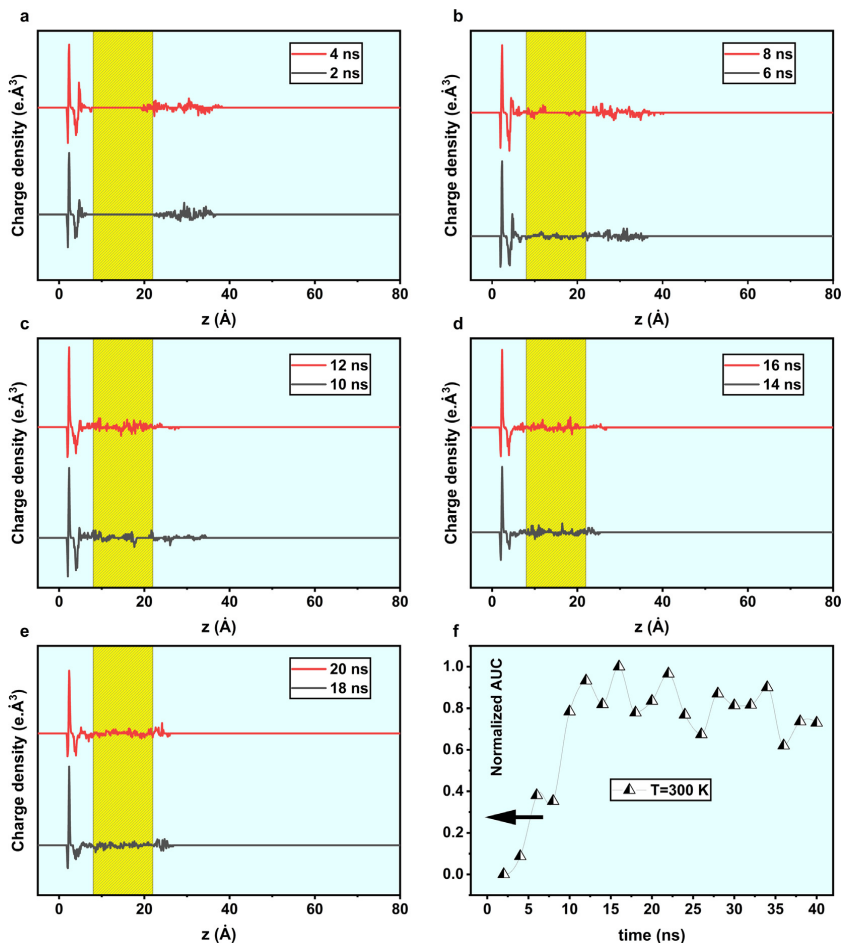
To better understand the ionic environment in the vicinity of calcite substrate the contribution of all types of ions based on the charge density are plotted in Figs. 8 and 9, displaying the charge density development with time at  $T=300$  K and  $T=360$  K.

It was mentioned that monovalent ions ( $\text{Na}^+$  and  $\text{Cl}^-$  in Fig. 2) have a higher affinity for calcite surface than divalent ones. Because, the monovalent ions diffuse into the structured water layers and divalent ones stay far from the calcite surface [55]. Figs. 8-9 demonstrate how the presence of structured ion layers in vicinity of calcite substrate leads to the formation of EDL which is compatible with the double layer theory of Gouy-Chapman [56].

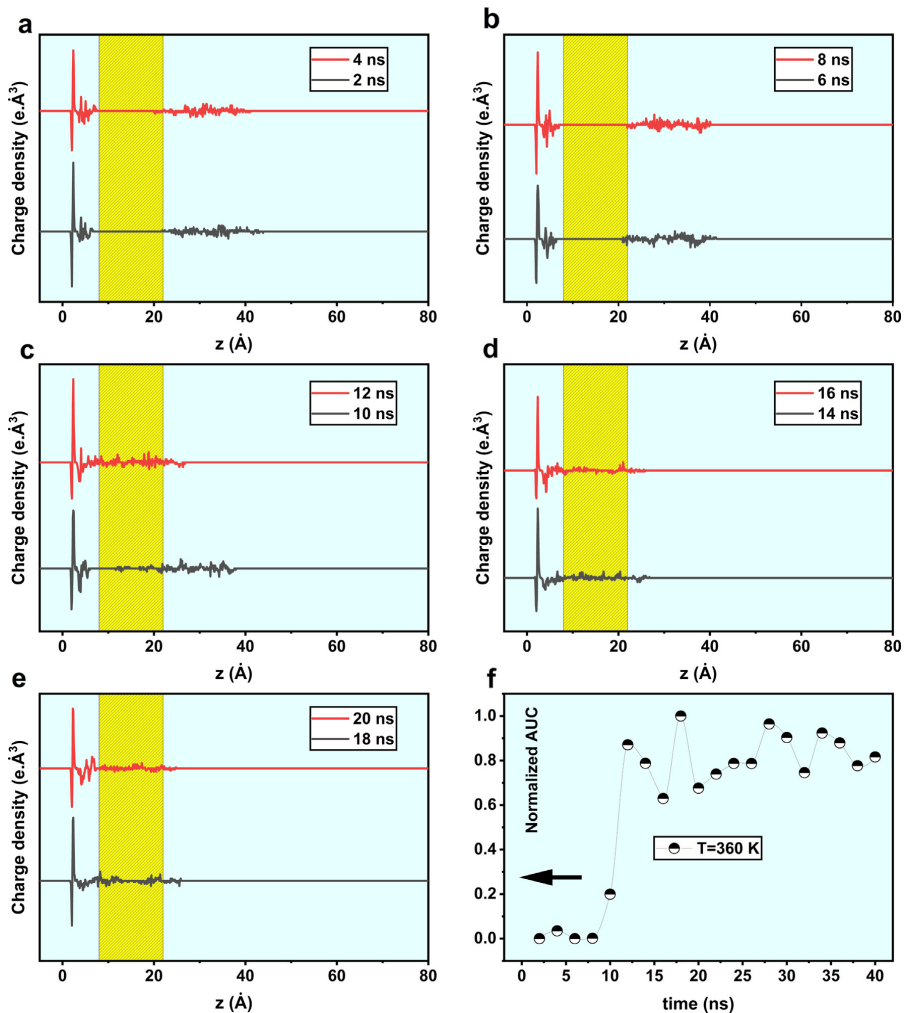
The EDL is made of stern layer with positive charge ( $\text{Na}^+$ ) and diffuse layer with negative charge ( $\text{Cl}^-$ ). This arrangement is in agreement with Koleini et al. [43] observation. As they reported in a different study used a neutral substrate of calcite and found that the protrude oxygen atoms of neutral calcite surface interact with  $\text{Na}^+$  and develop the EDL [36].

In Fig. 8a-b and Fig. 9a-b, the charge density curve oscillates initially, then experiences zero along with the oil phase, and finally oscillates again where the LSW exists. According to Fig. 8, which presents charge density at  $T=300$  K, a discontinuity is noticed between the oscillations at left and right at  $t = 2$  ns and 4 ns, indicating no charge has been distributed. The observed gap began to build up at  $t = 6$  ns, continued at  $t = 8$  ns, 10 ns, then completed at  $t = 12$  ns so that no gap is noticed in charge density within  $t = 14$ –20 ns.

On the other hand, the charge density behaves differently in terms of extension with time at  $T=360$  K. As seen, in Fig. 9a-b, a discontinuity similar to what is presented at  $T=300$  K sepa-



**Fig. 8.** At  $T=300$  K and several time steps, the charge density profile above the calcite surface is depicted within plots a-f. The oscillations near the solid surface show the double electrical layer (EDL) curve, which experiences zero across the oil phase until  $t = 8$  ns. The observed gap in charge density oscillations starts bridging at  $t = 10$  ns, which is accompanied by escaping the oil phase and merging FW with LSW.



**Fig. 9.** At  $T=360$  K and several time steps, the charge density profile above the calcite surface is depicted within plots a–f. The oscillations near the solid surface show the double electrical layer (EDL) curve, which experiences zero across the oil phase until  $t = 8$  ns. The observed gap in charge density oscillations starts bridging at  $t = 10$  ns, which is accompanied by escaping the oil phase and merging FW with LSW.

rates the charge density profile into two parts until  $t = 8$  ns, meaning that the oil phase resided between the FW and LSW phase.

When the simulation time step reaches 10 ns at  $T=360$  K, the gap in the charge density profile starts filling up. By integrating the area under the charge density curve (AUC) and normalizing, one may follow the change of the charge density evolution at each time step such as what is presented in Figs. 8f and 9f. The patterns represented in Fig. 8f and Fig. 9f track the charge density evolution with respect to the simulation time step at  $T=300$  K and  $T=360$  K, respectively. As seen, at  $T=300$  K, the charge density development starts earlier than  $T=360$  K. In contrast, the transition state at  $T=360$  K occurs quicker than the transition state at  $T=300$  K. There are several similarities between Figs. 6–7 and Figs. 8–9. In other

words, the charge density and water density not only evolve in the same timestep but also behave similarly over time. Therefore, oil detachment from calcite-brine interface occurs concurrently with bridging the observed gap in charge density which is consistent with Alotaibi [57] and Mahani [58] findings.

### 3.5. Distribution of the mono/divalent ions

The charge density trend is the result of the local distribution of various anions and cations. Each anion and cation depends on the inherent charge and hydration energy has a unique interaction with the calcite surface. In this section, the distribution of the mono/divalent ions will be investigated as a function of the simulation time step to study the repositioning of the ions before and

after oil detachment from calcite-rock interface. The mass density and charge density profile in previous sections showed that the transition stage at  $T=300$  K and  $T=360$  K happens at different time-steps i.e.,  $t = 4$  ns and  $t = 8$  ns, respectively. Hence, any displacement of mono/divalent ions before  $t = 4$  ns and  $t = 8$  ns could be related to a potential cause for oil displacement. To this end, Figs. 10 and 11 were plotted to track the position of various ions along

the z-axis. The blue vertical axis at the left side of each plot box displays z-axis. While the red vertical axis at the right side presents normalized AUC. As shown in Figs. 10a-b and 11a-b, the position of  $\text{Na}^+$  and  $\text{Cl}^-$  stabilizes at around 2.35 Å and 2.85 Å and temperature have no severe effect on the repositioning of  $\text{Na}^+$  and  $\text{Cl}^-$ . Regarding time dependency of ions position,  $\text{Na}^+$  settles at a fixed position before  $t = 4$  ns and have no intention to translate by temperature.

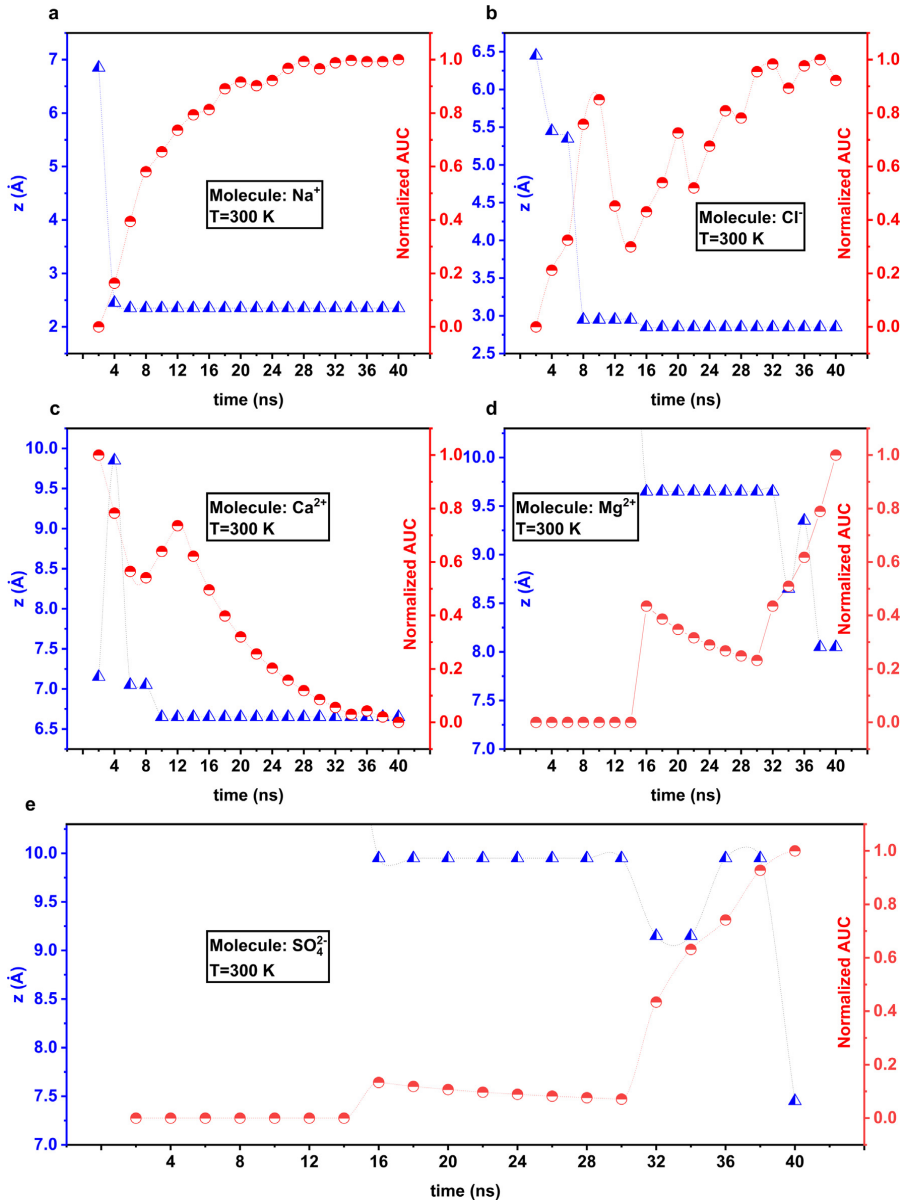
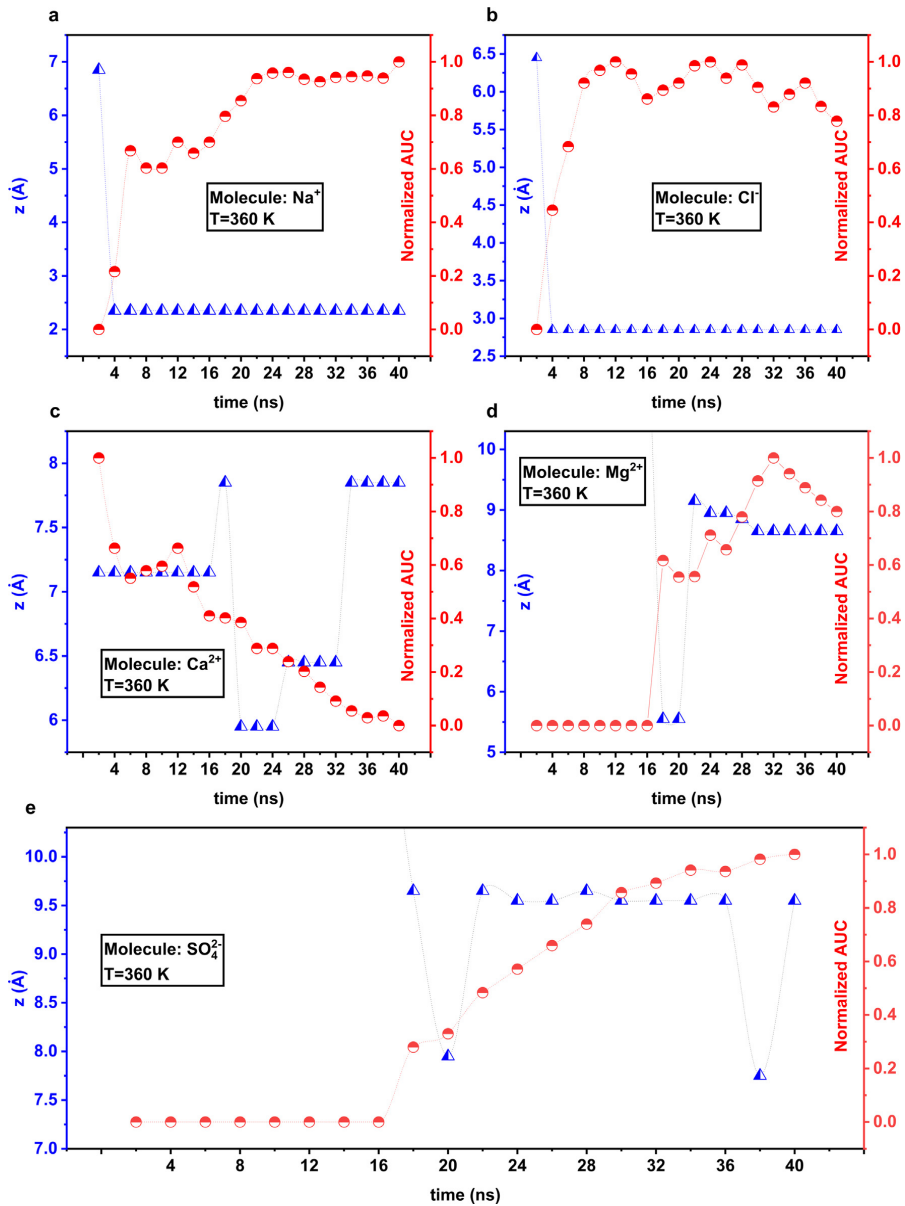


Fig. 10. The graphs illustrate the normalized AUC of  $g(r)$  at the right vertical axis and distance from the solid surface at the left vertical axis with respect to the time at  $T=300$  K.



**Fig. 11.** The graphs illustrate the normalized AUC of  $g(r)$  at the right vertical axis and distance from the solid surface at the left vertical axis with respect to the time at  $T=360$  K.

At the same time,  $\text{Cl}^-$  behaves similarly to  $\text{Na}^+$  at  $T=360$  K. Nevertheless, when  $T=300$  K the position of  $\text{Cl}^-$  stabilizes a bit later at  $t = 8$  ns. A previous study by Liu et al. [59] found that the monovalent ions ( $\text{Na}^+$  and  $\text{Cl}^-$ ) settle on the calcite surface, disturbing the structured water layers. In terms of monovalent ions, our observation is consistent with them.

Figs. 10c and 11c have recorded the position and distribution probability of divalent cation  $\text{Ca}^{2+}$ . Although, at  $T=300$  K, the blue curve lands on a fixed position after  $t = 8$  ns and it oscillates between different positions at  $T=360$  K. Nevertheless, the distribution probability of  $\text{Ca}^{2+}$  at high and low temperature decreases with time, as depicted with the red curve.

On the other hand, no severe change in the distribution probability of  $\text{SO}_4^{2-}$  and  $\text{Mg}^{2+}$  is noticed before  $t = 16$  ns, as displayed in Figs. 10d-e and 11d-e. In other words, because the red curve intersects zero, the blue curve ascends (beyond the axis scale) prior to  $t = 16$  ns, meaning that no  $\text{SO}_4^{2-}$  and  $\text{Mg}^{2+}$  ions were detected at a radius of 10 Å. By 10 Å, we mean the cut-off radius for  $g(r)$  function. Thus, any value greater than 10 Å will go to infinity, as shown in Figs. 10d-e and 11d-e. Although, the divalent ions i.e.,  $\text{SO}_4^{2-}$  and  $\text{Mg}^{2+}$  move toward the solid surface after  $t = 16$  ns and the relevant distribution probability increases simultaneously. However, in Sections 3.2 and 3.3, it was denoted that the oil detachment takes place much earlier than  $t = 16$  ns. This finding verifies the results reported by Alotaibi [57], Mahani [58] and Mehana [60] who found that divalent ions (i.e.,  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ ) had a minor impact compared to the critical role of EDL in oil detachment from calcite-brine interface.

#### 4. Conclusion

We utilized LAMMPS to conduct molecular dynamics simulations to explore the interaction of low salinity brine with a calcite mineral in a molecular scale. To mimic the rock-brine-oil system, the neutral surface of calcite is chosen as a rock surface, the oil is modeled with decane (hydrocarbon), toluene (aromatic) and benzoic acid (polar) and the low/high saline brines were simulated with different mixtures of  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$ , and  $\text{SO}_4^{2-}$ . For this simulation, two different scenarios were established so that each simulation scenario was completed within the 45 ns at a specific temperature, i.e.,  $T=300$  K and  $T=360$  K. The results show that:

- All of the mono/divalent ions were hydrated by  $\text{H}_2\text{O}$  molecules.
- The  $\text{H}_2\text{O}$  molecules are adsorbed onto the calcite surface as structured layers.
- Following the  $\text{H}_2\text{O}$  molecules, the monovalent ions  $\text{Na}^+$  and  $\text{Cl}^-$  settle adjacent to the calcite surface until the last timestep of simulation.
- The ordered layering of monovalent ions  $\text{Na}^+$  and  $\text{Cl}^-$  form an EDL at calcite-brine interface.
- The detachment of oil from calcite-brine interface occurs concurrently with extension in charge density.
- The position of  $\text{Ca}^{2+}$  ions at  $T=300$  K is more stable than at  $T=360$  K.
- Up to 16 ns the divalent ions  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  were not traceable within the 10 Å above the surface along the z-axis.  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  ions travel toward the calcite mineral surface after 16 ns and remain within 10 Å distance from surface.
- According to the results, the temperature change approximately didn't affect the position of  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{H}_2\text{O}$  molecules. Whereas, the location of the  $\text{Ca}^{2+}$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  ions varies as a function of temperature, indicating a dynamic behavior with the temperature change.

#### CRedit authorship contribution statement

**S. Ahmadi G.:** Conceptualization, Methodology, Software, Validation, Writing – original draft, Visualization, Formal analysis, Investigation, Writing – review & editing. **S. Abdolahi:** Software, Validation, Investigation. **J. Jähren:** Supervision. **R. Miri:** Supervision, Writing – review & editing. **H. Hellevang:** Supervision, Writing – review & editing.

#### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Appendix A. Supplementary material

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.molliq.2022.119490>.

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Supplementary material for

## Drivers of Low Salinity Effect in Carbonate Reservoirs Using Molecular Dynamic Simulation

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The nonbonding interaction between atoms is described by a Lennard-Jones 12–6 expression plus columbic term:

$$U(r_{ij}) = 4\varepsilon_{ij} \left[ \left( \frac{\sigma_{ij}}{r_{ij}} \right)^{12} - \left( \frac{\sigma_{ij}}{r_{ij}} \right)^6 \right] + \frac{1}{4\pi\varepsilon_0} \left( \frac{q_i q_j}{r_{ij}} \right)$$

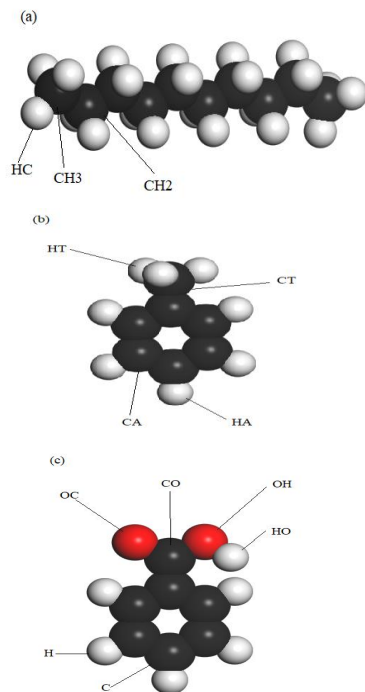
The bond stretching, angle bending, dihedral torsion and improper are represented, respectively, by:

$$U_b = k_b(r - r_0)^2$$

$$U_\theta = k_\theta(\theta - \theta_0)^2$$

$$U_{dihedral} = \frac{1}{2}k_1(1 + \cos(\varphi)) + \frac{1}{2}k_2(1 + \cos(2\varphi)) + \frac{1}{2}k_3(1 + \cos(3\varphi)) + \frac{1}{2}k_4(1 + \cos(4\varphi))$$

$$U_{improper} = K(\chi - \chi_0)$$



**Figure S1.** Molecular structure of (a) Decane, (b) Toluene, (c) Benzoic acid and definition of atom types

**Table S1.** Mass, charge, and Lennard-Jones parameters for water, Decane, Toluene, Benzoic acid, ions, and calcite

Symbols	Mass [g/mol]	Charge [ <i>e</i> ]	$\epsilon_{ii}$ [kcal/mol]	$\sigma_{ii}$ [Å]
Water (TIP3P[1])				
Ow	15.9994	-0.83	0.102	3.188
Hw	1.008	+0.415	0.0	0.0
Decane (OPLS-AA[2])				
CH3	12.0107	-0.18	0.066	3.55
CH2	12.0107	-0.12	0.066	3.55
HC	1.00784	+0.06	0.03	2.5
Toluene (OPLS-AA[2])				
HT	1.00784	+0.06	0.03	2.5
CT	12.0107	-0.065	0.066	3.5
CA	12.0107	-0.115	0.07	3.55
HA	1.00784	+0.115	0.03	2.42
Benzoic Acid (OPLS-AA[2])				
C	12.0107	-0.115	0.07	3.55
H	1.00784	+0.115	0.03	2.42
OC	15.999	-0.44	0.21	2.96
CO	12.0107	+0.635	0.105	3.75
OH	15.999	-0.53	0.17	3
HO	1.00784	+0.45	0.0	0.0
Ions (OPLS-AA[2] and Williams et al.[3])				

Na	23.0	+1.0	0.0005	4.07
Cl	35.453	-1.0	0.71	4.02
Mg	24.305	+2.0	0.875044	1.6444471
S	32.065	+2.3	0.1999	3.55
Os	15.999	-1.075	0.15525	3.25
Ca	40.0780	+2.0	0.449657	2.412031
Calcite (Xiao et al.[4])				
C <sub>calcite</sub>	12.0107	+0.999	0.088131	3.8233
Ca <sub>calcite</sub>	40.0780	+1.668	0.477866	2.3705
O <sub>calcite</sub>	15.9994	-0.889	0.13902	3.09086

The interatomic LJ parameters for calcite and water is represented in table S.2, while the geometric mixing rules were considered to calculate the cross-term interatomic potentials of other atoms.

$$\varepsilon_{ij} = \sqrt{\varepsilon_i \varepsilon_j}$$

$$\sigma_{ij} = \sqrt{\sigma_i \sigma_j}$$

**Table S2.** Interatomic LJ parameters for Calcite and water

Atom Type	Atom Type	$\varepsilon_{ij}$ [kcal/mol]	$\sigma_{ij}$ [Å]
Calcite-Calcite			
C <sub>calcite</sub>	O <sub>calcite</sub>	6.27	1.197
O <sub>calcite</sub>	O <sub>calcite</sub>	0.000273	4.744
Calcite-Water			
Ca	O <sub>w</sub>	0.269896	2.76

C	Ow	0.116079	3.46
O	Ow	0.14603	3.118
O	Hw	0.000006968	4.497

**Table S3.** Bonded stretch, angle bend and dihedral parameters for water, calcite and sulfate ion

Bond stretch	Bond type	$k_b$ [kcal/(mol·Å <sup>2</sup> )]	$r_0$ [Å]
	C <sub>calcite</sub> -O <sub>calcite</sub>	314.5	1.294
	Hw-Ow	450.0	0.9572
	S-Os	525.15	1.487
Angle bend	Angle type	$k_\theta$ [kcal/(mol·deg <sup>2</sup> )]	$\theta_0$ [deg]
	Hw-Ow-Hw	55.0	104.52
	O <sub>calcite</sub> -C <sub>calcite</sub> -O <sub>calcite</sub>	221.3	120.0
	Os-S-Os	139.906	109.47

**Table S4.** Bonded stretch, angle bend and dihedral parameters for Decane

Bond stretch	Bond type	$k_b$ [kcal/(mol·Å <sup>2</sup> )]	$r_0$ [Å]
	CH3-CH2	268	1.529
	CH2-CH2	268	1.529

	CH3-HC	340	1.09		
	CH2-HC	340	1.09		
Angle bend	Angle type	$k_\theta$ [kcal/(mol·deg <sup>2</sup> )]	$\theta_0$ [deg]		
	CH3-CH2-CH2	58.35	112.7		
	CH2-CH2-CH3	58.35	112.7		
	CH2-CH2-CH2	58.35	112.7		
	HC-CH3-HC	33	107.8		
	HC-CH2-HC	33	107.8		
Dihedrals	Dihedral type	$k_1$ [kcal/mol]	$k_2$ [kcal/mol]	$k_3$ [kcal/mol]	$k_4$ [kcal/mol]
	CH3-CH2-CH2-CH2	1.3	-0.05	0.2	0.0
	CH2-CH2-CH2-CH3	1.3	-0.05	0.2	0.0
	CH2-CH2-CH2-CH2	1.3	-0.05	0.2	0.0
	CH3-CH2-CH2-HC	0.0	0.0	0.3	0.0
	CH2-CH2-CH3-HC	0.0	0.0	0.3	0.0
	CH2-CH2-CH2-HC	0.0	0.0	0.3	0.0
	HC-CH3-CH2-HC	0.0	0.0	0.3	0.0
	HC-CH2-CH3-HC	0.0	0.0	0.3	0.0
	HC-CH2-CH2-HC	0.0	0.0	0.3	0.0

**Table S5.** Bonded stretch, angle bend, dihedral and improper parameters for Toluene

Bond stretch	Bond type	$k_b$ [kcal/(mol·Å <sup>2</sup> )]		$r_0$ [Å]	
	CT-HT	340.0		1.09	
	CA-CT	317.0		1.51	
	CA-CA	469.0		1.4	
	CA-HA	367.0		1.08	
Angle bend	Angle type	$k_\theta$ [kcal/(mol·deg <sup>2</sup> )]		$\theta_0$ [deg]	
	HT-CT-HT	33.0		107.8	
	CA-CT-HT	35.0		109.5	
	CA-CA-CA	63.0		120.0	
	CA-CA-CT	70.0		120.0	
	CA-CA-HA	35.0		120.0	
Dihedrals	Dihedral type	$k_1$ [kcal/mol]	$k_2$ [kcal/mol]	$k_3$ [kcal/mol]	$k_4$ [kcal/mol]
	CA-CA-CT-HT	0.0	0.0	0.0	0.0
	CA-CA-CA-CT	0.0	7.25	0.0	0.0
	CT-CA-CA-HA	0.0	7.25	0.0	0.0
	CA-CA-CA-CA	0.0	7.25	0.0	0.0
	CA-CA-CA-HA	0.0	7.25	0.0	0.0
	HA-CA-CA-HA	0.0	7.25	0.0	0.0
Impropers	Improper type	K [kcal/mol]		$\chi_0$ [deg]	
	CA-CA-CA-HA	2.5		180.0	



	CA-HA-CA-CA	2.5	180.0
	CA-CA-CA-CT	2.5	180.0
	CA-CT-CA-CA	2.5	180.0

**Table S6.** Bonded stretch, angle bend, dihedral and improper parameters for Benzoic acid

Bond stretch	Bond type	$k_b$ [kcal/(mol·Å <sup>2</sup> )]		$r_0$ [Å]	
	OC-CO	570.0		1.229	
	CO-OH	450.0		1.364	
	C-CO	400.0		1.49	
	OH-HO	553.0		0.945	
	C-C	469.0		1.4	
	C-H	367.0		1.08	
Angle bend	Angle type	$k_\theta$ [kcal/(mol·deg <sup>2</sup> )]		$\theta_0$ [deg]	
	OH-CO-OC	80.0		121.0	
	OH-CO-C	70.0		120.0	
	OC-CO-C	80.0		120.4	
	CO-OH-HO	35.0		113	
	C-C-C	63.0		120.0	
	CO-C-C	85.0		120.0	
C-C-H	35.0		120.0		
Dihedrals	Dihedral type	$k_1$ [kcal/mol]	$k_2$ [kcal/mol]	$k_3$ [kcal/mol]	$k_4$ [kcal/mol]

	OC-CO-OH-HO	0.0	5.0	0.0	0.0
	C-CO-OH-HO	4.0	5.0	0.0	0.0
	OC-CO-C-C	0.0	2.1	0.0	0.0
	OH-CO-C-C	0.0	2.1	0.0	0.0
	CO-C-C-C	0.0	7.25	0.0	0.0
	CO-C-C-H	0.0	7.25	0.0	0.0
	C-C-C-C	0.0	7.25	0.0	0.0
	C-C-C-H	0.0	7.25	0.0	0.0
	H-C-C-H	0.0	7.25	0.0	0.0
Improper	Improper type	K [kcal/mol]		$\chi^0$ [deg]	
	OH-C-CO-OC	10.5		180.0	
	OC-OH-CO-C	10.5		180.0	
	CO-C-C-C	2.5		180.0	
	C-C-C-H	2.5		180.0	
	C-H-C-C	2.5		180.0	
	C-CO-C-C	2.5		180.0	

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# Appendices



## Appendix A

# InterPore 13th Annual Meeting, 31 May - 4 June 2021

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On the fluid-rock interface, the order of the molecular structure and dynamical properties of fluid deviates from that of the bulk phase and the fluid exhibits a different thermodynamic behavior. To develop an understanding of the fluid-rock interface molecular dynamic (MD) simulation is conducted for water-calcite system. In this study, the results of MD simulations explicitly exhibit the layering transition of water on water-calcite interface. To predict the water properties near calcite wall, we have defined a contribution for Helmholtz energy extended from SAFT equation of state (EOS). In this approach, the confined water molecules interact with calcite surface through a square well energy  $\varepsilon$  estimated by MD simulation at a certain temperature (T). The outcomes of MD simulations confirm the fluctuation of energy, within the confinement, corresponds to the the calcite electrostatic field on the bulk water. The modified SAFT shows a good agreement with MD observations and the introduced model can predict the thermodynamic properties of water at systems with low water content.





Appendix B

# **83rd EAGE Annual Conference & Exhibition**



## Mineral-Fluid Interface Properties: A Molecular Dynamic Study

### Introduction

Along with the mineral-fluid interfaces, a transition zone exists wherein the fluid exhibits different thermodynamic properties from the bulk phase. The interfacial properties of mineral-fluid interfaces are the consequences of mineral and fluid mutual interaction. Evaluating the properties of the fluid confined within the mineral-fluid interface is of interest to a variety of research fields such as bio (Walsh and Knecht, 2017), energy (Zhu et al., 2018), surface chemistry (Wang et al., 2018) and geology (Mishra et al., 2014). In order to accurately estimate the confined fluid properties, it is essential to develop our understanding of underlying mechanisms of interaction between a solid mineral and fluid.

There is a scarcity of experimental data on interfacial properties, thus modeling approaches can play an essential role in capturing the thermodynamic properties at the interface. The Monte Carlo (MC) algorithm is one option for gaining insights into confined fluid properties (Jin et al., 2017). In this regard, Li et al. (Li et al., 2005) have investigated capillary condensation and evaporation of the confined phase in slit-like pores with MC simulations. They reported that the phase transfer under pore confinement occurs at a pressure lower than bulk pressure. Zhang et al. (Zhang and Wang, 2006) investigated the fluid-solid interaction on the critical point change by applying the discrete wall potential model. They found the critical point increases for weak fluid-solid interactions and decreases for strong interface interactions. Barbosa et al. (Barbosa et al., 2016) modified the Travalloni (Travalloni et al., 2014) model by evaluating the effect of different confinement degrees on the fluid structure. However, the samples in MC method do not need to follow a physical process because of the ergodic generation process. Hence, additional alternatives, such as molecular dynamic (MD), come into consideration. Using MD, one can simulate the mineral-fluid interfaces using a known molecular interaction so-called force field. Unlike MC, MD simulation does not lose information about the actual physical process. In other words, not only can one gain information about the equilibrium state in MD, but one can also pursue the physical path reaching equilibrium. This simulation approach has demonstrated its potential as a viable tool for exploring the interfacial effects in systems with solid-fluid interactions (Sedghi and Piri, 2018). The use of MD simulation to study the mineral-fluid interface has received considerable attention in the literature (Adapa et al., 2018). For instance, Zhang et al. (Zhang et al., 2021) have studied the transport of two phase flow inside a calcite nanopore with MD. They observed the formation of the water bridge in the center of the nanopore when the water/oil proportion was high. Kirch et al. (Kirch et al., 2018) investigated the interface of calcite and brin water (including  $\text{Na}^+$ ,  $\text{Cl}^-$  and  $\text{Ca}^{2+}$  ions) with MD simulation. The observed epitaxial ordering of water molecules on the surface of calcite precludes the direct adsorption of various chemical species.

### Theory

In this study, calcite is chosen as the mineral which is one of the most abundant minerals in nature with rhombohedral structure,  $R\bar{3}c$  space group, and unit cell parameters of  $a=b=4.988 \text{ \AA}$ ,  $c=17.061 \text{ \AA}$ ;  $\alpha=\beta=90^\circ$ ,  $\gamma=120^\circ$  (Markgraf and Reeder, 1985). The calcite layers were cleaved along the  $(10\bar{1}4)$  surface. Then, water molecules were mounted above the calcite slab with PACKMOL (Martinez et al., 2009) software. Figure 1 shows the configuration of calcite-water in the simulation box. Water was provided in three different lengths, i.e.,  $L_z=2.5 \text{ nm}$ ,  $4 \text{ nm}$  and  $7 \text{ nm}$ . The boundary condition along x and y-axes is periodic, while along the z-axis, the boundary condition is fixed. The open source LAMMPS (Plimpton, 1995) software is used to conduct the MD simulations. The Nose-Hoover (Nosé, 1984) thermostat is applied to implement a canonical ensemble at  $T=300 \text{ K}$ ,  $400 \text{ K}$  and  $500 \text{ K}$ . Zhao (Zhao et al., 2019) and SPC/E (Berendsen et al., 1987) are two different force fields that were applied in this simulation. The former describes the interaction of calcite species, whereas the latter models the interactions of water molecules. Each simulation run took 2 ns to complete, including 1 ns for equilibration and 3 ns for production.

### Results and discussion

Figure 2 displays the water density profile along the z-axis. Figure 2a depicts the density profile for  $L_z=2.5 \text{ nm}$ , whereas 2b and 2c exhibit the density trends for  $L_z=4 \text{ nm}$  and  $L_z=7 \text{ nm}$ , respectively. Based

on the density profile behavior, three distinct zones (depicted in Figure 1) could be identified. The layering zone dominated by the interaction of calcite and water molecules is depicted by the first two large oscillations (peaks). The threshold of oscillations then drops, and the curve continues with a horizontal-like trend demonstrating the density behavior in the bulk-like region. About 0.5 Å above the calcite slab and before the largest peak is named the free zone, which is narrower than a radius of a water molecule and therefore, no water exists there. As shown, for the local density within the layering and bulk-like zones, one can write  $\rho_{300\text{ K}} > \rho_{400\text{ K}} > \rho_{500\text{ K}}$ . Since local density cannot reflect a density inside the classified zones, the average density should be calculated instead. To this end, the integral product over the marked zones should be calculated.  $\delta$  and  $\sigma$  in Figure 1 represent the thickness of the layering and free zones, respectively. The free zone starts from the surface of the calcite slab and ends at  $z = \sigma$ . Here,  $\sigma = 0.5$  Å, which is around half of the radius of a water molecule and also equals the lower band of layering zone. The top band of the layering zone is the position in which the density experience 110% of the minimum density at the bulk-like zone. On the other hand, the end of the bulk-like zone is considered a position wherein the density reaches 90% of the minimum density at the bulk-like zone.

Figure 3 shows the calculated densities based on the results of MD simulations at different temperatures and various water lengths. The density at T=300 K, 400 K, and 500 K is displayed by black squares, red circles, and green triangles. The placement of the black squares in the top row demonstrates that low temperatures induce larger density values at a constant  $L_z$ . The green triangles at the bottom, on the other hand, illustrate that low densities correspond to high temperatures for a given  $L_z$ . In other words, T=300 K offers the highest density for all simulated lengths of water. It is worth mentioning that without calcite presence, the water density at T=300 K, 400 K, and 500 K is 996 kg/m<sup>3</sup>, 937 kg/m<sup>3</sup>, and 831 kg/m<sup>3</sup>, respectively (Green and Southard, 2019). However, with T = 300 K at the calcite-water interface, the projected density based on the MD results becomes 890 kg/m<sup>3</sup>, 899 kg/m<sup>3</sup> and 916 kg/m<sup>3</sup> for  $L_z = 2.5, 4$  and 7 nm, respectively. When the results mentioned above are compared, one can see that the density within the confinement at the calcite-water interface has diminished. Furthermore, comparing the black squares, red circles, and green triangles at a given temperature reveals that the higher  $L_z$  causes a higher density value. To understand this behavior, the intermolecular interactions inside the simulation box might be argued. It is known that at the calcite-water interface and very close to the calcite surface, the interaction between solid calcite and water prevails over the interaction between water molecules. This explains explicitly why two water layers (two huge peaks in Figure 2) are adsorbed to the calcite surface. According to Figure 3, raising  $L_z$  corresponds to the rise in density, meaning the calcite effect diminishes by increasing the average energy in the waterside. In other words, the confinement approaches the properties of the water without the presence of calcite.

## Conclusion

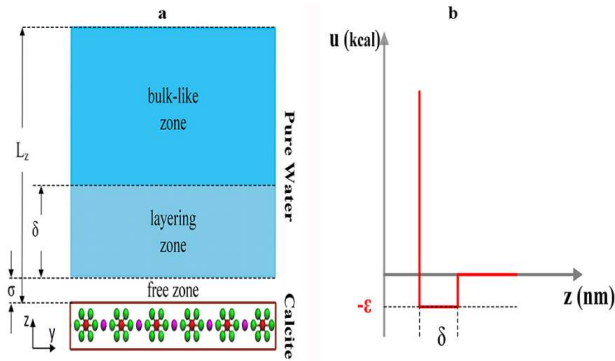
The calcite-water interface is simulated using MD technique and the density trends were plotted at different T and  $L_z$ . In the density profiles, three distinct zones can be recognized. In order to calculate the average density inside each region, the numerical integral product was applied and it is assumed that 110% of the minimum density at the bulk-like is the end of the layering zone. Although due to the effect of the calcite slab, the large oscillations are observed within the layering zone, the average density at a given temperature is smaller than the density at the same temperature without the presence of calcite. The explanation is the peaks coincide with troughs which mitigates the average value. The bolt findings of this study are:

- The maximum local density (peak) within the layering zone at T=300 K reaches 2140, 2020 and 1760 kg/m<sup>3</sup> for  $L_z=2.5$  nm, 4 nm and 7 nm, respectively.
- The minimum local density (tough) within the layering zone at T=300 K reaches 488, 501 and 504 kg/m<sup>3</sup> for  $L_z=2.5$  nm, 4 nm and 7 nm, respectively.
- The average density at T=300 K becomes 890 kg/m<sup>3</sup>, 899 kg/m<sup>3</sup> and 916 kg/m<sup>3</sup> for  $L_z = 2.5, 4$  and 7 nm, respectively.
- The average densities in the layering zone lay on lower values because the integral product sums the peaks and troughs.
- At a fixed  $L_z$ , the high density values correspond to the low temperature.

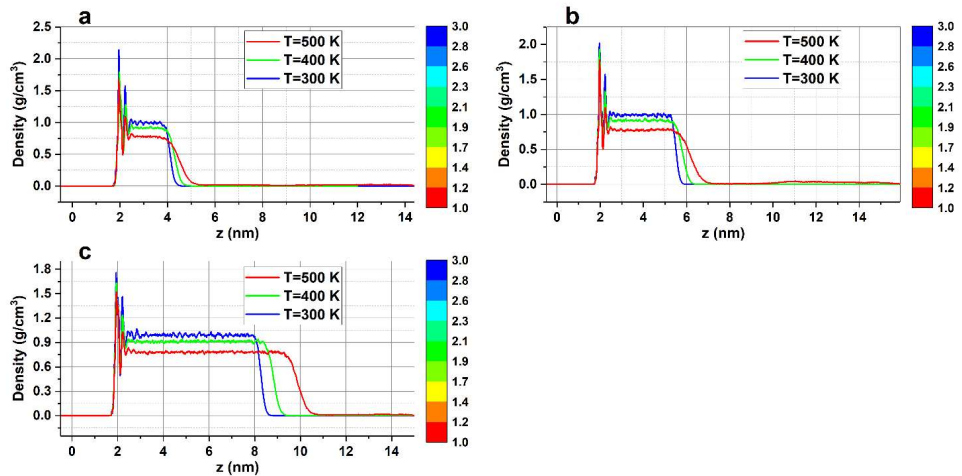
- At a fixed T, the high density values correspond to high  $L_z$ .

## References

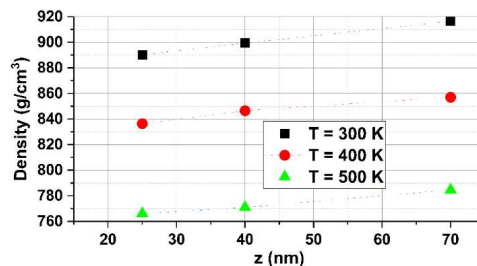
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**Figure 1.** The diagram illustrates the calcite-water configuration in MD simulation box. Three different zones are observed which are free zone, layering zone and bulk-like zone.



**Figure 2.** The profile of density of water along the  $z$ -axis for different lengths of water. As observed, the highest local density value belongs to the lowest temperature (blue curve), which is  $T=300\text{ K}$



**Figure 3.** The density value at calcite-water interface at different temperatures and various water lengths. The density within the layering zone is maximum and minimum when  $T=300\text{ K}$  and  $500\text{ K}$ , respectively. The increase in  $L_z$  at a given temperature corresponds to the rise in density value.

## Appendix C

# InterPore 14th Annual Meeting, 30May - 2June 2022

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The thermodynamic characteristics of water confined inside a nano-mineral pore differs from the bulk properties because of the competition between water-water and wall-water attractions near the solid walls. We used molecular dynamic (MD) simulation, to capture the influence of the solid walls of a slit shape calcite nanopore on the confined water provided in different widths namely 2 nm, 3 nm, 4 nm and 5 nm. The simulations are conducted with NVT ensemble at  $T = 300$  K, 350 K, 400 K, and 450 K while each simulation run is completed within 6 ns. The results shows the density and total energy near the pore wall increases with temperature. To determine the new properties imposed by the nano-calcite pore, an equation of state (EoS) was developed based on the statistical association fluid theory (SAFT) by introducing a new term for Helmholtz free energy. Within a reliable absolute relative error (ARE), the results of the modified SAFT overlap with the outcomes of MD simulation. This approach can be applied in predicting the fluid properties near wall, which is the concern of several fields such as CO<sub>2</sub> storage, hydrogen storage and enhanced oil recovery (EOR) and etc.





Appendix D

## **Geoconversion 2022**



## Low Salinity Water Impact on the Calcite-Water Interface: A Molecular Dynamic Study

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### Summary

In recent years, low salinity water (LSW) injection into carbonates and sandstone reservoirs, known as water flooding, has been adopted as a promising technique for enhanced oil recovery (EOR). This technology which is appealing to industry because of its low cost, can maintain pressure after initial depletion and displace oil by exploiting the effect of the viscous forces. Despite the rising industrial interest in LSW method, a coherent mechanism explanation for the technology has yet to be developed. Unknown molecular interactions in a rock-brine system are the primary cause for the lack of a cohesive mechanism driving LSW. In order to study molecular aspects of the interaction between a rock slab (solid phase) and brine (fluid phase), we used the molecular dynamic (MD) technique to simulate a system including calcite and brine solution. The results show that all mono/divalent ions are hydrated initially and a layer of water molecules located at 1.85 Å above the calcite surface. The Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup> and SO<sub>4</sub><sup>2-</sup> ions scatter at a radius of 2.45 Å, 4.15 Å, 4.45 Å, and 4.15 Å from the calcite slab, establishing the electrical double layer (EDL) along the z-axis and parallel to the calcite surface.

### Introduction

Over millions of years, the cohabitation of brine water and oil within an oil reservoir has resulted in a thermodynamic equilibrium between reservoir rock, brine and oil. Water flooding with a known composition can disrupt the current equilibrium by altering the rock's wettability. Rock wettability within the oil reservoirs plays an essential role in subsurface multiphase flow behavior. Thus, advancements in EOR techniques are directly or indirectly related to changes in the wetting properties of the reservoir. Recently, water flooding has been utilized widely to displace oil, thereby improving the EOR technology. Injection of water with low salinity includes injection of diluted brine in either carbonates or sandstone reservoirs through secondary recovery/tertiary mode to enhance the oil recovery<sup>1</sup>. The industry as well showed immense interest in this technology. Because LSW injection, on the one hand, is cheap and straightforward to apply. On the other hand, it can maintain pressure after initial depletion and displace oil by exploiting the effect of the viscous forces.

Many research studies have focused on the capability of LSW injection until now. It is known that the presence of mono/divalent ions (i.e., Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup> and SO<sub>4</sub><sup>2-</sup>) control the wettability transition of the reservoir from thoroughly oil-wet to water-wet<sup>2</sup>. For example, Austad<sup>3</sup> et al. have reported that CaSO<sub>4</sub> is a key chemical for observing the LSW injection effect. They raised the sulfate content within an experiment while decreasing the NaCl concentration, and they found 88 percent

improvement in recovery. They also declared that the EOR low salinity impact is feasible in both carbonate and sandstone reservoirs. Mehraban<sup>4</sup> et al. have observed that not only concentrations of sulfate ions but also higher  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  concentrations resulted in considerable improvements in wettability alteration and recovery.

Improved oil recovery using the LSW approach is ascribed to several mechanisms, such as interfacial tension reduction<sup>5</sup>, multicomponent ion exchange (MIE)<sup>6</sup>, and electrical double layer (EDL) expansion<sup>7</sup>. Despite numerous attempts to realize the driving processes of wettability change, the interaction mechanism between LSW ions and the rock surface remains unknown at the molecular scale. To investigate the molecular interactions between a rock slab and brine, we employed molecular dynamic (MD) simulation. In this simulation, calcite plays role of the solid mineral interacting with a brine solution, including  $\text{H}_2\text{O}$  molecules,  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  ions.

## Theory

Calcite ( $\text{CaCO}_3$ ) is a mineral found in abundance in natural geological systems. Since calcite is a key ingredient of limestone, dolomite, and chalk, it is also among the most prevalent mineral observed in oil reservoirs. Hence, investigation of the calcite mineral interacting with the brine on a molecular scale can shed light on the complexity of the molecular mechanism leading to the oil displacement due to the injection of LSW. As a result, several studies have focused on the surface characteristics of calcite.

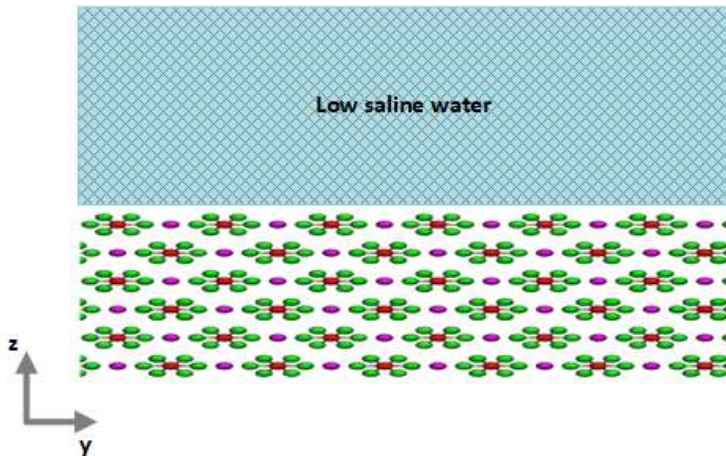
To study molecular interactions between a calcite slab and brine solution, we employed LAMMPS<sup>8</sup> (Large Atomic/Molecular Massively Parallel Simulator) for molecular dynamic (MD) simulations. In this study, calcite ( $\text{CaCO}_3$ ) was chosen as the rock mineral because it is among the most prevalent mineral found in oil reservoirs. The most stable cleavage of calcite, 1014 plane, was utilized to construct a rock surface and the established force field by Xiao<sup>9</sup> was chosen to control the interaction among different species of calcite (i.e., Ca, C and O) in the solid phase. Then, the water molecules are wrapped and mounted above the constructed calcite slab with PACKMOL<sup>10</sup> software. TIP3P<sup>11</sup> defines the force field between the water molecules.

Table 1. Chemical composition of the different components in low saline water (LSW).			
Low saline water ions			
$\text{Na}^+$ [ppm]	$\text{Cl}^-$ [ppm]	$\text{Mg}^{2+}$ [ppm]	$\text{SO}_4^{2-}$ [ppm]
13700	24468	1620	3310
<i>*Note: Total density of Low saline water = 1.196 gr/cm<sup>3</sup></i>			

The utilized elements and associated concentrations have been tabulated in Table 1. The number of elements is based on the density at T=300 K and pressure of 1 atm.

Table 2. calculated number of LSW molecules for MD simulation.				
Low saline water ions				
H <sub>2</sub> O	Na <sup>+</sup>	Cl <sup>-</sup>	Mg <sup>2+</sup>	SO <sub>4</sub> <sup>2-</sup>
1101	14	16	2	1

Table 2 includes the number of required molecules to make the chemical concentrations which are mentioned in Table 1.

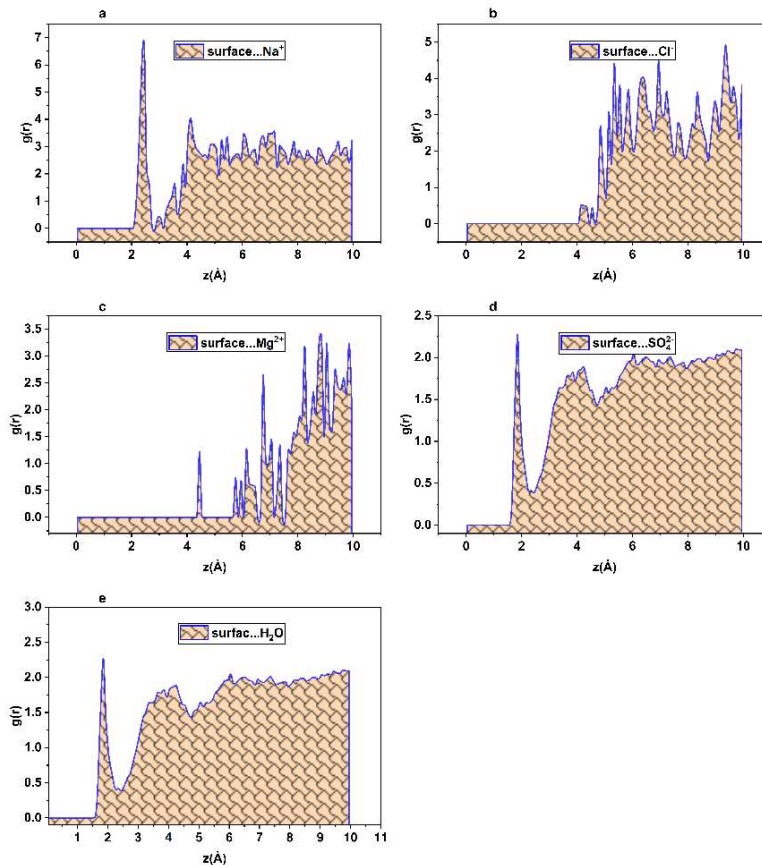


**Figure 1.** The sketched geometry represents the schematic configuration of the second system simulated with MD, which includes LSW (H<sub>2</sub>O, Na<sup>+</sup>, Cl<sup>-</sup>, SO<sub>4</sub><sup>2-</sup> and Mg<sup>2+</sup>) interacting with a calcite slab.

To make a brine solution, it is required to mix the pure water molecules with mono/divalent ions. To this end, water molecules are combined with Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup> and SO<sub>4</sub><sup>2-</sup> representing the brine solution. Different protocols define the governing force field between mentioned cations and anions. To put it differently, the OPLS-AA<sup>12</sup> force field models the interaction of Na<sup>+</sup>, Cl<sup>-</sup> and Mg<sup>2+</sup>, whereas the interaction of divalent anion SO<sub>4</sub><sup>2-</sup> is modeled by Williams<sup>13</sup> force field. A canonical ensemble (NVT) implemented by the Nose-Hoover<sup>14</sup> thermostat ensures that the simulation is conducted at T=300 K. Taking a timestep of 1 ns, the simulation run is completed within 20 ns, 5 ns for equilibration and 15 ns for production.

## Results and discussions

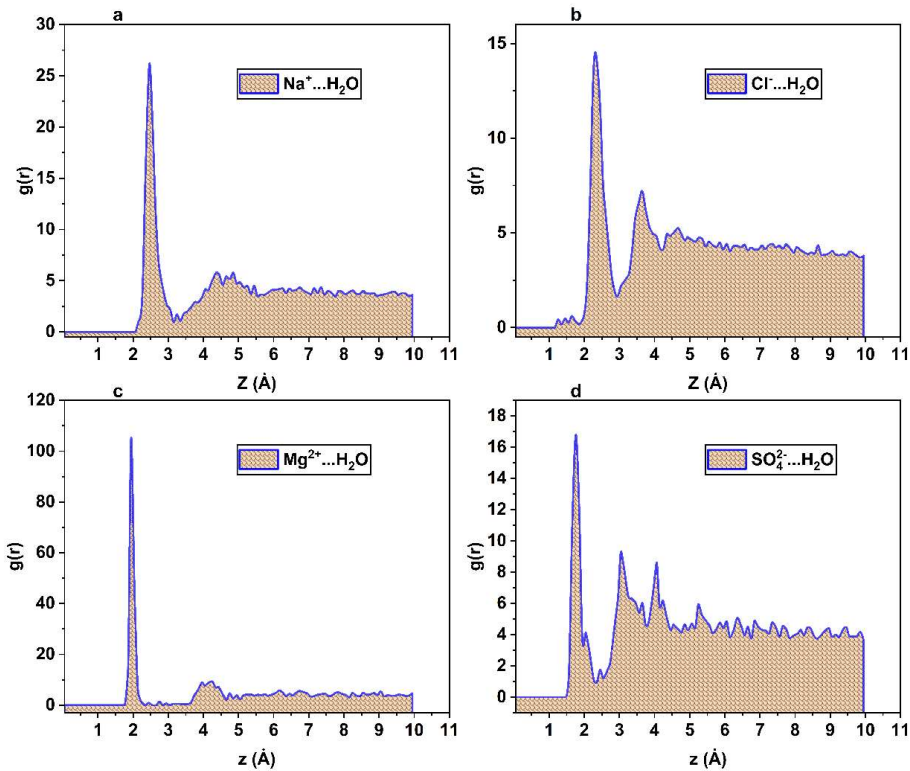
The trend of the radial distribution function of different ions and water molecules are plotted in Figure 2. According to Figure 2e, a layer of water is adsorbed on the rock surface with a local density that is 2-3 times that of the bulk density. This observation and relevant consequences have been reported in previous studies<sup>15,16</sup>. The water molecules connect to the oxygen of the calcite from the hydrogen side and locate at a radius of 1.85 Å along the z-axis. After water molecules, Na<sup>+</sup> ions stay at the closest distance to the calcite surface, which is 2.45 Å, as shown in Figure 2a.



**Figure 2.** Illustration of the radial distribution function for different ions and water molecules with respect to the solid surface at T=300 K. The distance between Na<sup>+</sup>, Cl<sup>-</sup>, Mg<sup>2+</sup>, SO<sub>4</sub><sup>2-</sup> and H<sub>2</sub>O from solid surface is 2.45 Å, 4.15 Å, 4.45 Å, 4.15 Å and 1.85 Å, respectively.

Rest of the mono and divalent ions are  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  which are scatter at a radius of 4.15 Å, 4.45 Å, and 4.15 Å from the calcite slab, respectively.

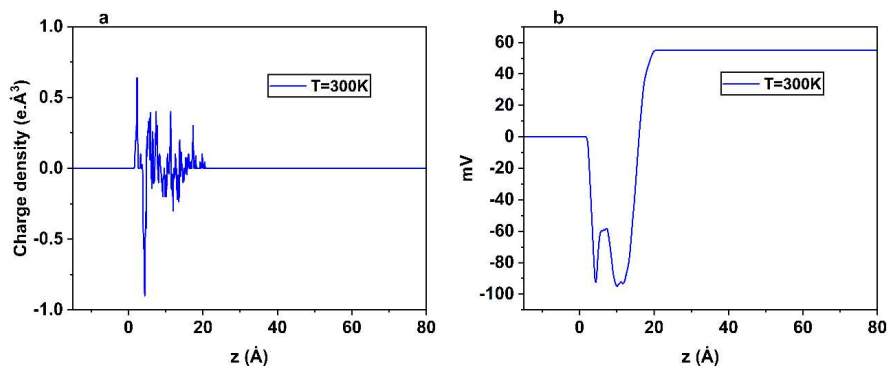
The trend of radial distribution function  $g(r)$  in Figure 3 presents the distance between each anion and cation and the water molecules which surrounded them at  $T=300\text{K}$ . As seen, all of the mono/divalent ions are hydrated because the water molecules scatter at a distance of 2.5 Å, 2.2 Å, 1.85 Å, and 2.4 Å, from  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ , respectively. The shorter hydration radius is due to the higher hydration energy impact.



**Figure 3.** The profile of the radial distribution function shows the distance between the water molecules and different ions at  $T=300\text{K}$ . All of the mono/divalent ions are hydrated and the water molecules scatter at a distance of 2.5 Å, 2.2 Å, 1.85 Å, and 2.4 Å, from  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{SO}_4^{2-}$  and  $\text{Mg}^{2+}$ , respectively.

Figure 4 shows the charge density profile. As seen, the development of a positive stern layer and negative diffuse layer is indicated by a positive and negative peak next to the calcite surface. The charge density profile above the calcite slab demonstrates the establishment of an electrical

double layer (EDL) parallel to the calcite slab, which includes monovalent cations in the stern layer and anions within the diffuse layer. Calculation of the mathematical area under the curve for charge density (Figure 4a) shows that the charge summation is negative.



**Figure 4.** The charge density and zeta potential are shown with plots a and b, respectively.

## Conclusions

Calcite is one of the most common minerals identified in oil reservoirs because it is the main component of limestone, dolomite, and chalk. Thus, investigation of the underlying mechanism of calcite-LSW interaction in a molecular scale can result in new understandings which can improve the efficiency of the EOR technology. Since, the influence of the LSW on EOR improvement has rarely been addressed at the molecular level, we used LAMMPS to explore the surface interaction of calcite with brine solution. Study of the different ions interaction with the calcite surface shows that the mono/divalent ions initially are hydrated. Water molecules from the first adsorbed layer on the calcite surface, dwelling at the closest distance, 1.85 Å above the calcite surface. Following that, hydrated  $\text{Na}^+$ ,  $\text{Cl}^-$ ,  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$  remain at 2.45 Å, 4.15 Å, 4.45 Å, and 4.15 Å with respect to the solid surface, respectively. The charge density profile also exhibits the formation of the EDL parallel to the calcite surface, including the positive stern layer and the negative diffuse layer. Therefore, it can be said that the positive stern layer is formed by  $\text{Na}^+$  and  $\text{Cl}^-$  established the negative diffuse layer. The observed oscillation of charge density curve after the diffuse layer reflects the presence of  $\text{Mg}^{2+}$  and  $\text{SO}_4^{2-}$ . The presence of  $\text{SO}_4^{2-}$  in the outer layer of EDL and negative charge summation of EDL might be a good cause for repulsion of the oil molecules and turning the calcite surface water wet.



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